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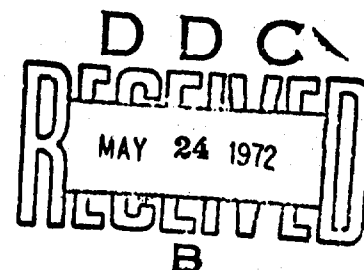
APCRL-72-0082  
22 DECEMBER 1971  
PHYSICAL SCIENCES RESEARCH PAPERS, NO. 477



**AIR FORCE CAMBRIDGE RESEARCH LABORATORIES**  
L. G. HANCOM FIELD, BEDFORD, MASSACHUSETTS

**The Temperature Coefficients of Acoustic  
Surface Wave Velocity and Delay on  
Lithium Niobate, Lithium Tantalate,  
Quartz, and Tellurium Dioxide**

ANDREW J. SLOBODNIK, Jr.



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CONSTRUCTION/APPENDIX CODES	
LIST:	ANAL. AND/OR SPECIAL
A	

Unclassified

Security Classification

DOCUMENT CONTROL DATA - R&D		
(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)		
1. ORIGINATING ACTIVITY (Corporate author) Air Force Cambridge Research Laboratories (LZM) L. G. Hanscom Field Bedford, Massachusetts 01730		2a. REPORT SECURITY CLASSIFICATION Unclassified 2b. GROUP
3. REPORT TITLE THE TEMPERATURE COEFFICIENTS OF ACOUSTIC SURFACE WAVE VELOCITY AND DELAY ON LITHIUM NIOBATE, LITHIUM TANTALATE, QUARTZ, AND TELLURIUM DIOXIDE		
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) Scientific. Interim.		
5. AUTHOR(S) (First name, middle initial, last name) Andrew J. Slobodnik, Jr.		
6. REPORT DATE 22 December 1971	7a. TOTAL NO. OF PAGES 128	7b. NO. OF REFS 29
8a. CONTRACT OR GRANT NO.	9a. ORIGINATOR'S REPORT NUMBER(S) AFCRL-72-0082	
b. PROJECT, TASK, WORK UNIT NOS. 5635-03-01	9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report) PSRP No. 477	
c. DOD ELEMENT 61102F		
d. DOD SUBELEMENT 681305		
10. DISTRIBUTION STATEMENT Approved for public release; distribution unlimited.		
11. SUPPLEMENTARY NOTES TECH, OTHER		12. SPONSORING MILITARY ACTIVITY Air Force Cambridge Research Laboratories (LZM) L. G. Hanscom Field Bedford, Massachusetts 01730
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DD FORM 1473  
1 NOV 65

Unclassified

Security Classification

Unclassified

Security Classification

16.	KEY WORDS	LINK A		LINK B		LINK C	
		ROLE	WT	ROLE	WT	ROLE	WT
	Acoustic surface waves Temperature coefficient of delay Temperature coefficient of velocity Acoustic surface wave velocities Coupling to interdigital transducers Surface wave pure mode axes Tellurium dioxide Lithium tantalate Microwave acoustic material constants Acoustic signal processing Quartz Lithium niobate Surface wave numerical data Wave propagation Piezoelectric materials Acoustic delay lines Zero temperature coefficient cuts of $\text{TeO}_2$ Surface wave power flow angle						

Unclassified

Security Classification

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MICROWAVE PHYSICS LABORATORY

PROJECT 5635

**AIR FORCE CAMBRIDGE RESEARCH LABORATORIES**

L. G. HANSCOM FIELD, BEDFORD, MASSACHUSETTS

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**AIR FORCE SYSTEMS COMMAND**  
**United States Air Force**



## Abstract

A systematic search for zero temperature coefficient of acoustic surface wave delay has been made on the materials  $\text{TeO}_2$ , quartz,  $\text{LiTaO}_3$  and  $\text{LiNbO}_3$ . Such temperature compensated orientations are needed for application to wideband multi-function modems and other signal processing devices.

Two temperature compensated cuts of  $\text{TeO}_2$  have been discovered. These two orientations possess simultaneously zero temperature coefficients of delay, zero power flow angles and ultra-low surface wave velocities (1387 and 1424 m/sec). This last property allows long time delays in short spaces with consequent reductions in size and weight. The piezoelectric-coupling parameters ( $\Delta v/v$ ) for these orientations are  $2 \times 10^{-6}$  and  $8 \times 10^{-5}$ .

The lowest temperature coefficient of delay on  $\text{LiTaO}_3$  was found to be 23 ppm/°C for an orientation having 1.55° of beam steering. The sacrifice of several parts per million in temperature sensitivity (to 30 and 33 ppm/°C) yields two pure mode orientations having velocities of 3300 m/sec and moderate coupling ( $\Delta v/v = 0.0037$  and  $0.0045$ ). An orientation of  $\text{LiTaO}_3$  has been discovered having substantially higher coupling ( $\Delta v/v = 0.0084$ ) than any previously known.

The 41.5° rotated cut, X-propagating orientation of  $\text{LiNbO}_3$  has a temperature coefficient of delay of 72 ppm/°C which is the best yet found for this material.

## Preface

This work was undertaken in response to the Rome Air Development Center (RADC) Research Need 71-21 as documented on AF Form 111 and entitled "Research on Surface Wave Phenomena for Application to Wideband Multi-Function Modems." The following statements are quoted from this document. "New materials or cut orientations are needed which can support acoustic surface waves and which possess zero or very small temperature coefficients with low insertion loss." "Currently, the most popular materials used to provide signal processing functions with acoustic surface waves are the piezoelectrics. Of those used, only the ST cut of quartz provides a zero-temperature coefficient over any appreciable range."

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# **The Temperature Coefficients of Acoustic Surface Wave Velocity and Delay on Lithium Niobate, Lithium Tantalate, Quartz, and Tellurium Dioxide**

## **1. INTRODUCTION**

Surface wave-acoustic devices are currently coming into widespread systems use for the performance of a variety of delay and signal processing functions (Bush et al, 1970; Bush, 1971). However, for many applications it is highly desirable to use a temperature compensated cut to support the surface waves, that is, a crystal-line orientation having zero temperature coefficient of delay. In fact, Carr et al (1971) have shown that a limitation on the application of surface wave encoders and decoders to multiple-access, secure communications systems is the degradation of the peak-to-sidelobe ratio of the autocorrelation function due to temperature differences.

In spite of several recent theoretical and experimental searches (Schulz et al, 1970; Holland and Schulz, 1970; Welsh, 1971; Lewis et al, 1971, and Schulz and Holland, 1971) the only temperature compensated cuts presently known are on  $\alpha$  quartz. The most widely used is the ST-cut, X-propagating orientation discovered by Schulz et al (1970). Unfortunately, crystalline quartz possesses a very low piezoelectric coupling constant which leads to undesirably high insertion losses for any devices constructed using this material.

Two materials which have relatively high piezoelectric coupling are lithium niobate and lithium tantalate. An orientation having zero temperature coefficient

(Received for publication 17 December 1971)

Here  $T$  is temperature and  $v_s$  is the surface wave velocity. A desired temperature compensated cut occurs at room temperature whenever Eq. (1) equals zero for  $T_1 = 25^\circ\text{C}$ .

For the purposes of numerical calculation, the following approximation to Eq. (1) was used to compute the temperature coefficient of velocity (for  $\text{TeO}_2$ ,  $20^\circ\text{C}$  was used as the center reference temperature):

$$\text{TCV} \approx \frac{1}{v_s(25^\circ\text{C})} \left[ \frac{v_s(35^\circ\text{C}) - v_s(15^\circ\text{C})}{20^\circ\text{C}} \right] \quad (2)$$

The actual procedure consisted of three steps:

- I Computation of material constants at  $15^\circ\text{C}$ ,  $25^\circ\text{C}$  and  $35^\circ\text{C}$  ( $10^\circ\text{C}$ ,  $20^\circ\text{C}$  and  $30^\circ\text{C}$  for  $\text{TeO}_2$ )
- II Computation of surface wave velocities at each of these temperatures using the results of step I
- III Use of Eq. (2) to compute TCV.

As the surface wave velocity is highly anisotropic, each of these three steps had to be repeated at one degree intervals for all orientations investigated.

Step I was accomplished using the temperature coefficients of the material constants themselves, as tabulated in Appendix A, in conjunction with Eq. (3) which is merely a truncated Taylor Series expansion.

$$X(T) \approx X(T_0) \left[ 1 + \frac{1}{X(T_0)} \frac{\partial X}{\partial T} (T - T_0) + \frac{1}{2X(T_0)} \frac{\partial^2 X}{\partial T^2} (T - T_0)^2 \right] \quad (3)$$

Here  $X$  is the desired material constant,  $T_0$  is room temperature and  $1/X(T_0) \partial X / \partial T$  and  $1/2X(T_0) \partial^2 X / \partial T^2$  are the first and second order normalized temperature coefficients respectively. Where second order coefficients of the material constants were not readily available, Eq. (3) was truncated after the first order term. Also, where direct measurements of the temperature coefficients of the density were not available, these coefficients were calculated from the coefficients of thermal expansion according to Eq. (4) which is derived in Appendix B.

$$\frac{1}{\rho(T_0)} \frac{\partial \rho}{\partial T} = -[\alpha_{11} + \alpha_{22} + \alpha_{33}] \quad (4)$$

Here  $\rho$  is the density and  $\alpha_{ii}$  are the coefficients of thermal expansion.

The results of step I, that is complete material constant matrices for lithium niobate, lithium tantalate, quartz and tellurium dioxide at  $15^\circ\text{C}$ ,  $25^\circ\text{C}$  and  $35^\circ\text{C}$  ( $10^\circ\text{C}$ ,  $20^\circ\text{C}$  and  $30^\circ\text{C}$  for  $\text{TeO}_2$ ), are tabulated in Appendix C.

Step II consisted of computing the surface wave velocities at 15°C, 25°C and 35°C using the results of step I. The calculations were made using a computer program based on the work of Campbell and Jones (1968, 1970a and 1970b).

The results of step II were then directly substituted into Eq. (2) thus determining the temperature coefficient of velocity.

For most delay line, filter and other signal processing applications the actual parameter of interest is not the temperature coefficient of velocity but is in fact the change in delay time with temperature (Lolland and Schulz, 1970). The first order temperature coefficient of delay is given by Eq. (5).

$$\text{TCD} = \frac{1}{\tau} \frac{\partial \tau}{\partial T} \Big|_{T_1} \quad (5)$$

Here  $\tau = l/v_s$  is the delay time and  $l$  is the distance between two material points.

The temperature coefficient of delay is related to the temperature coefficient of velocity through the coefficient of thermal expansion,  $\alpha$ .

$$\frac{1}{\tau} \frac{\partial \tau}{\partial T} = \left( \frac{l}{v_s} \right)^{-1} \frac{\partial}{\partial T} \left( \frac{l}{v_s} \right) = \frac{1}{l} \frac{\partial l}{\partial T} - \frac{1}{v_s} \frac{\partial v_s}{\partial T} \quad (6a)$$

$$\frac{1}{\tau} \frac{\partial \tau}{\partial T} = \alpha - \frac{1}{v_s} \frac{\partial v_s}{\partial T} \quad (6b)$$

Note that the appropriate value of  $\alpha$  in this equation depends very much on the orientation being considered since the matrix of the coefficient of thermal expansion is anisotropic. The proper value of  $\alpha$  is obtained by rotating the basic matrix through the appropriate Euler angles (Goldstein, 1970) and combining in the standard manner similar to the methods used in rotating the elastic, piezoelectric and dielectric constants for velocity calculations (Campbell and Jones, 1968).

For the purposes of this report, Eq. (6) was used directly for calculating TCD by using the previously determined approximate value of TCV along with the appropriate value of  $\alpha$ .

### 3. DATA

The purpose of this section is to present a tabulation (beginning on page 9) of the temperature coefficients of velocity and delay for a wide variety of cuts and orientations of  $\text{LiNbO}_3$ ,  $\text{LiTaO}_3$ , quartz and tellurium dioxide. In addition, the surface wave velocity, the coupling parameter,  $\Delta v/v$  (Campbell and Jones, 1968 and 1970b), and the electromechanical power flow angle,  $\phi$  (the deviation of the time

average power flow from the phase velocity vector) are presented on facing pages. This information allows the device designer to choose a given material orientation with full knowledge of all applicable parameters including coupling of electromagnetic to acoustic energy, pure mode axes (directions for which  $\phi = 0$ ) and the effect of beam steering (Slobodnik et al, 1970 and Slobodnik and Conway, 1970b). Use of electromechanical power flow rather than the incomplete mechanical power provides greater accuracy than previously available (Slobodnik and Conway, 1970a).

The orientations tabulated are quantitatively defined using the Euler angles  $\lambda$ ,  $\mu$ , and  $\theta$  as explained in Figure 1. The standard cuts and orientations are shown in Figure 2a to c along with their corresponding Euler angles. Many non-standard orientations have also been investigated in the attempt to discover zero or minimum values of the temperature coefficient of delay. These orientations are identified only by their Euler angles. The use of "rotated constants" allows further flexibility in the investigation of off-axis orientations (although round-off errors are somewhat greater in computation of temperature coefficients). In these cases the propagation axes 1, 2 and 3 do not initially line up with the crystalline axes X, Y and Z but rather with those crystalline orientations resulting from a preliminary Euler angle rotation through the "rotated constant" angles. For further details of this notation the reader is referred to Appendix D.

Finally it can be noted that, wherever possible, the data tabulated in this section was compared with previous theoretical and experimental results (Schulz et al, 1970; Holland and Schulz, 1970; Welsh, 1971; Lewis et al, 1971; and Schulz and Holland, 1971). In all cases reasonable agreement was obtained.

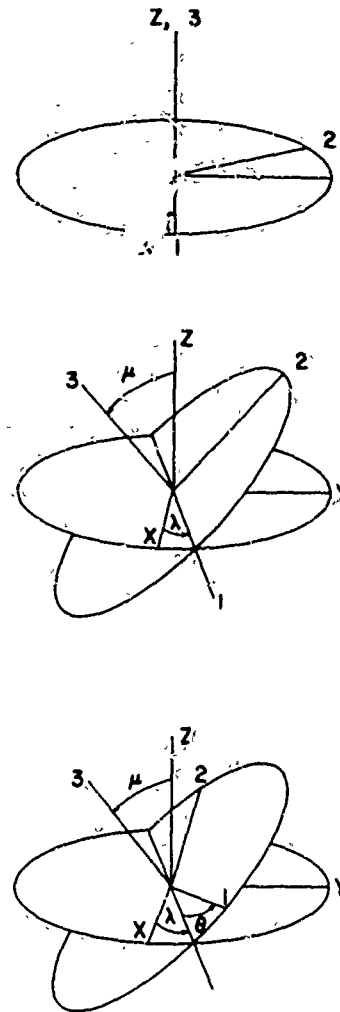


Figure 1. Coordinate System Used to Define Acoustic Surface Wave Propagation. The phase velocity vector lies along the 1 axis while the plate normal lies along the negative 3 axis. The crystalline axes are given by X, Y, and Z while the Euler angles are  $\lambda$ ,  $\mu$ , and  $\theta$  (after H. Goldstein in Classical Mechanics).

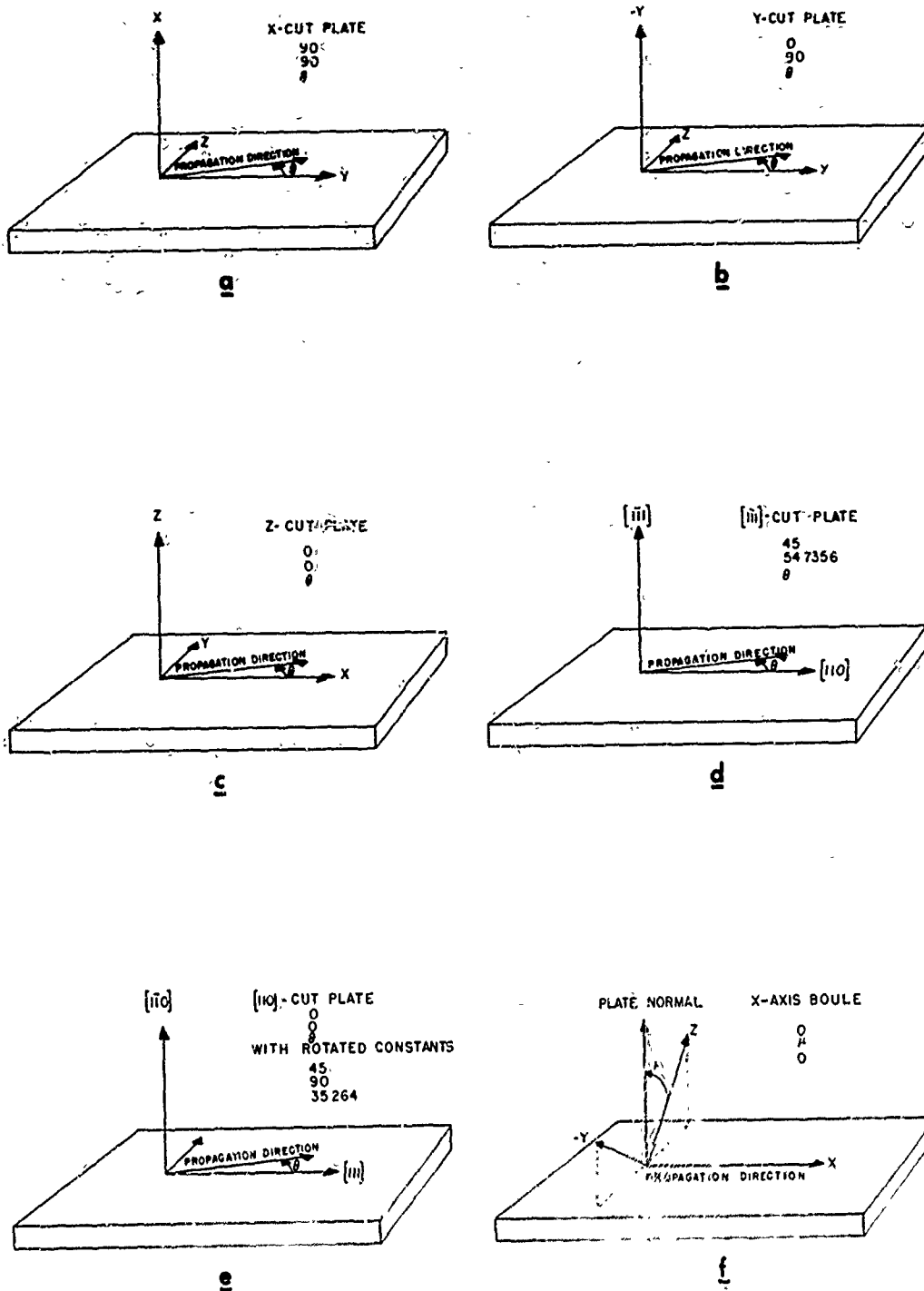


Figure 2. Fifteen Standard Crystalline Orientations Along with Corresponding Euler Angle Notation

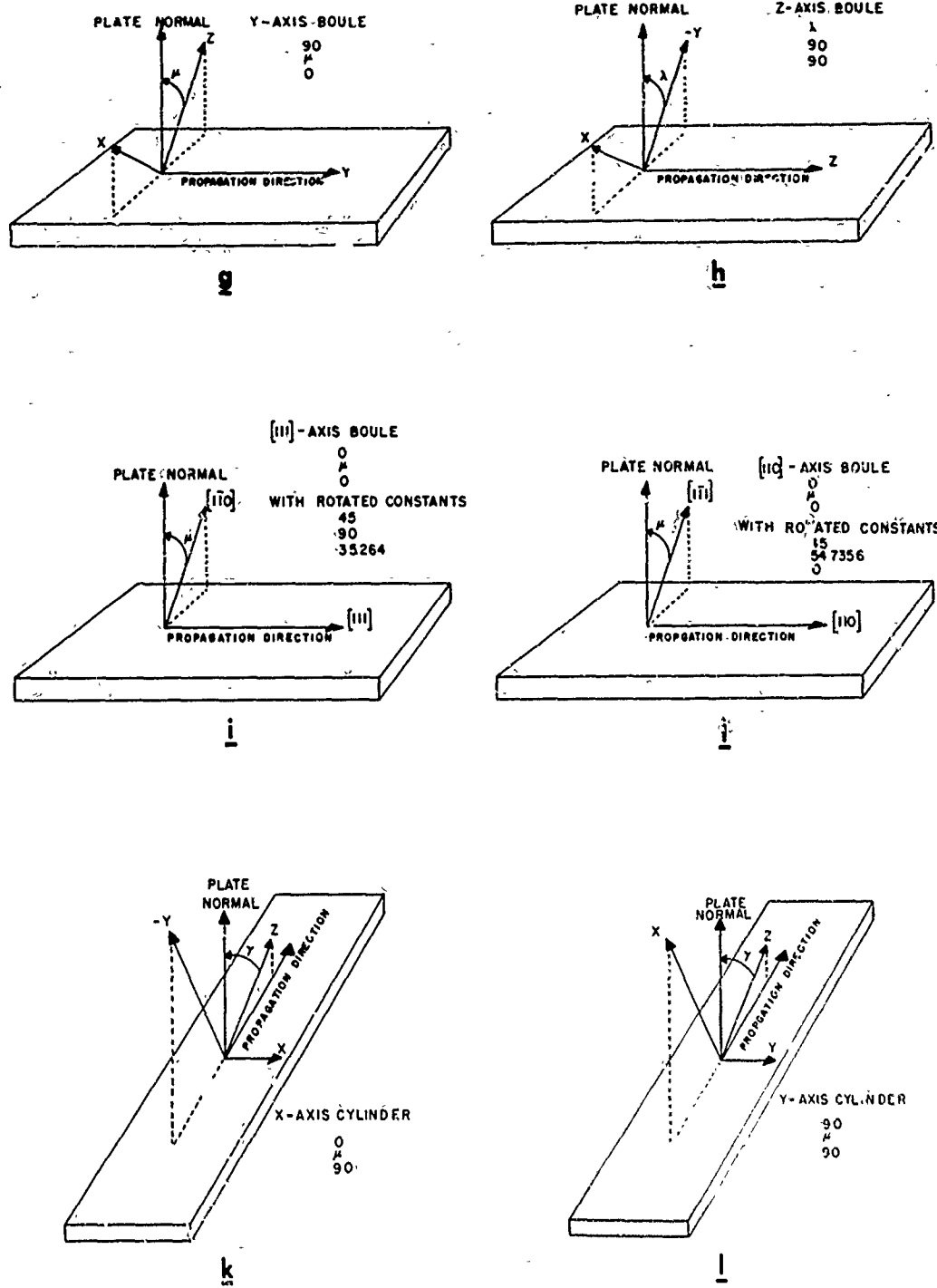


Figure 2 (Contd). Fifteen Standard Crystalline Orientations Along With Corresponding Euler Angle Notation

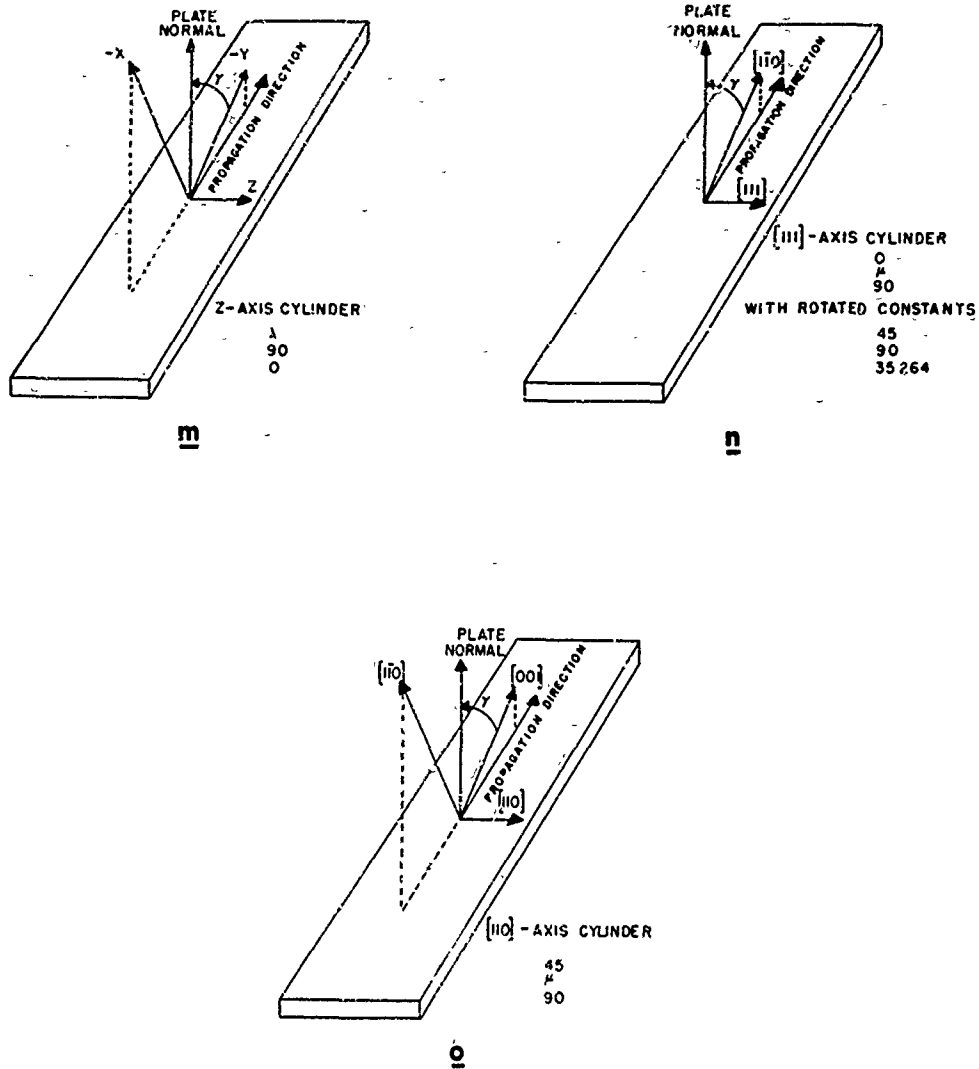
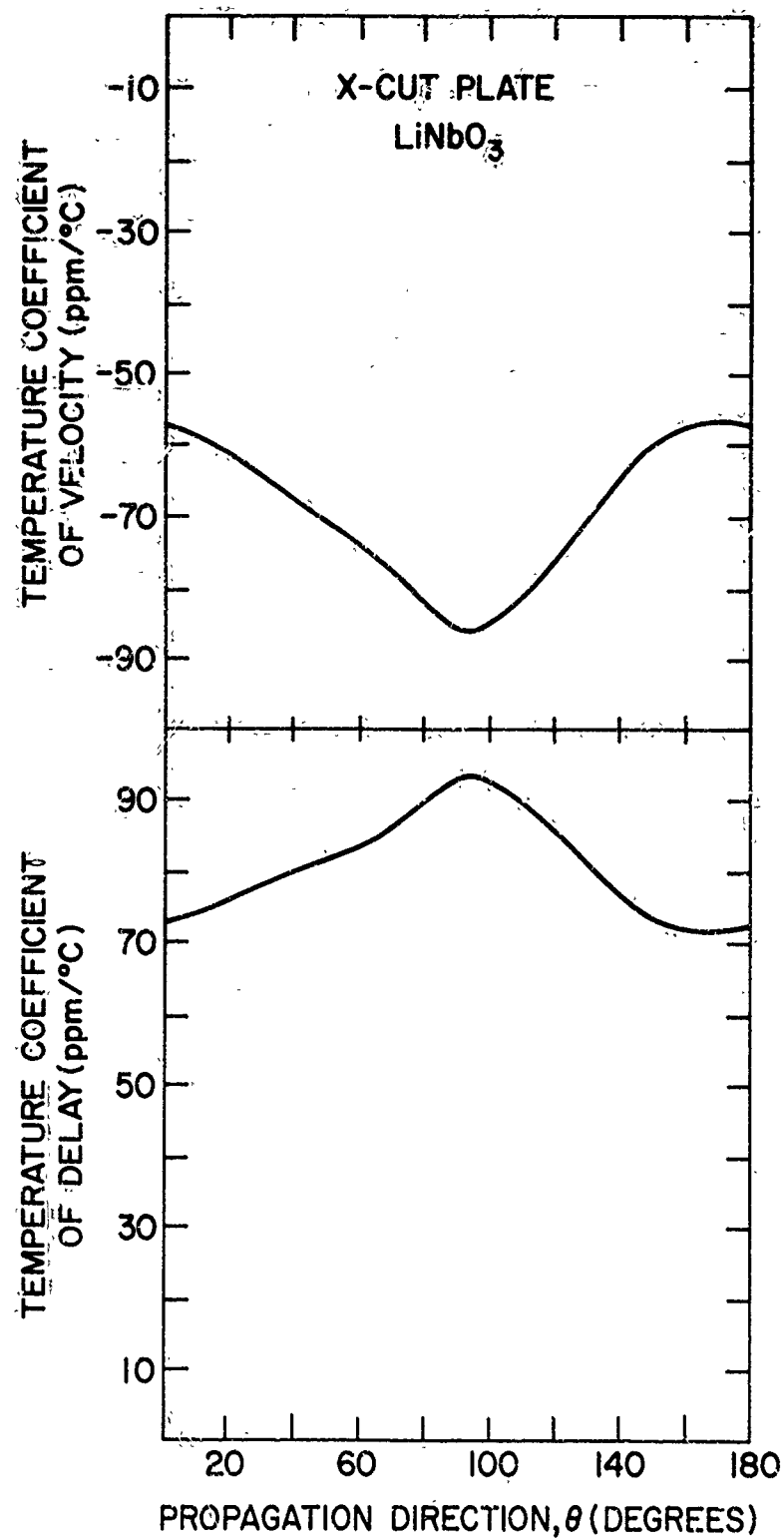
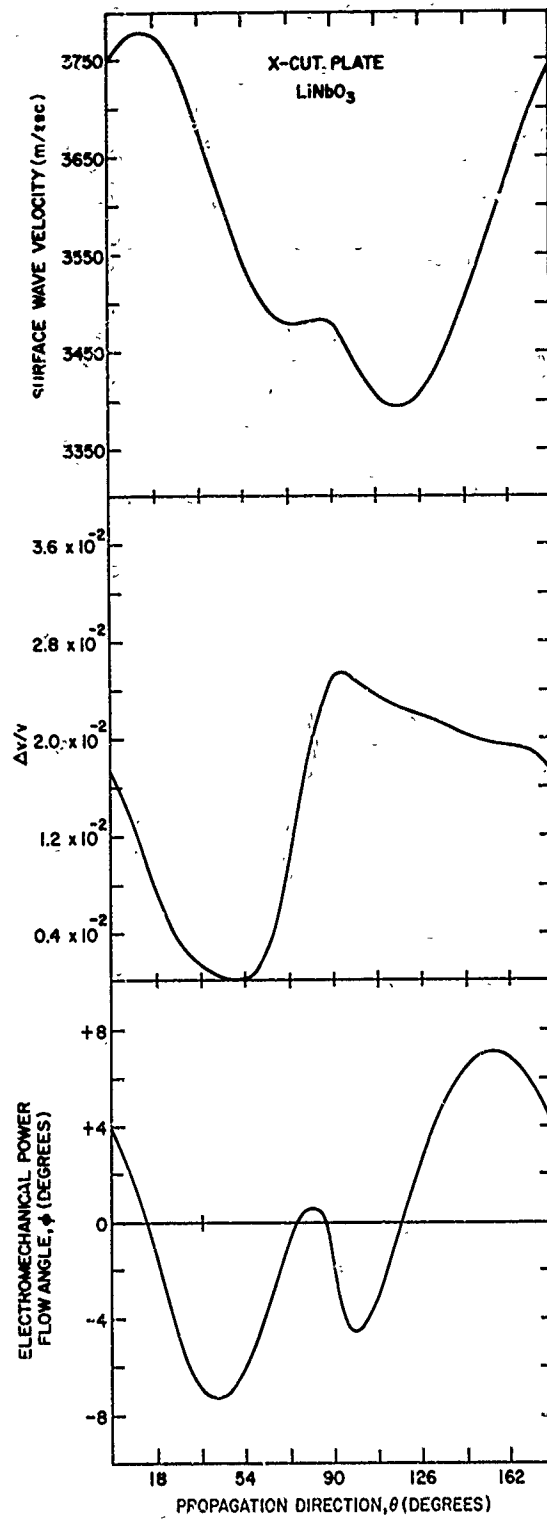


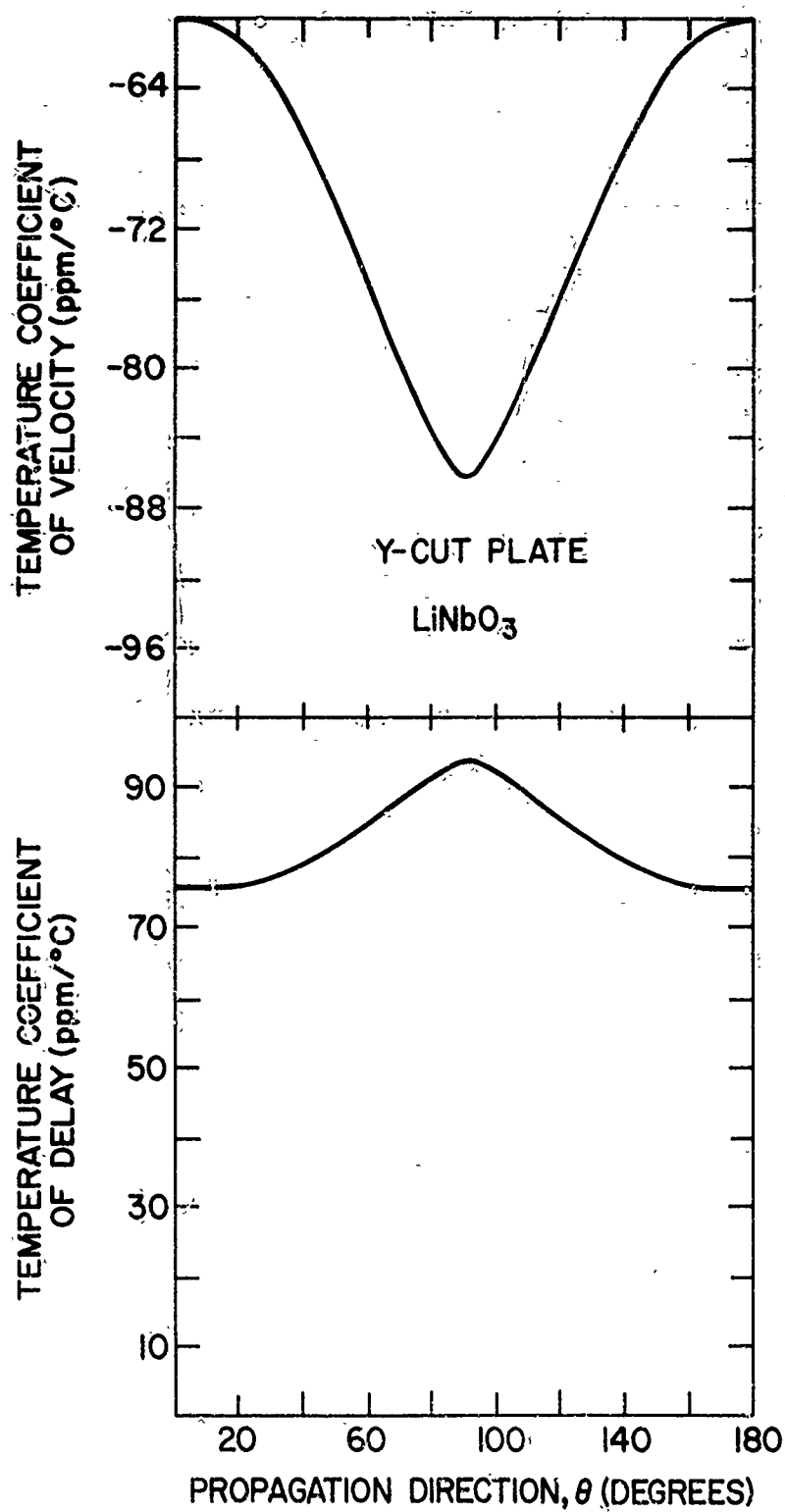
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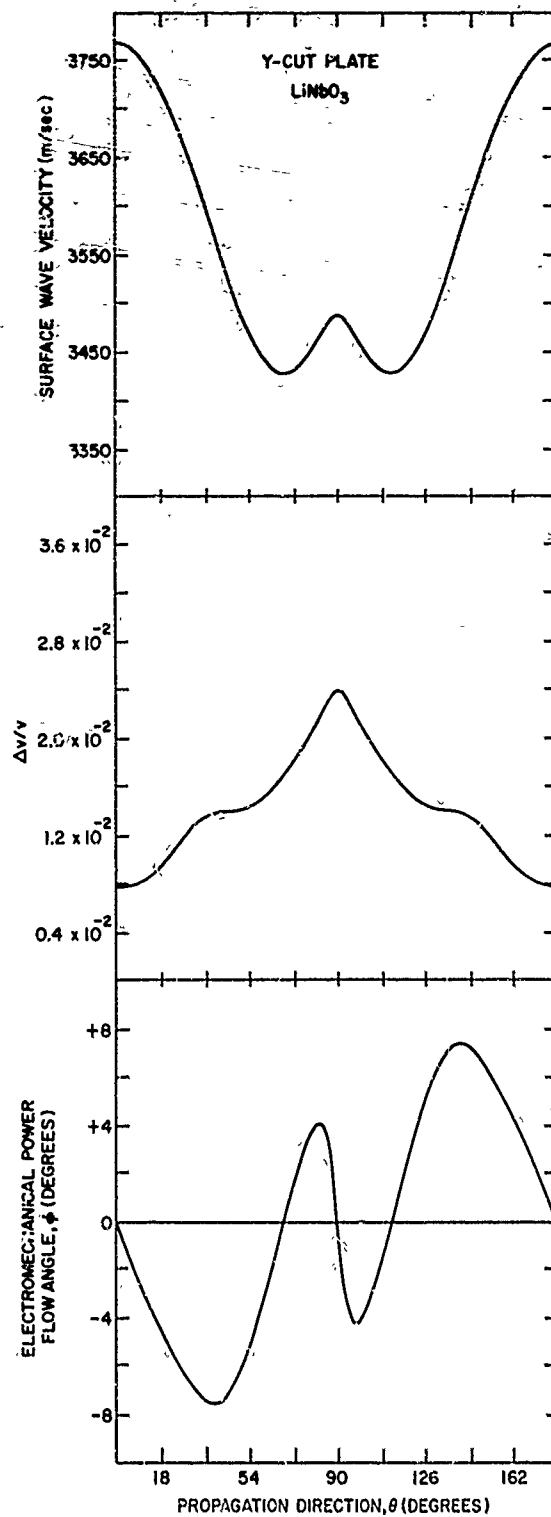


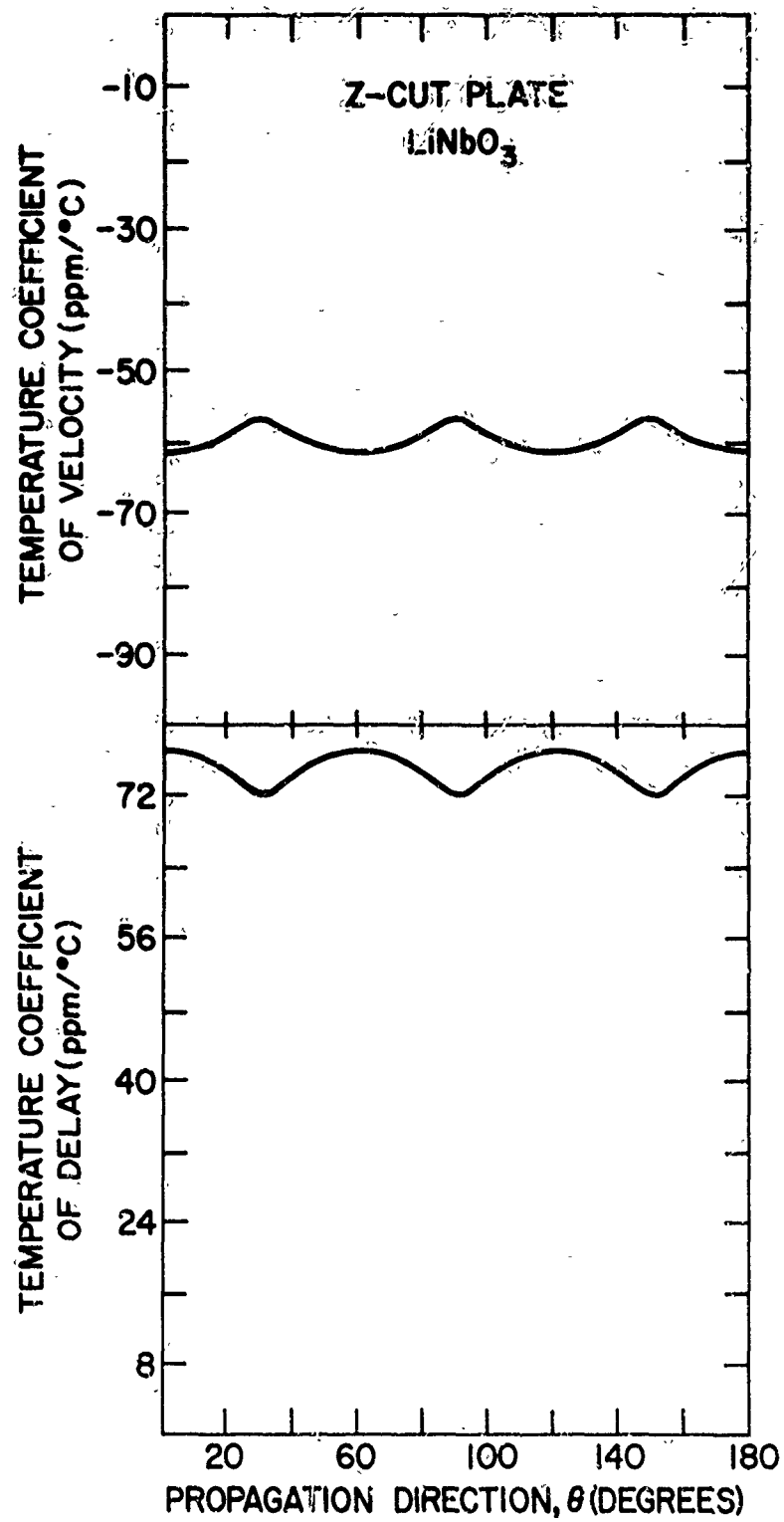
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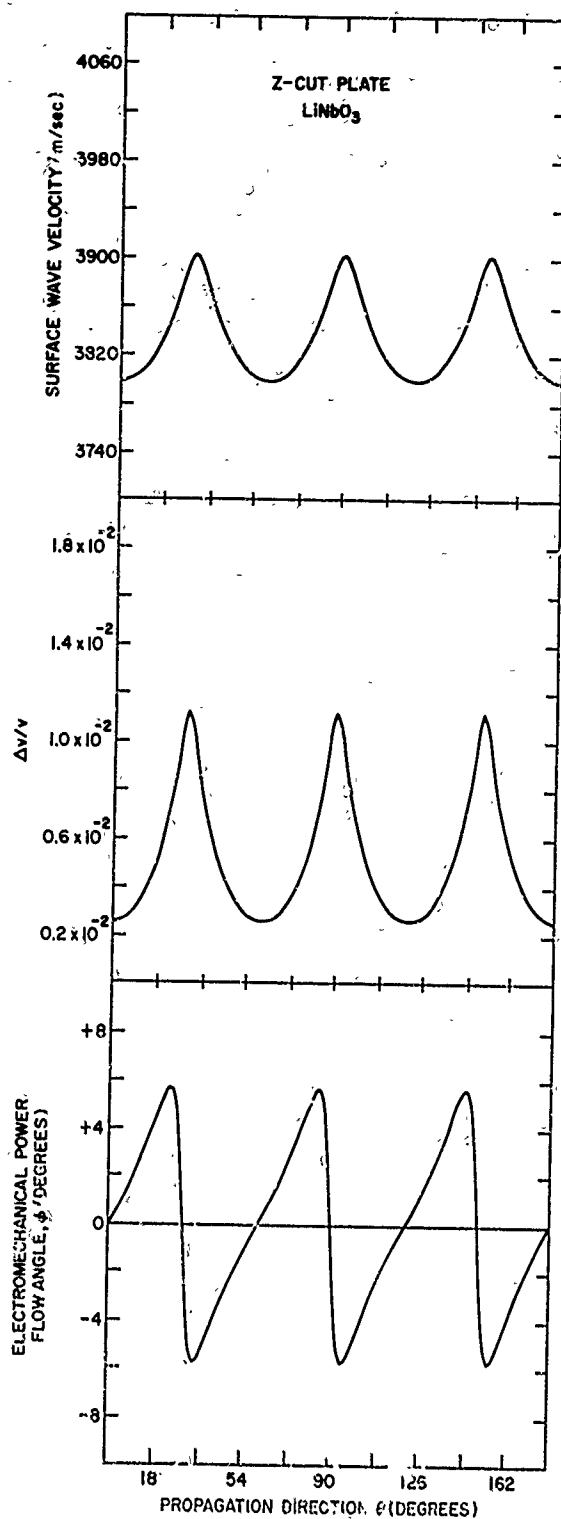


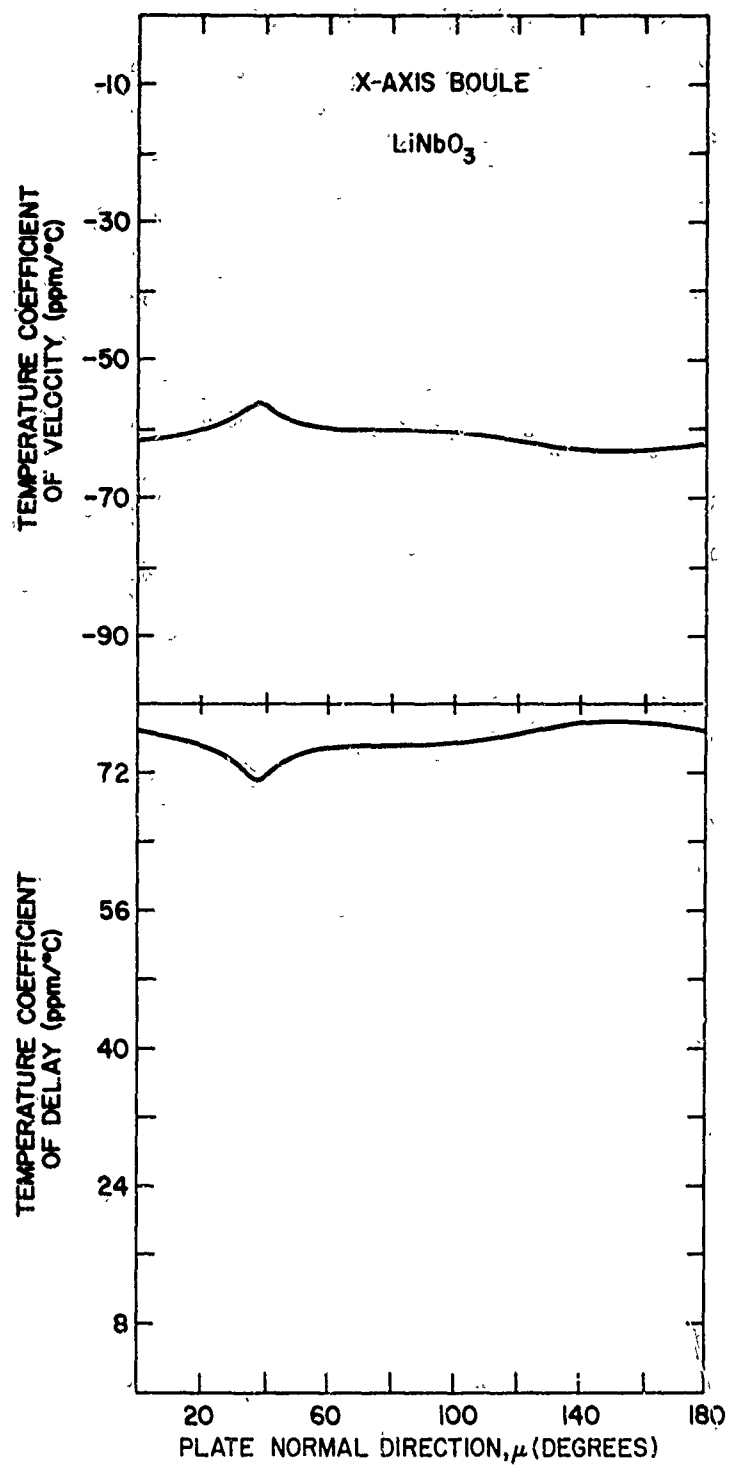




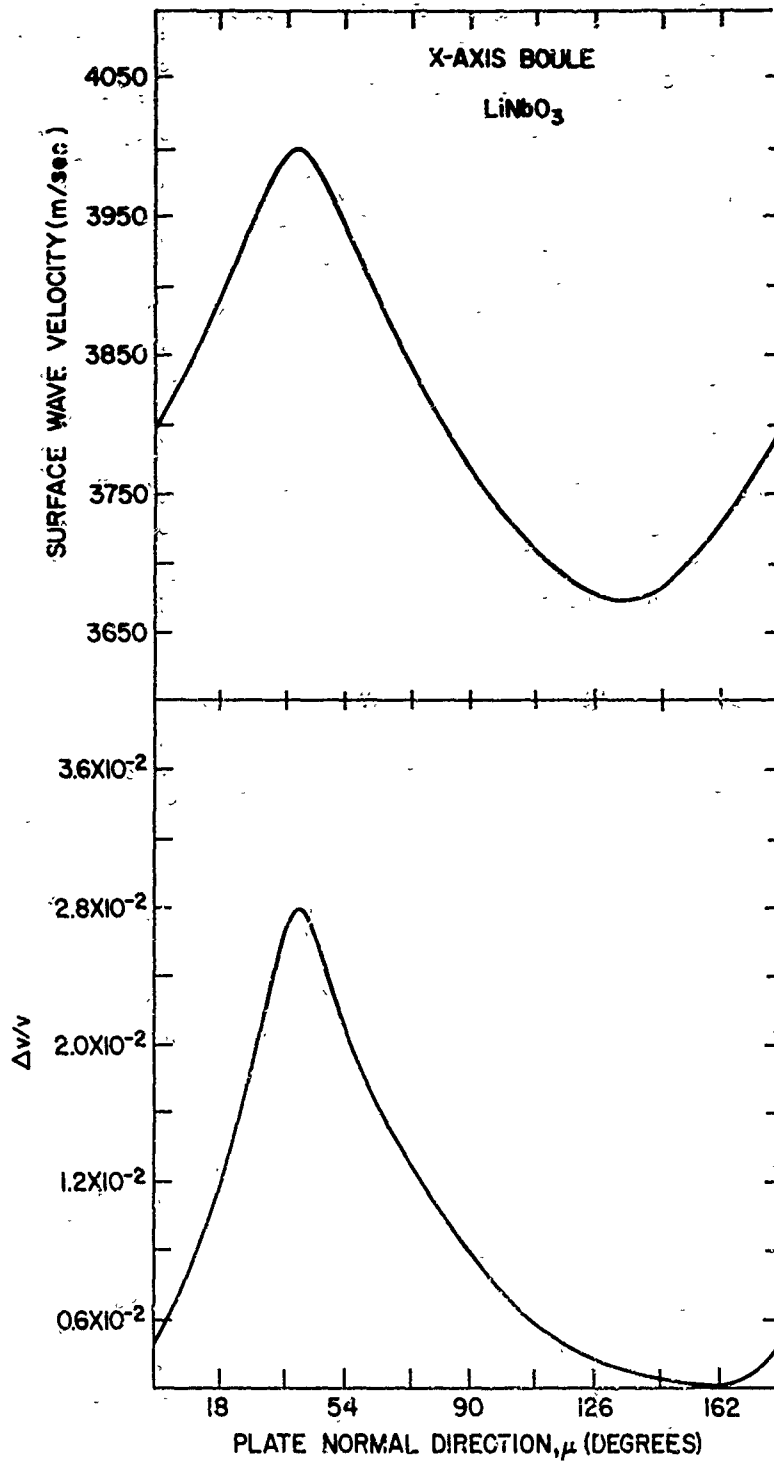




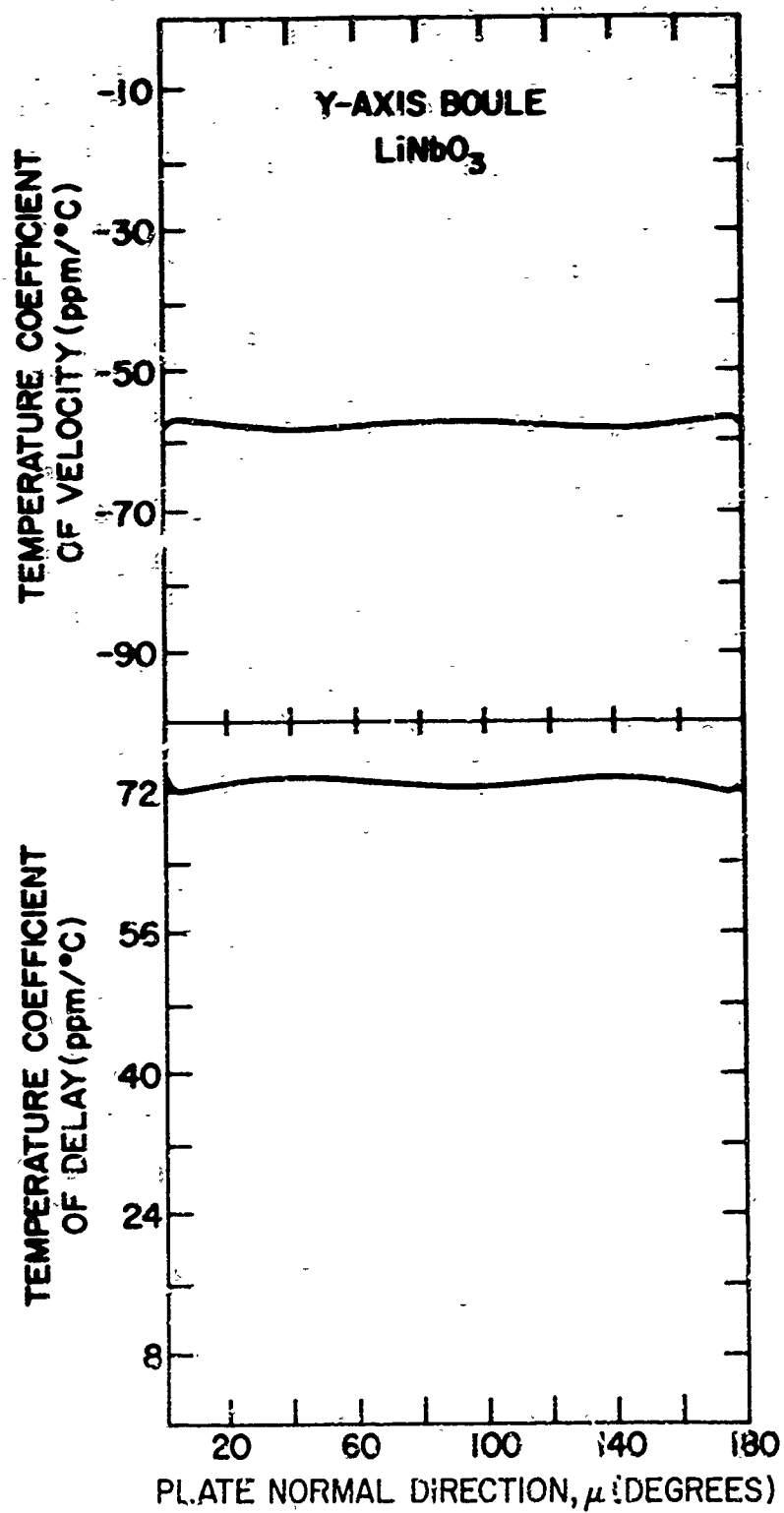


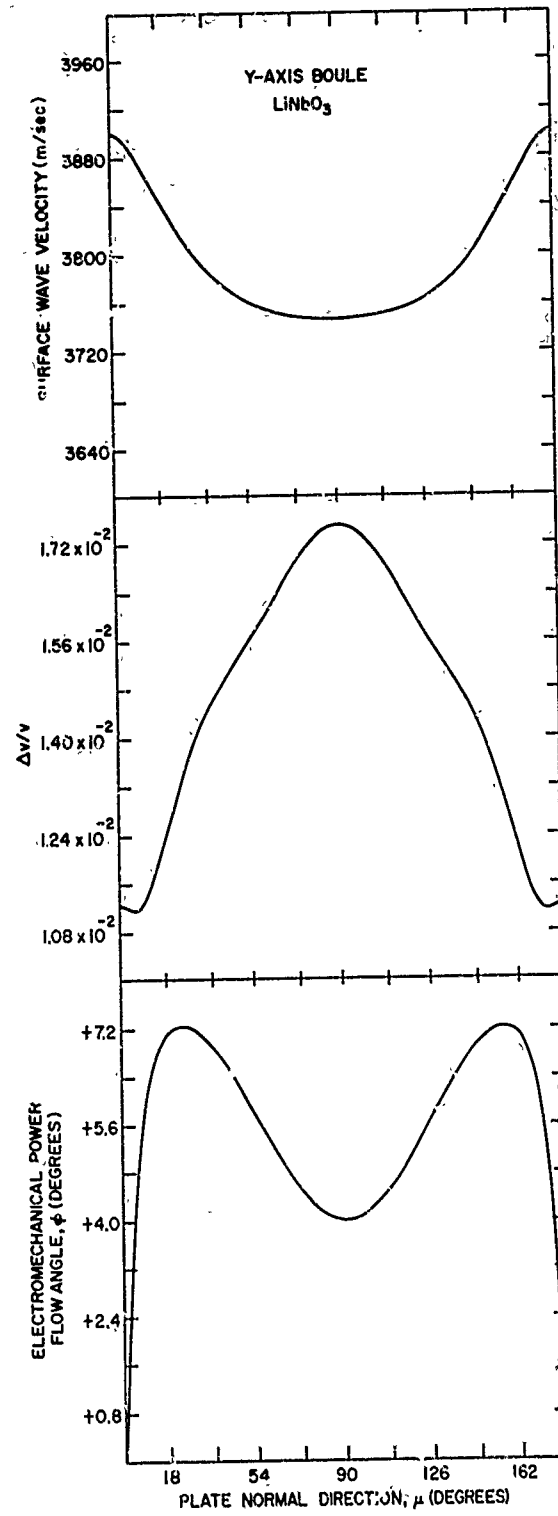


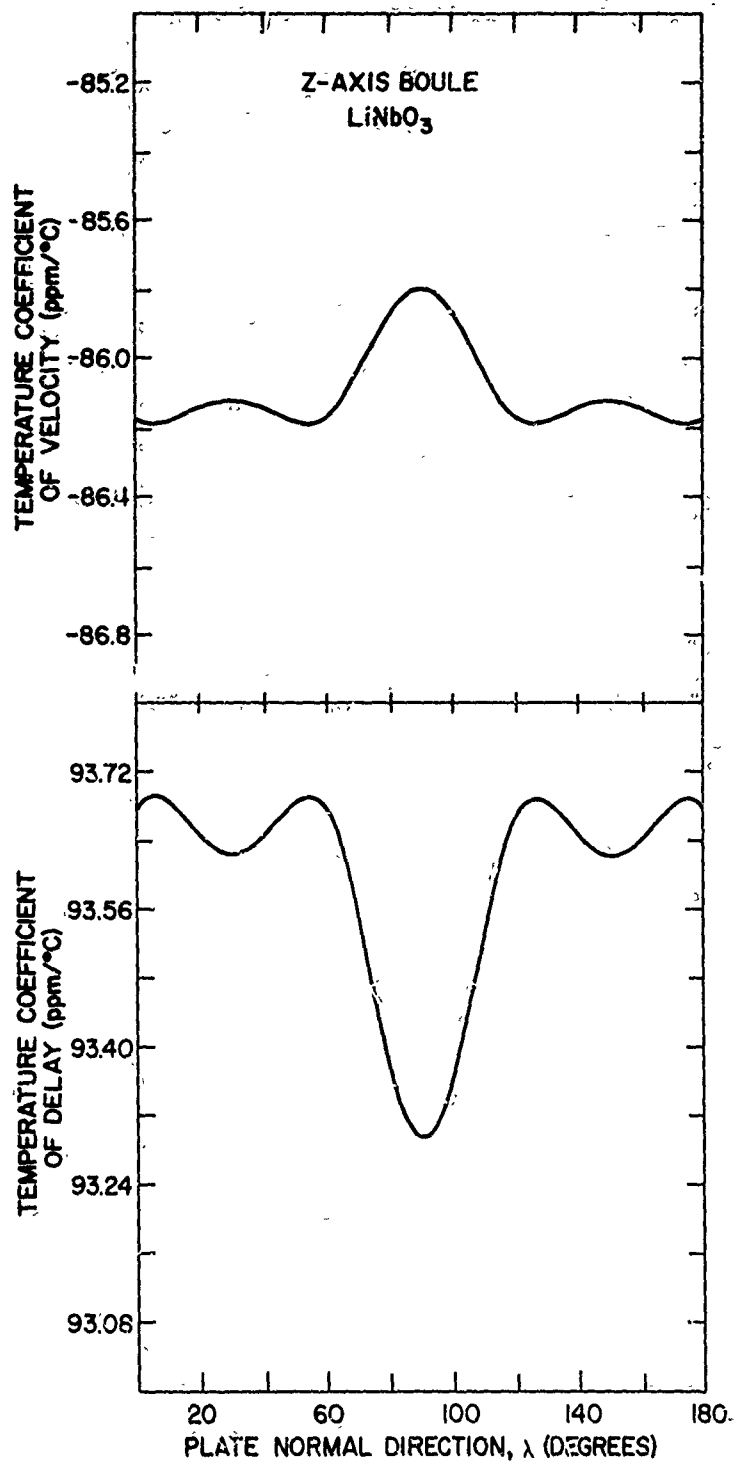


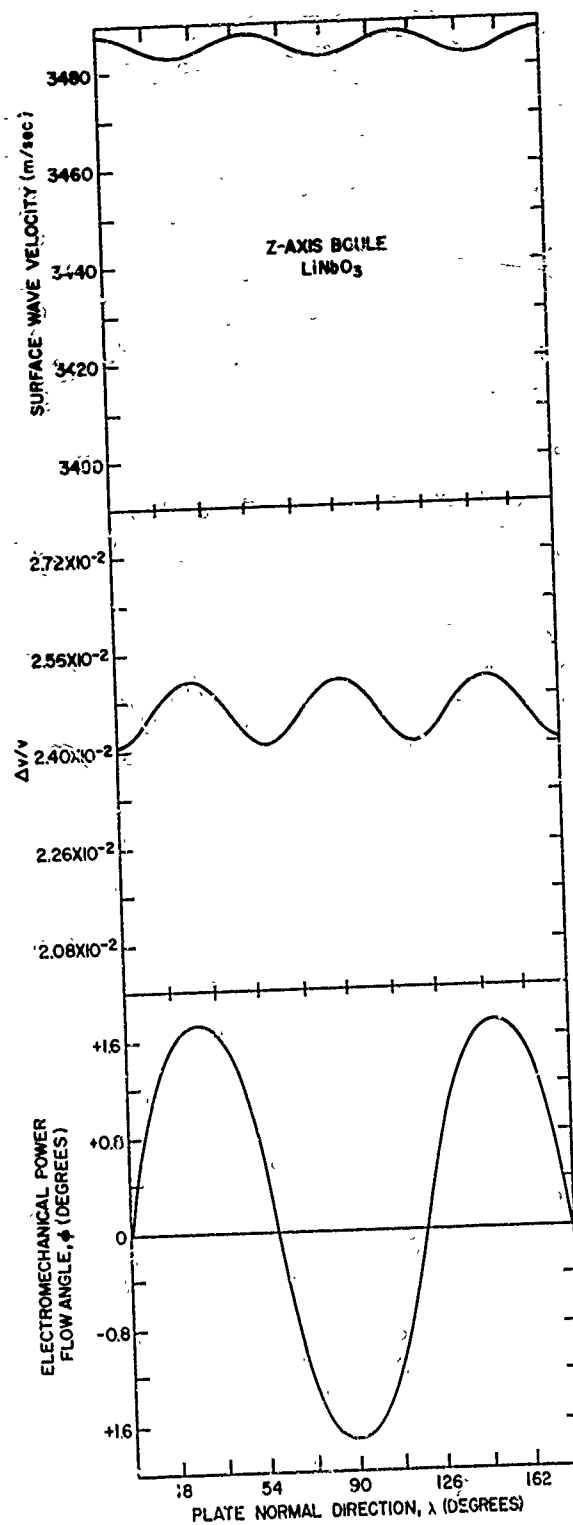


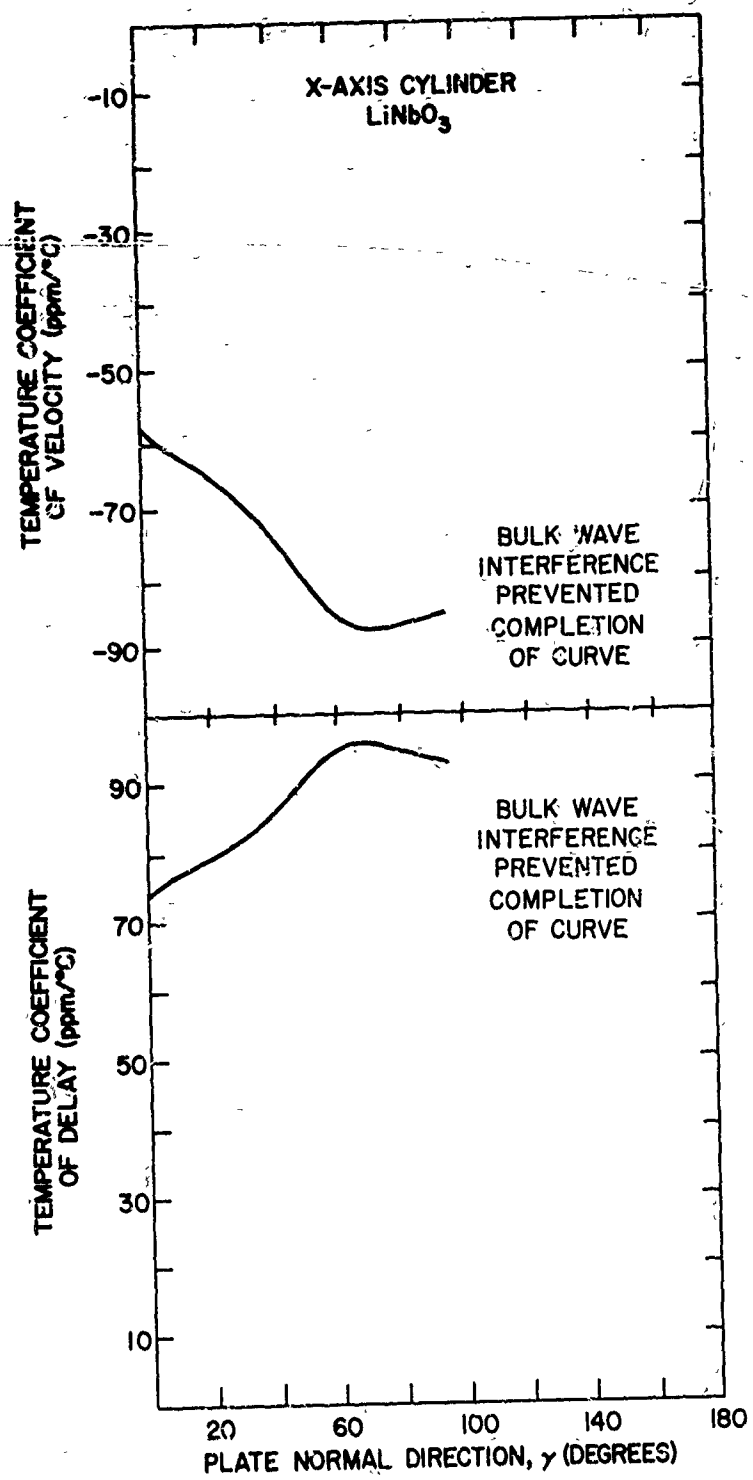
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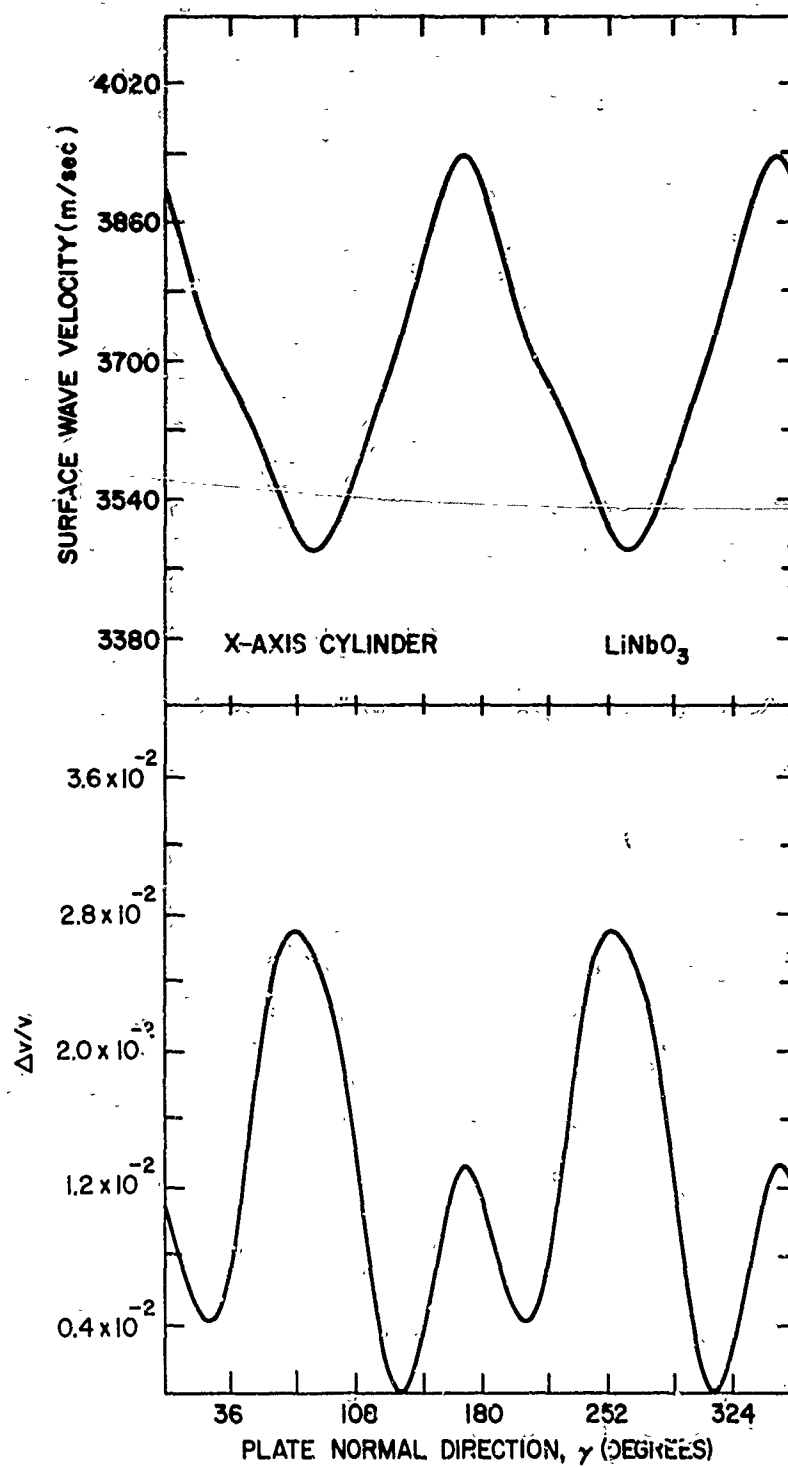




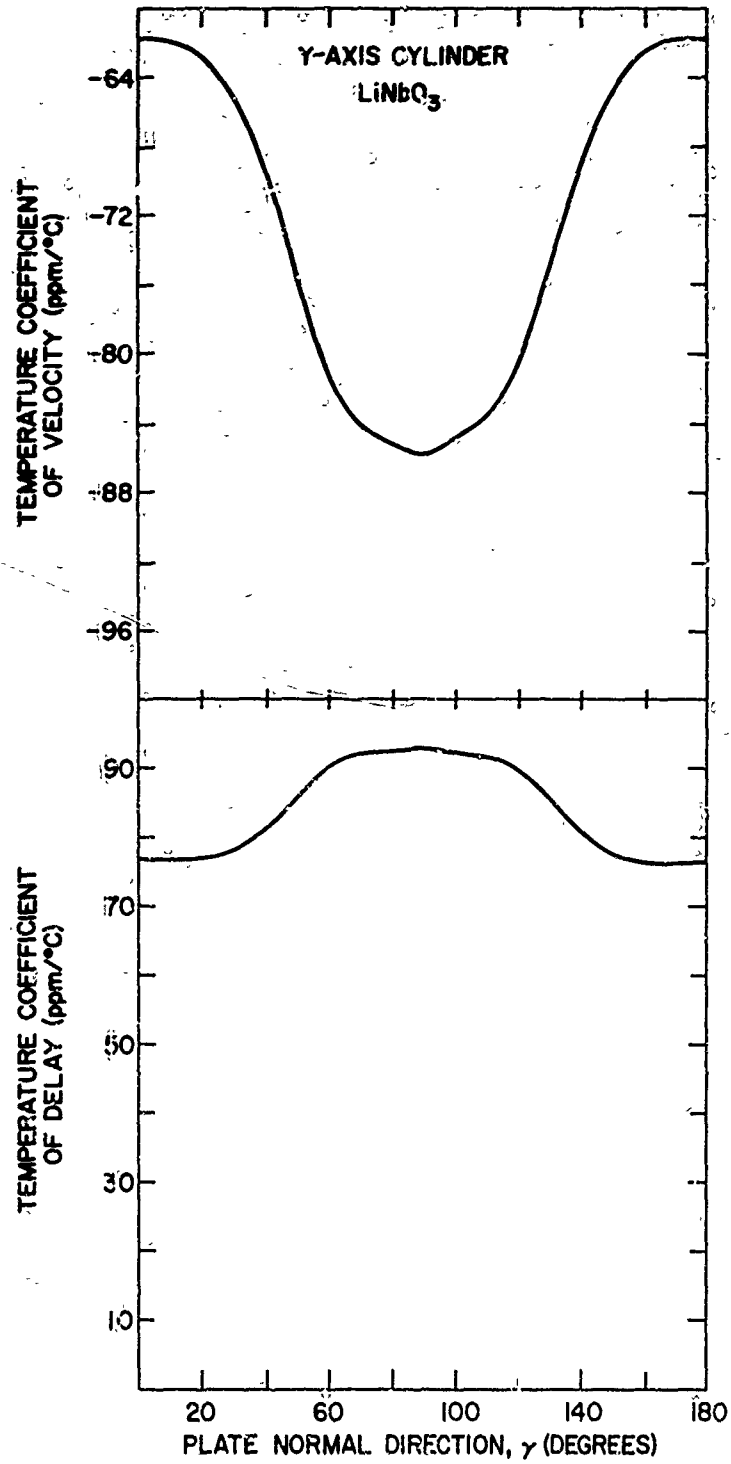




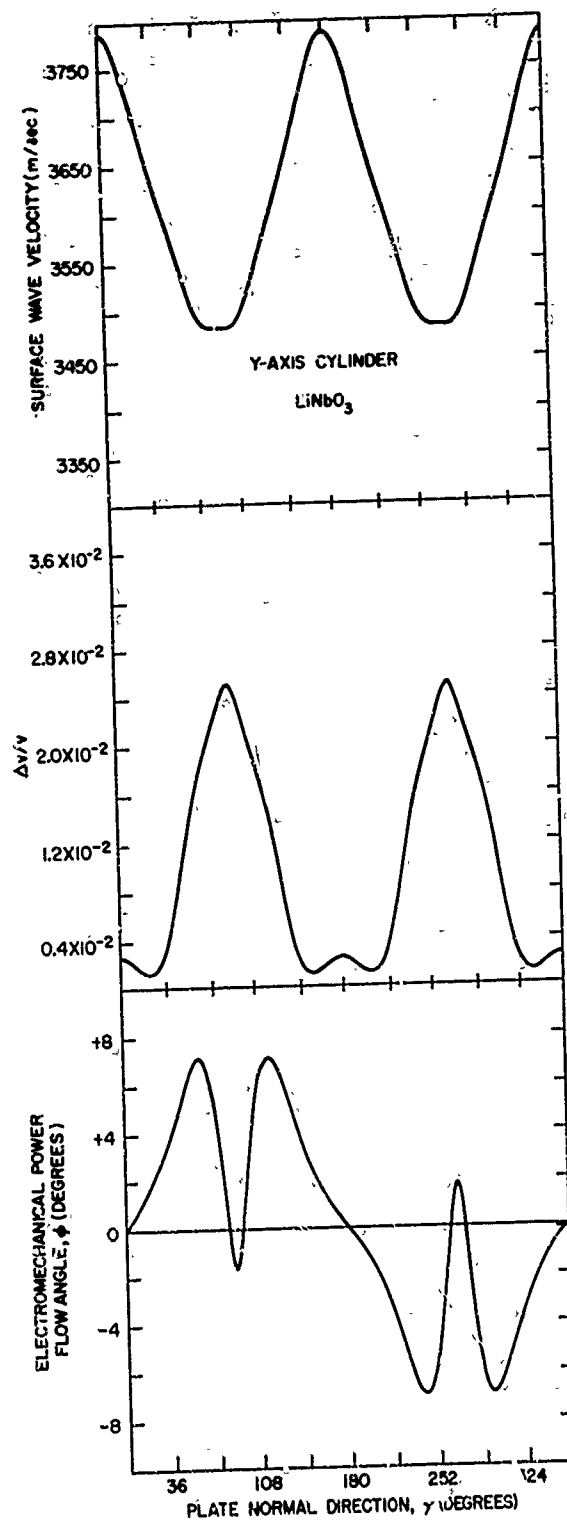


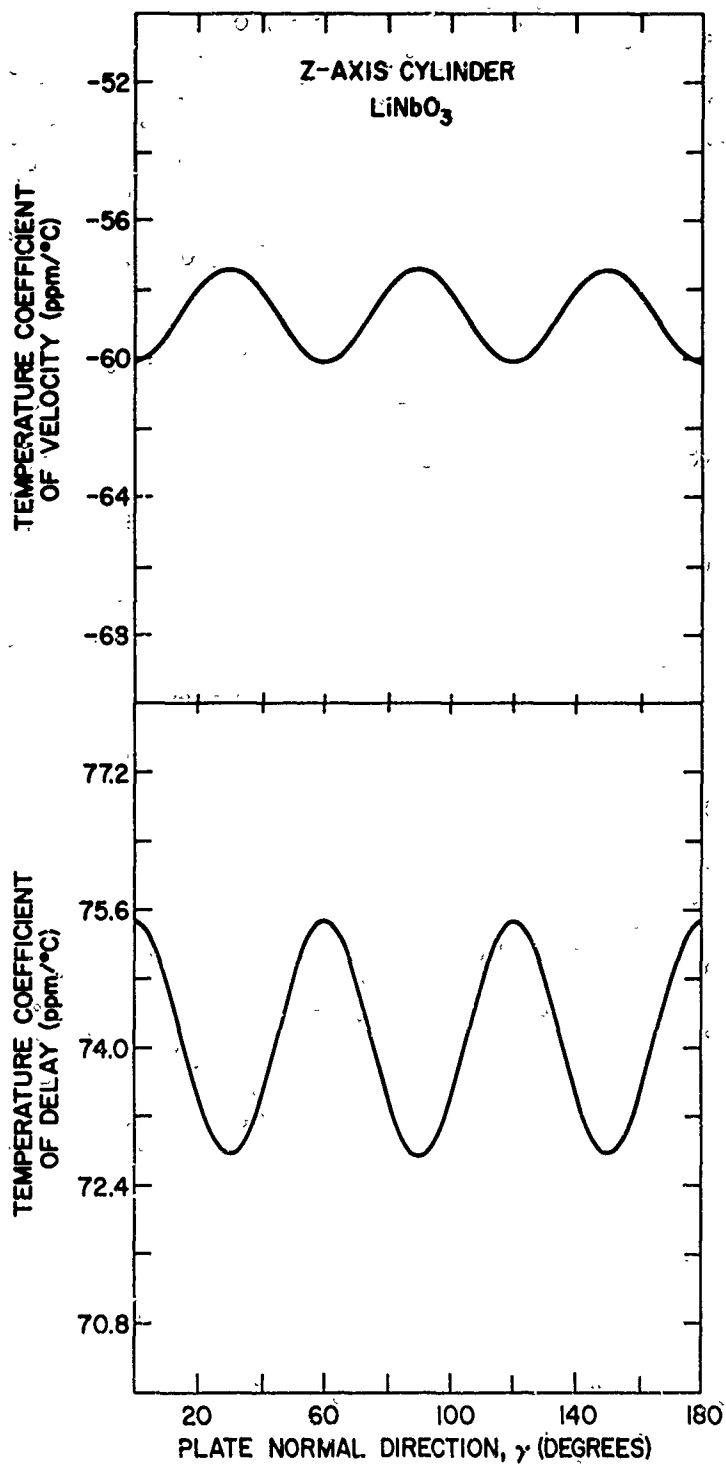


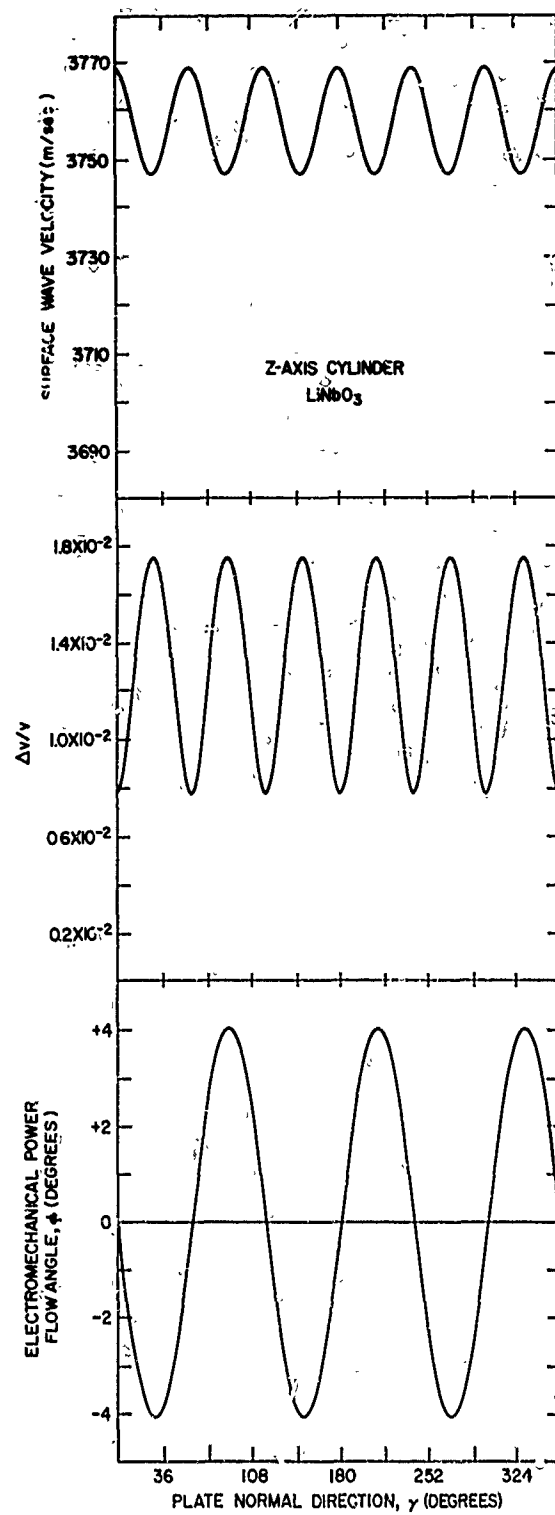
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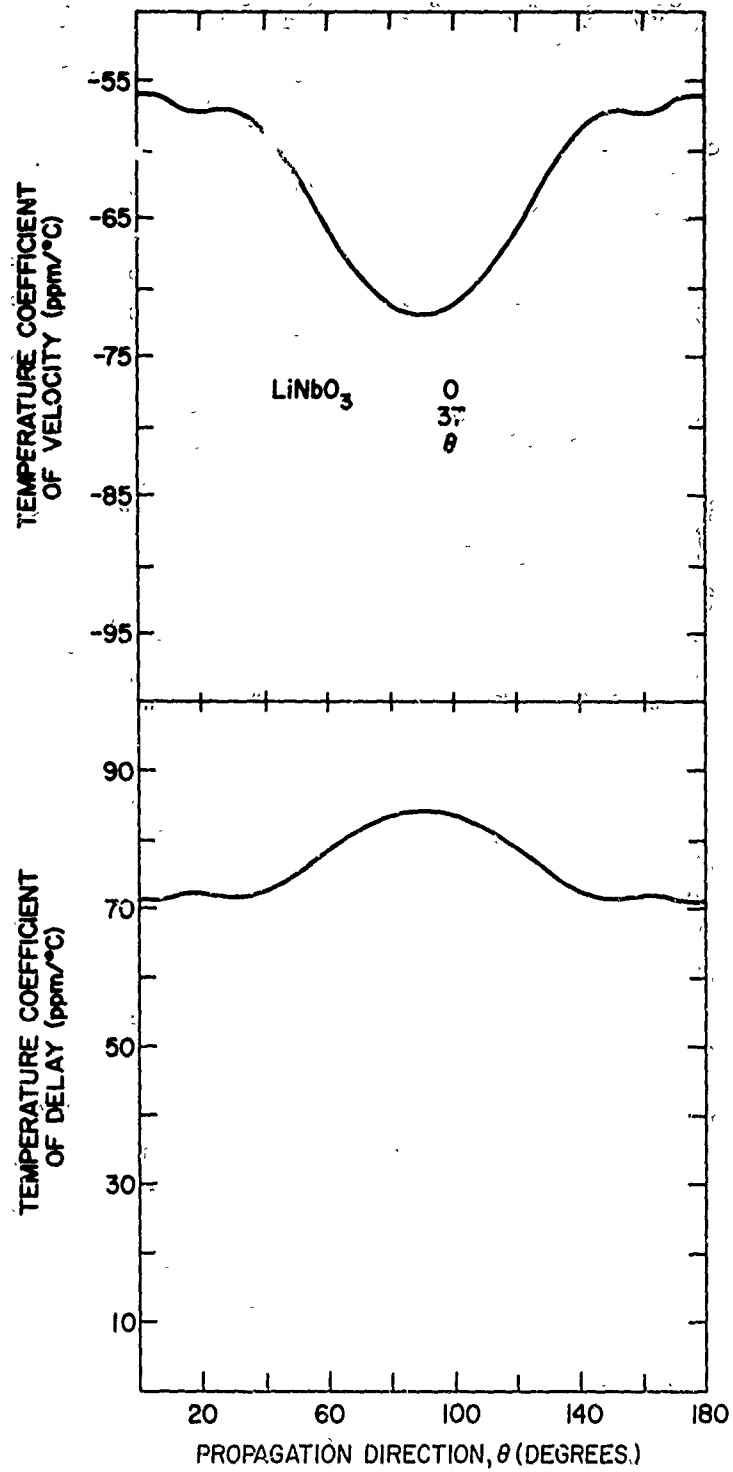


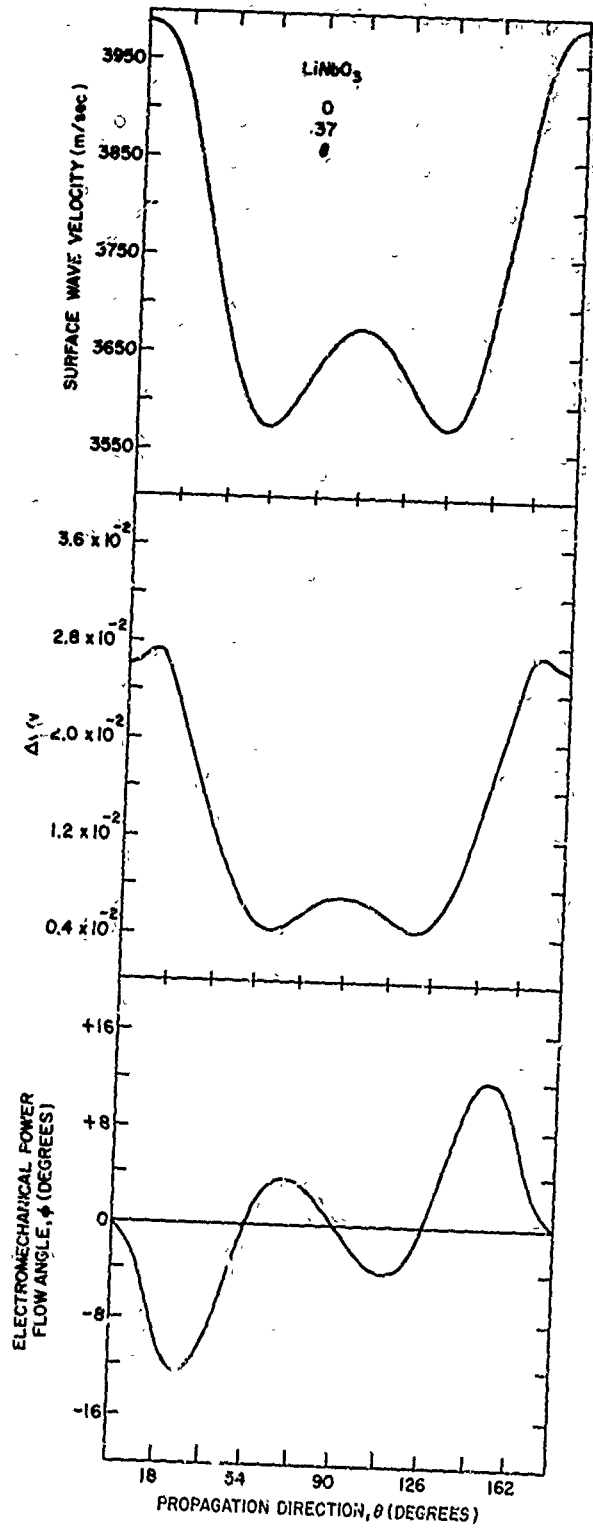


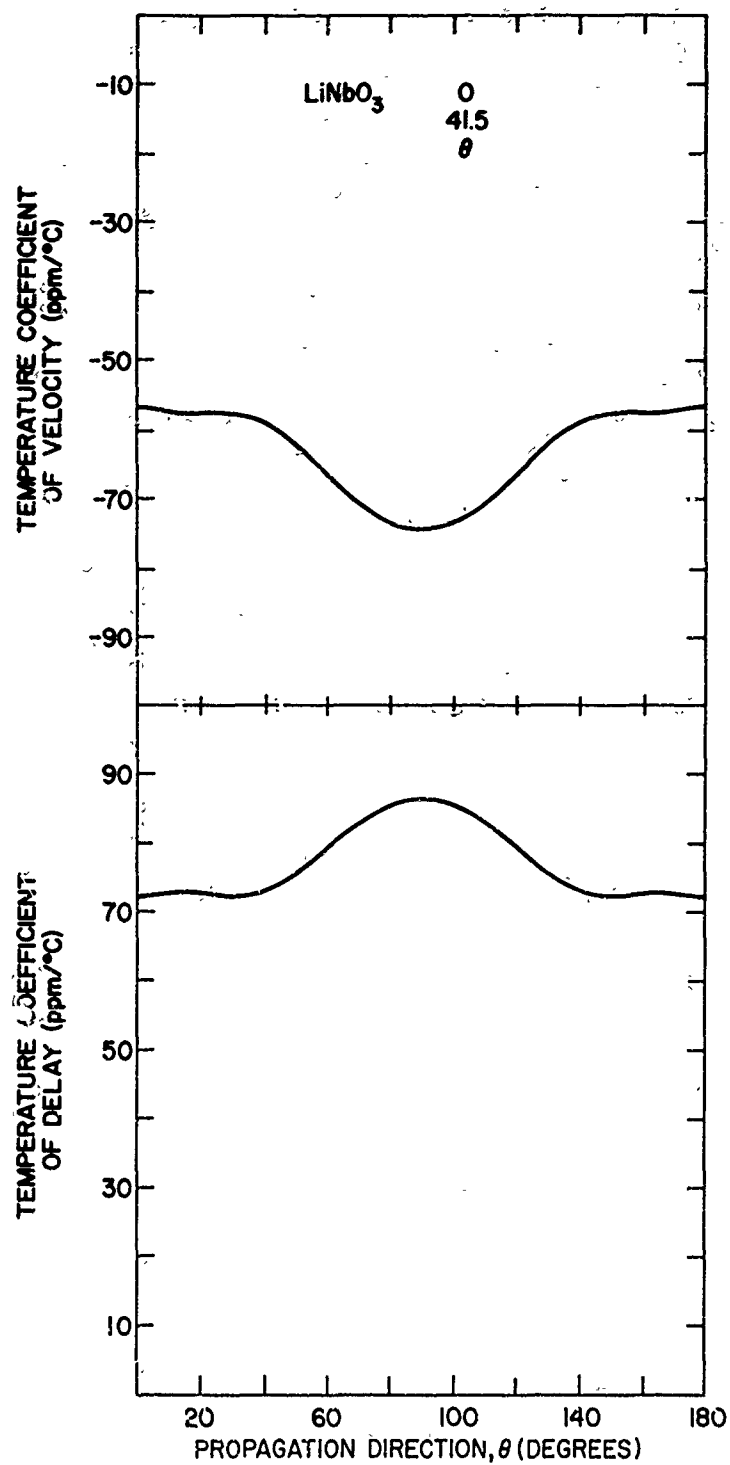


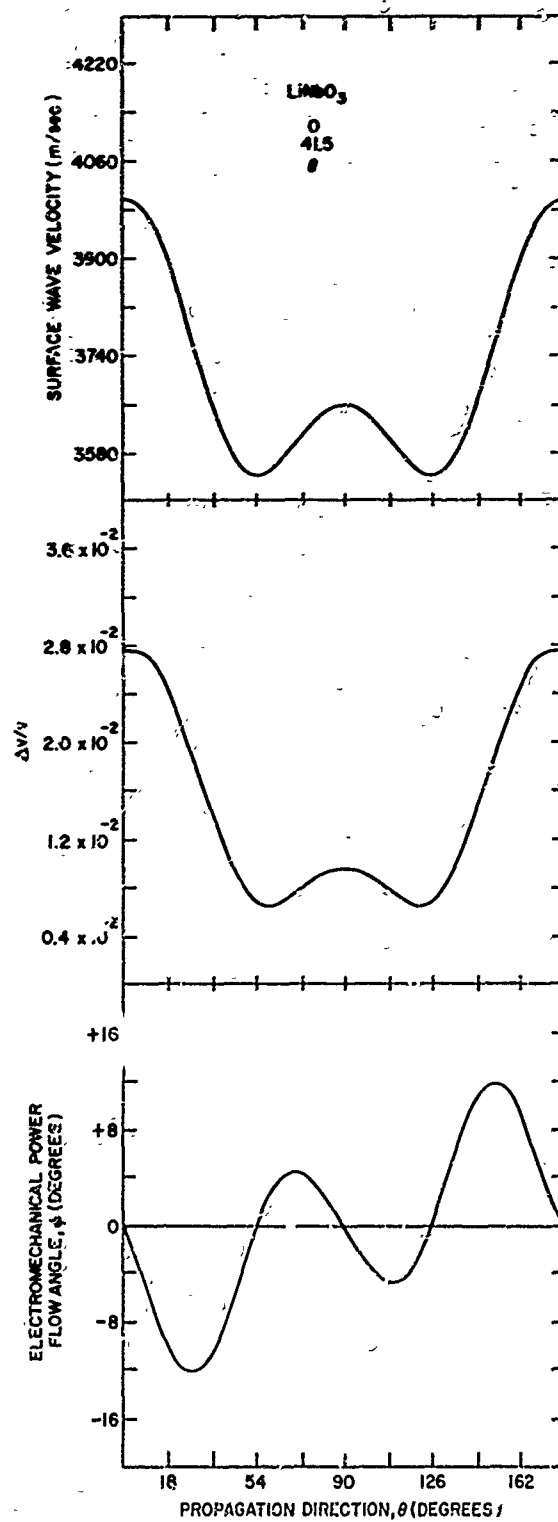


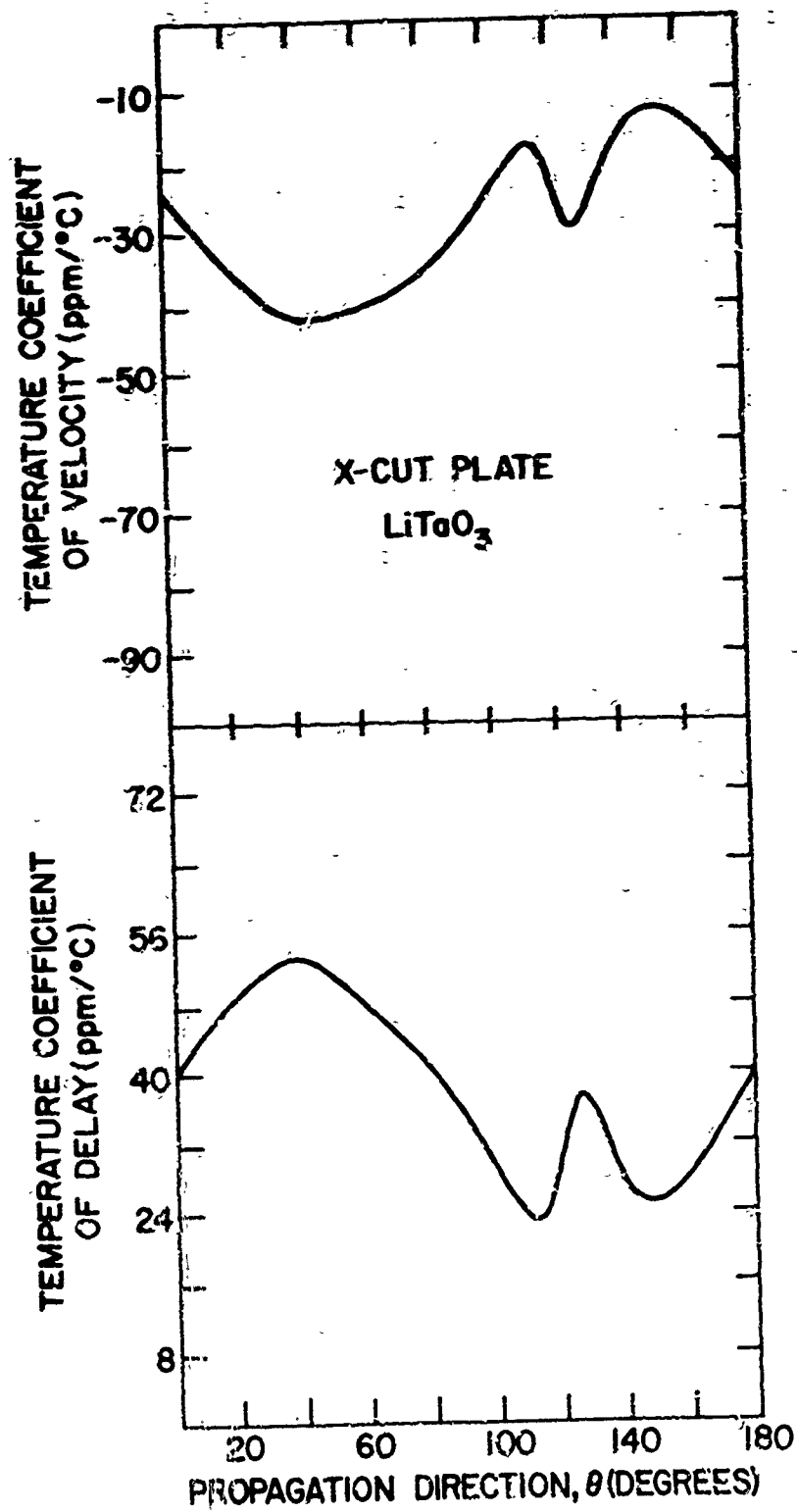




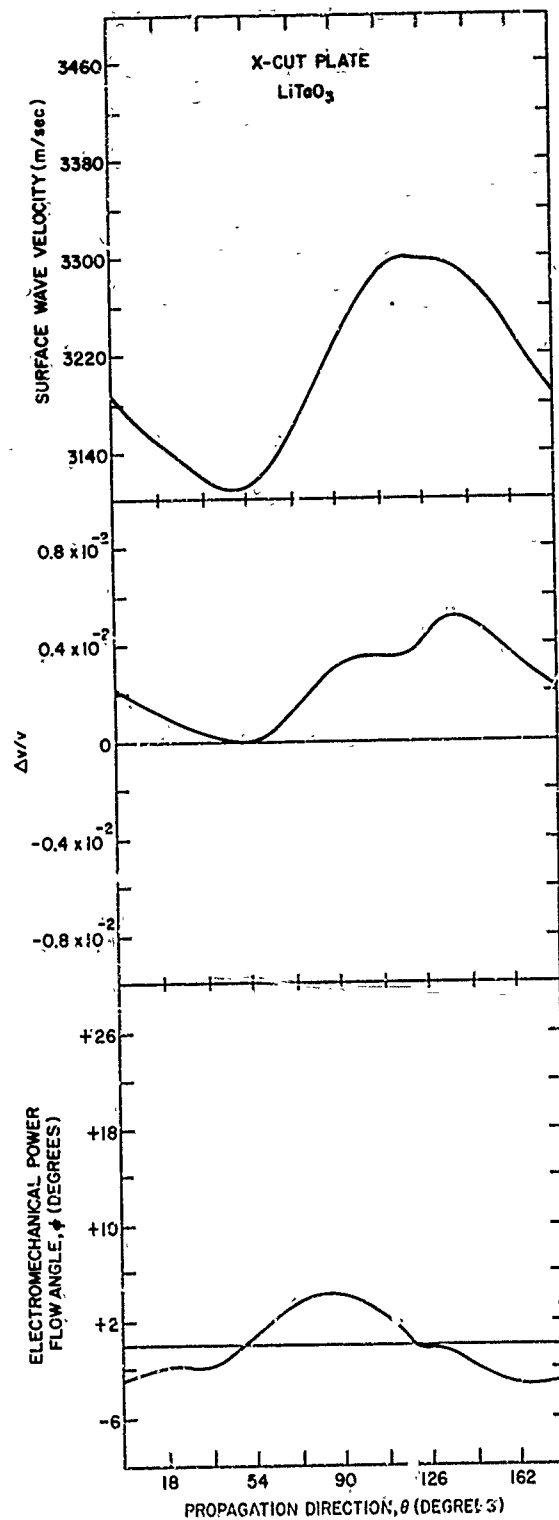


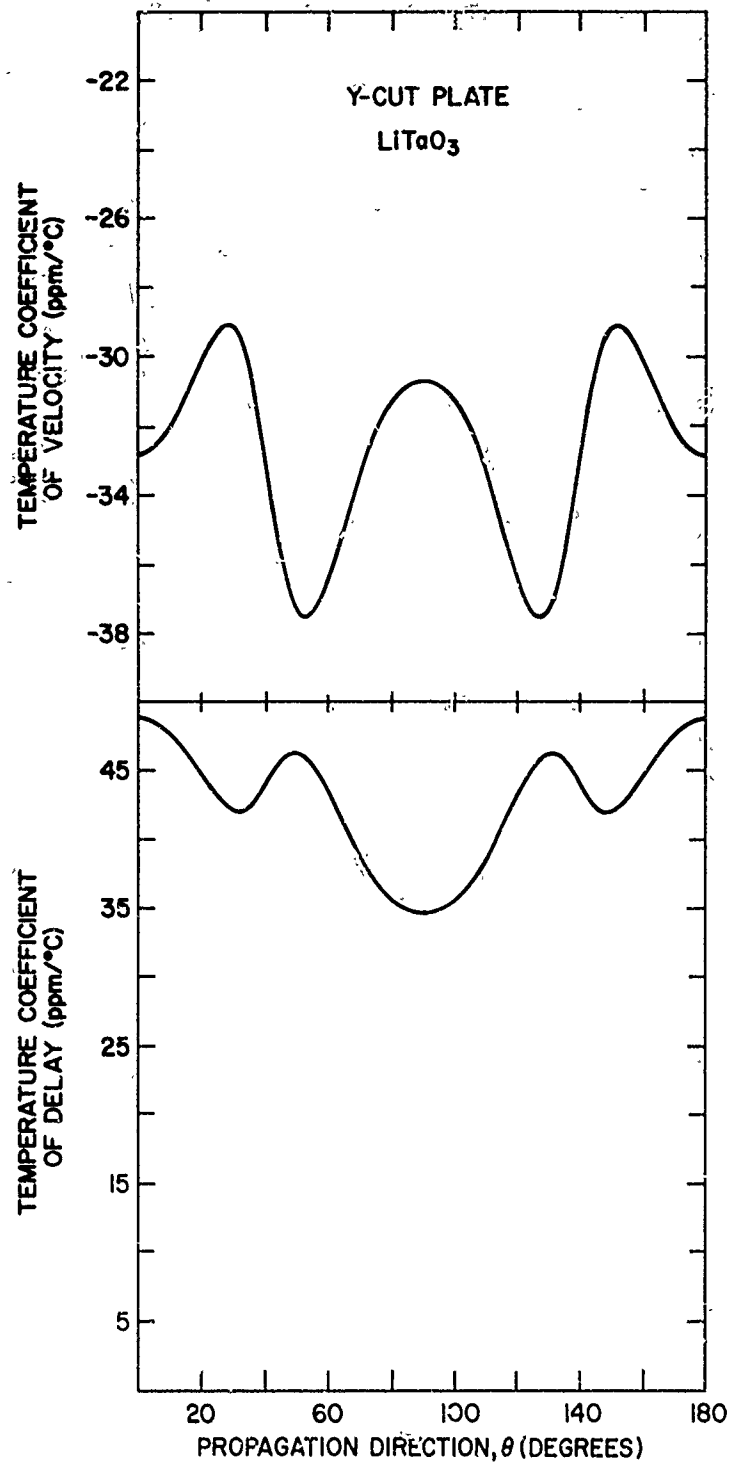


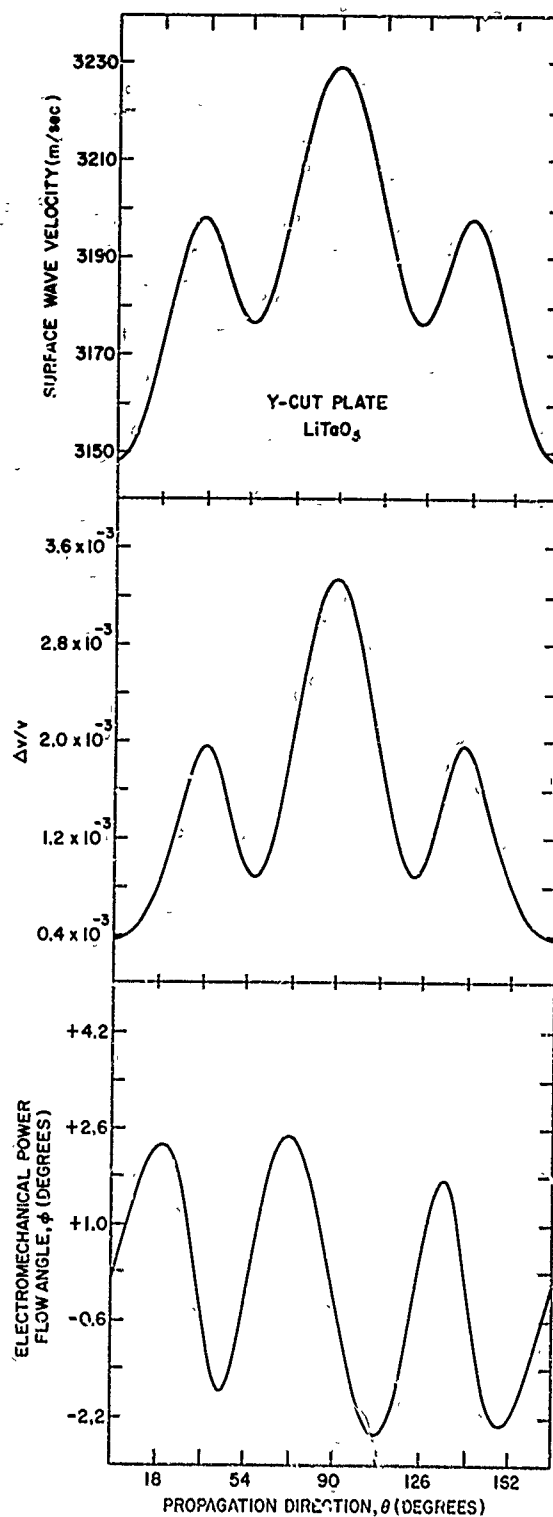


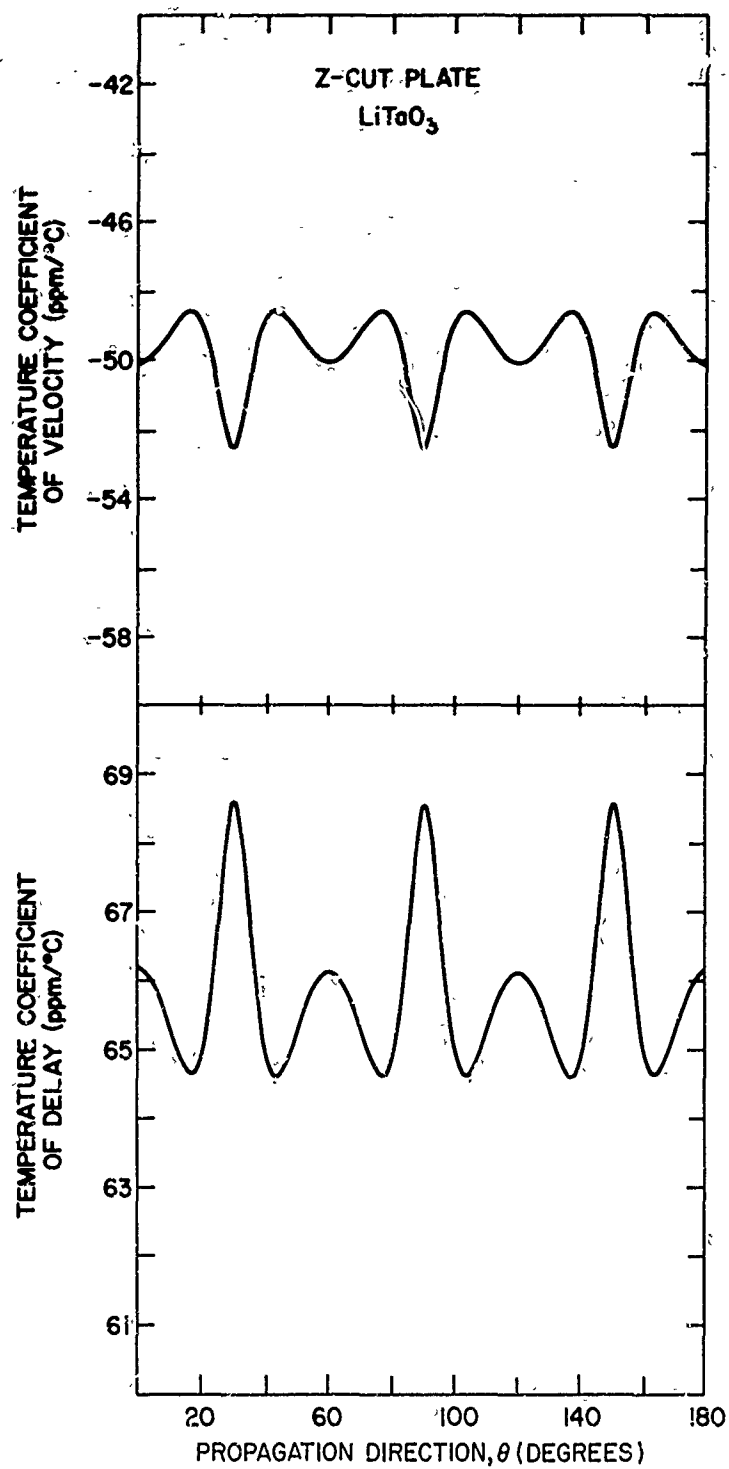


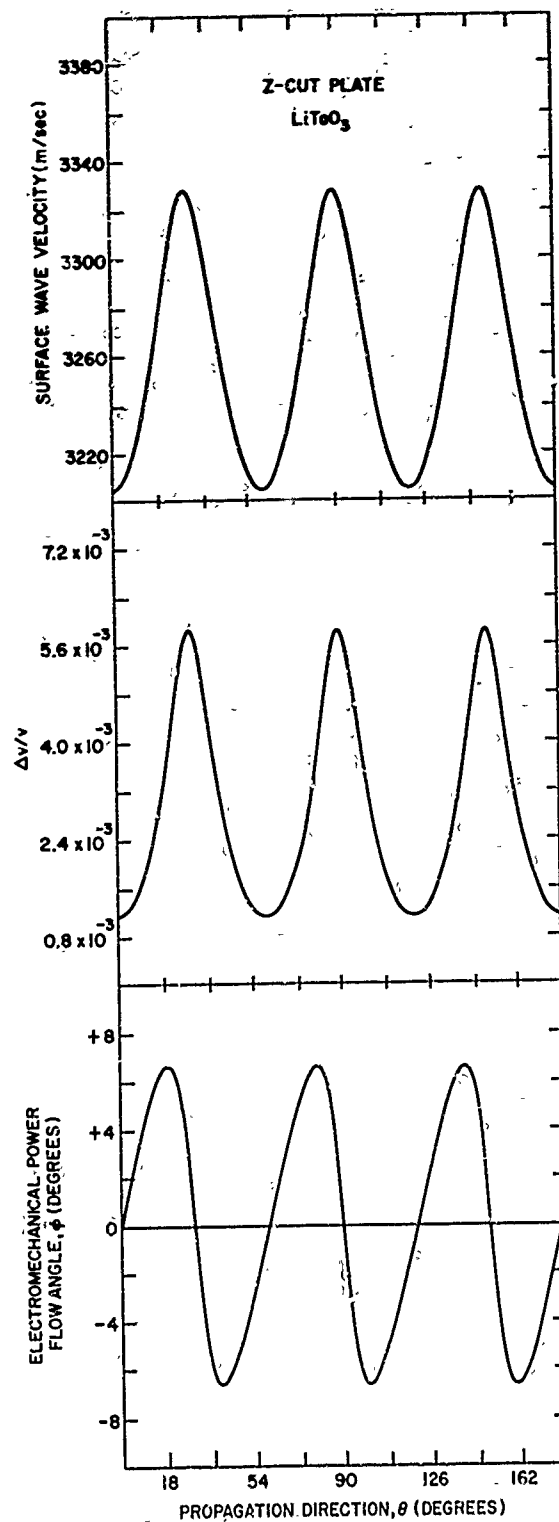


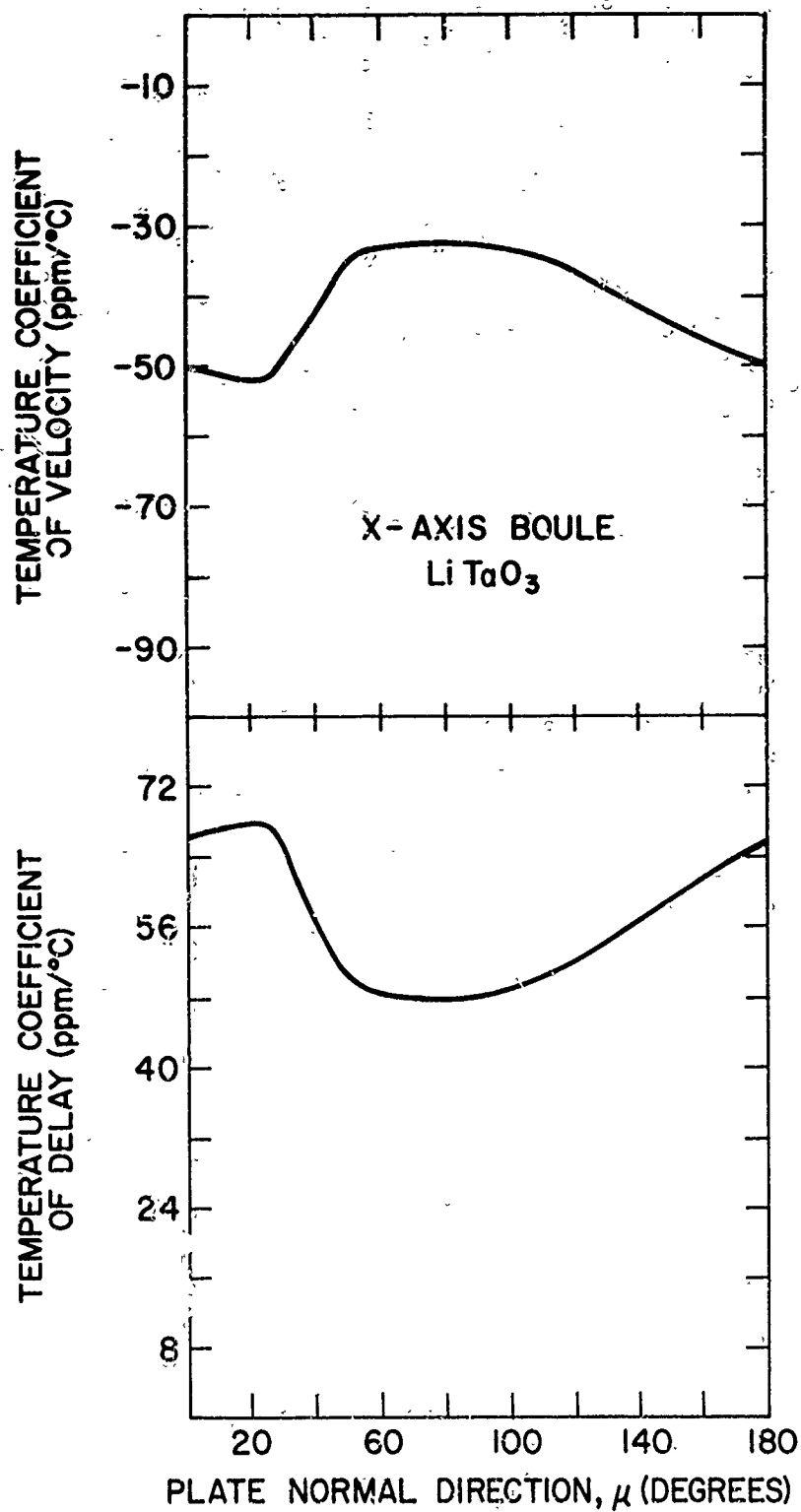


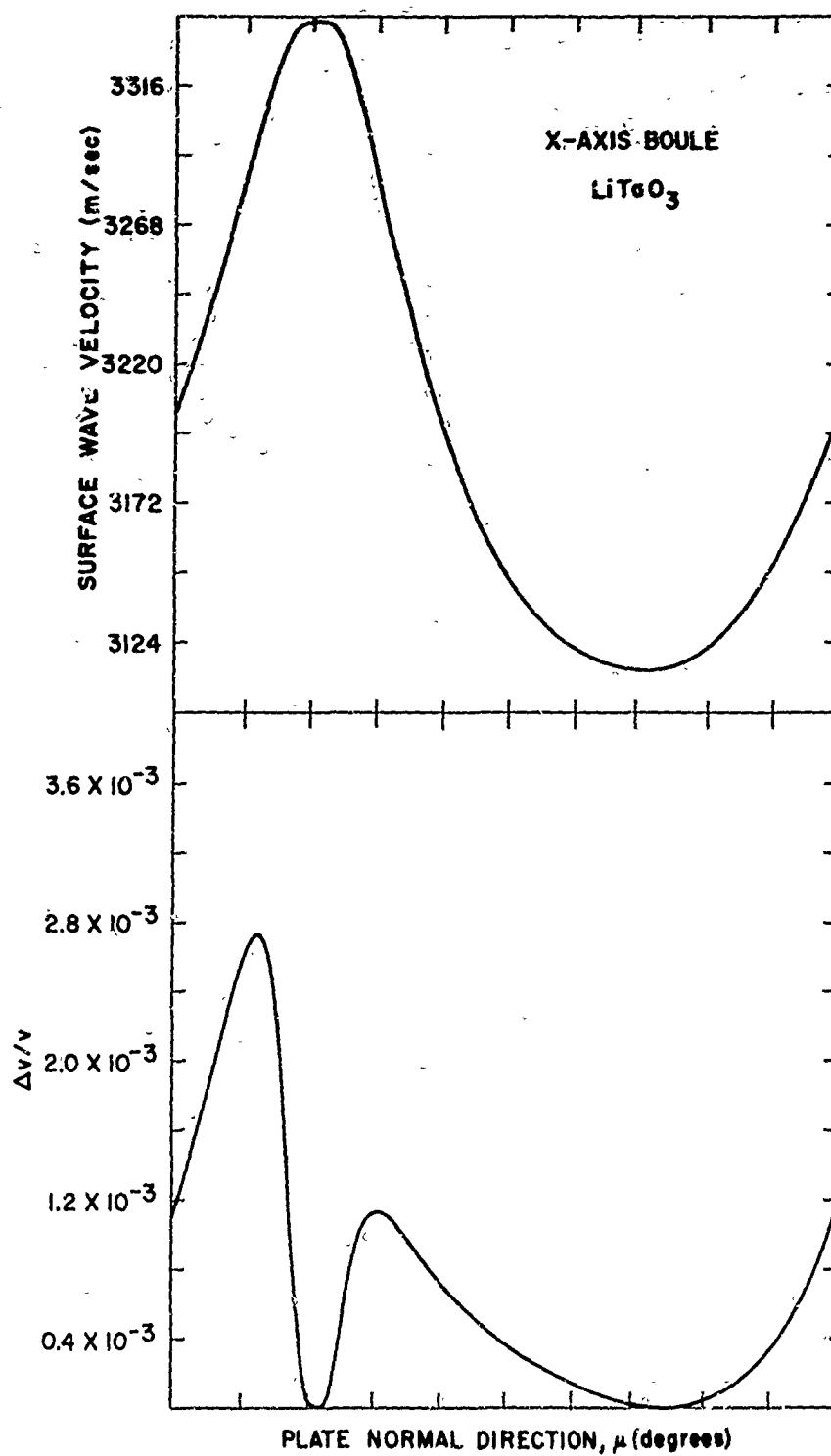




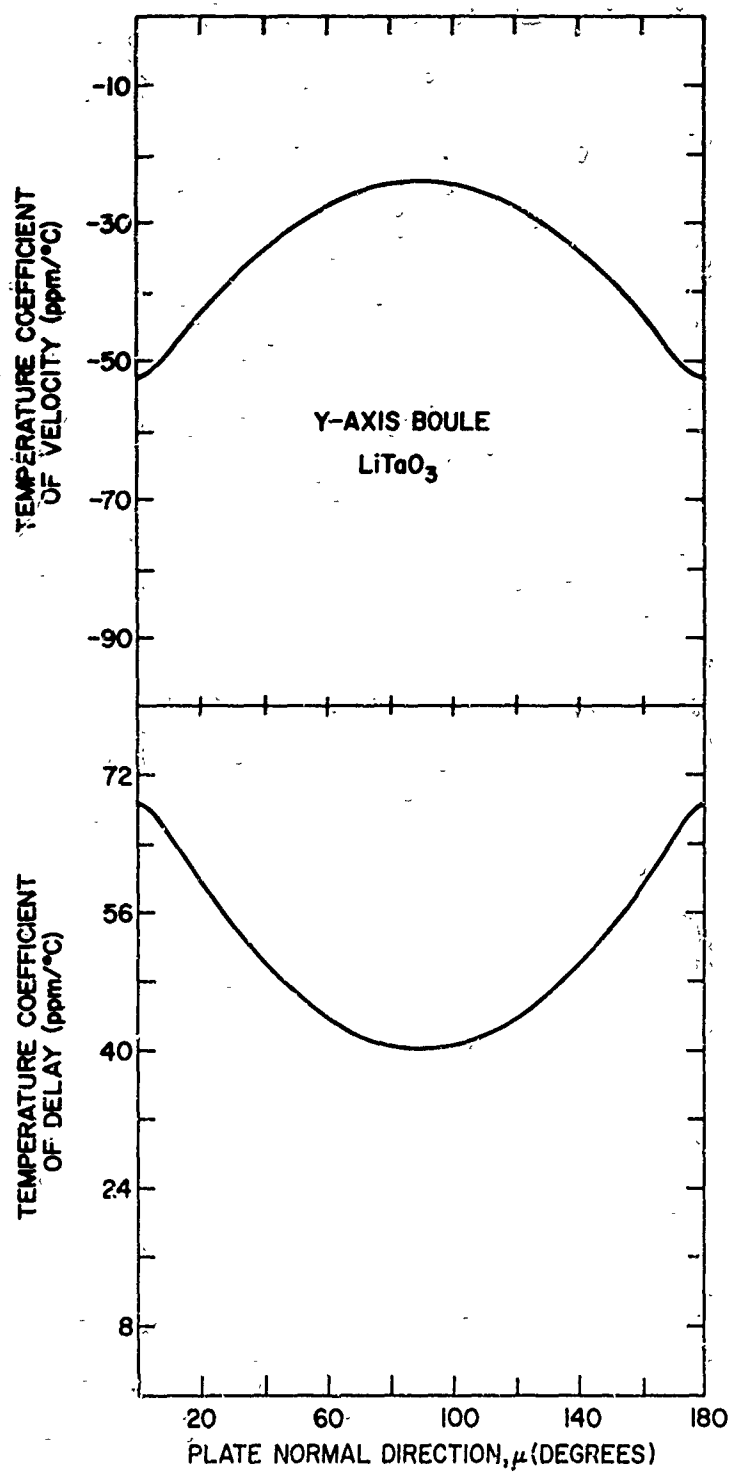




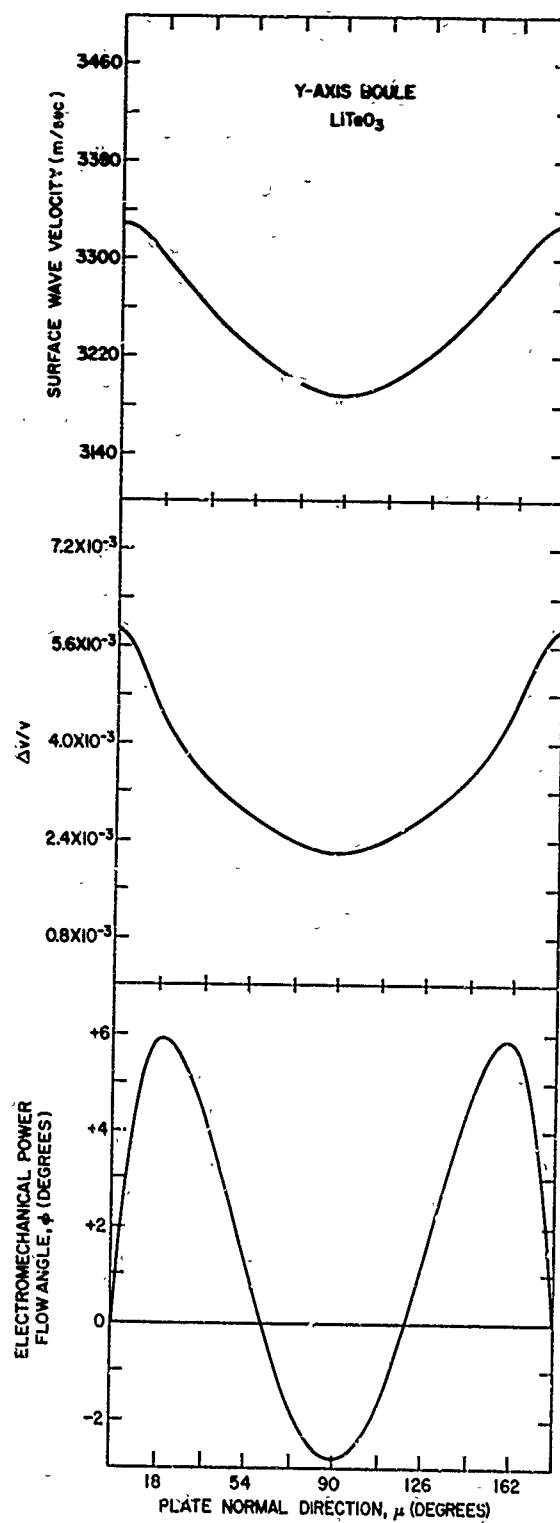


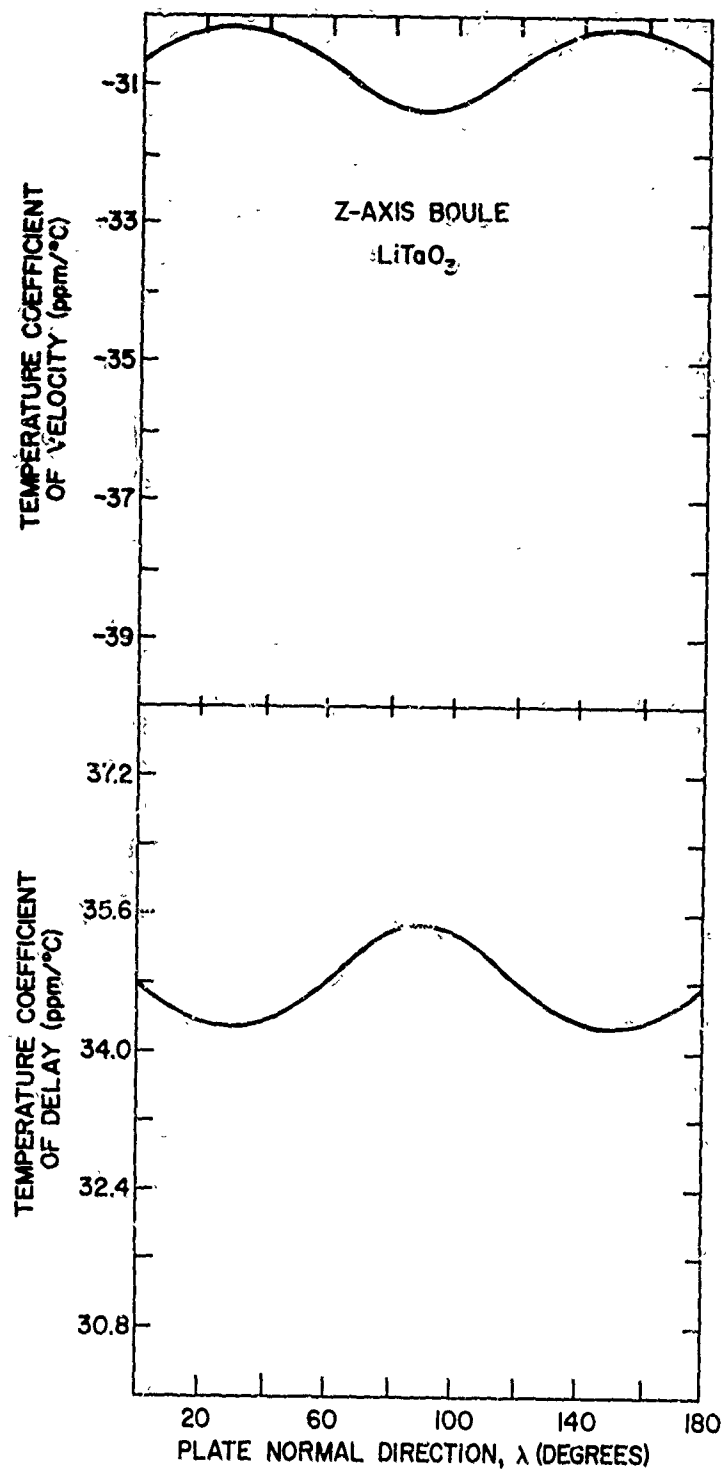


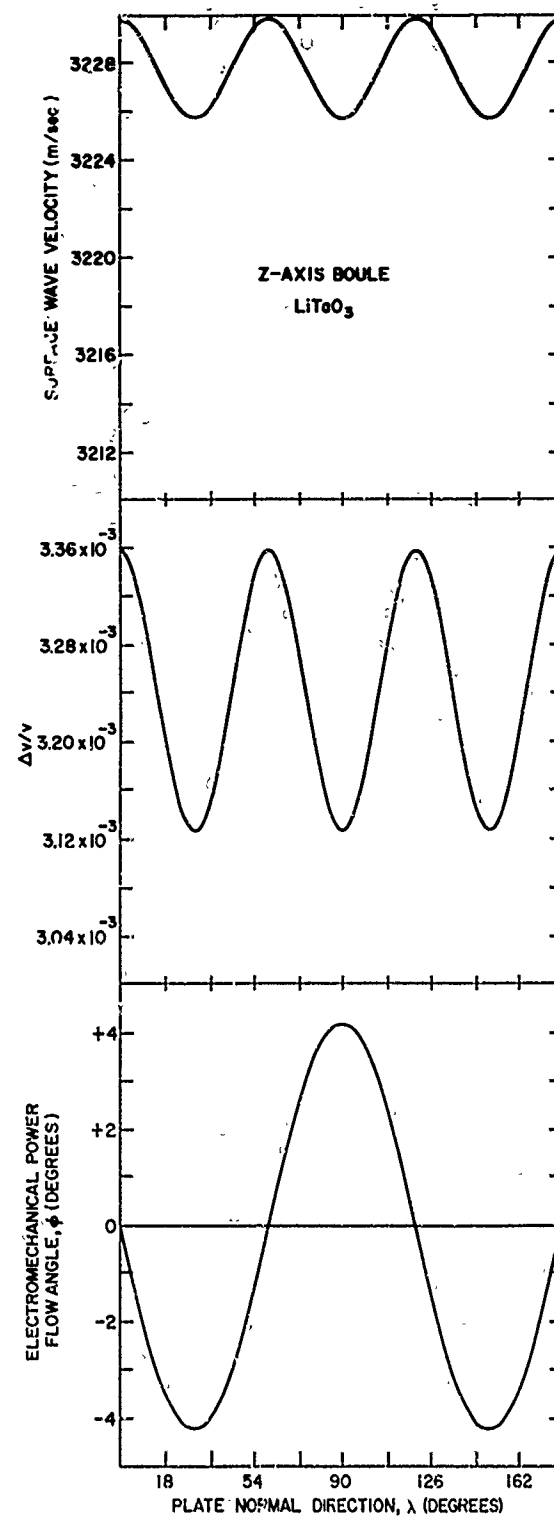
NOTE: TIME AVERAGE POWER FLOW  
ANGLE IDENTICALLY ZERO.

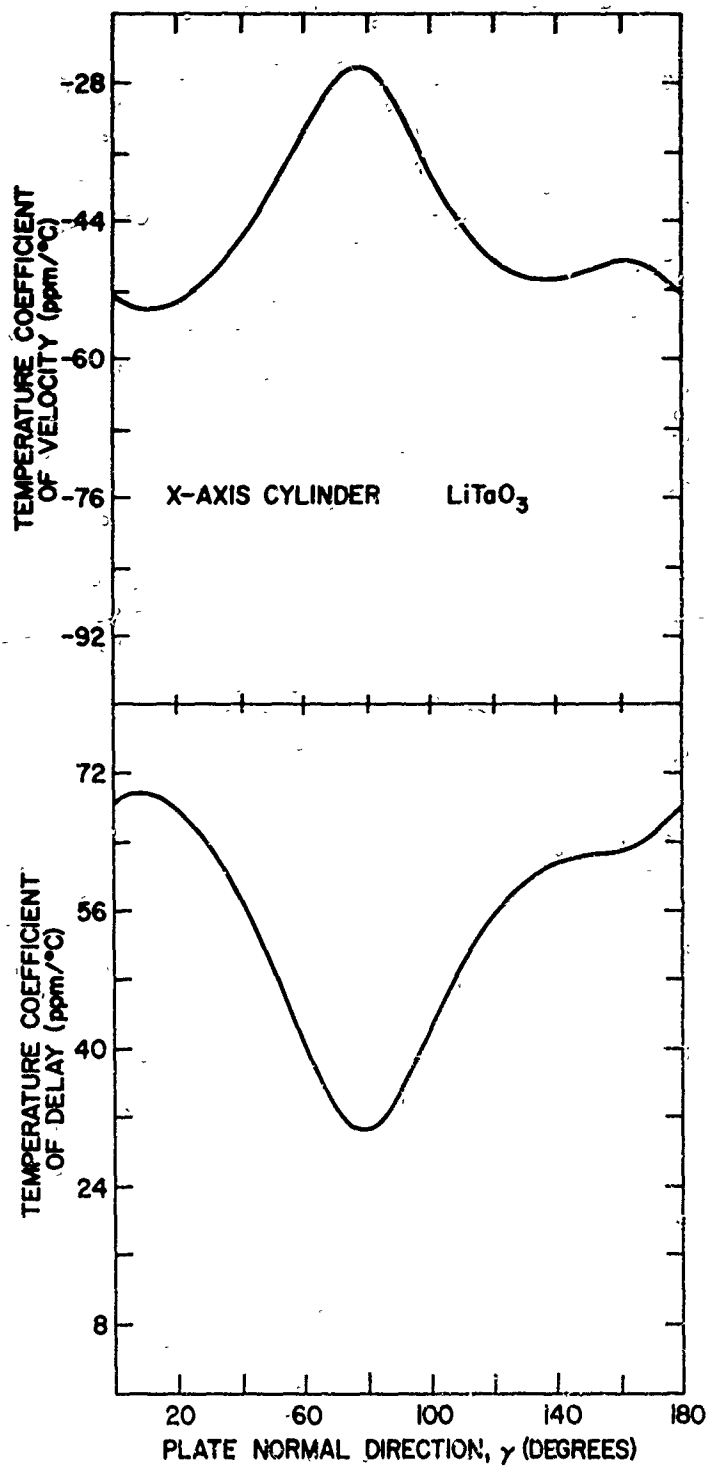


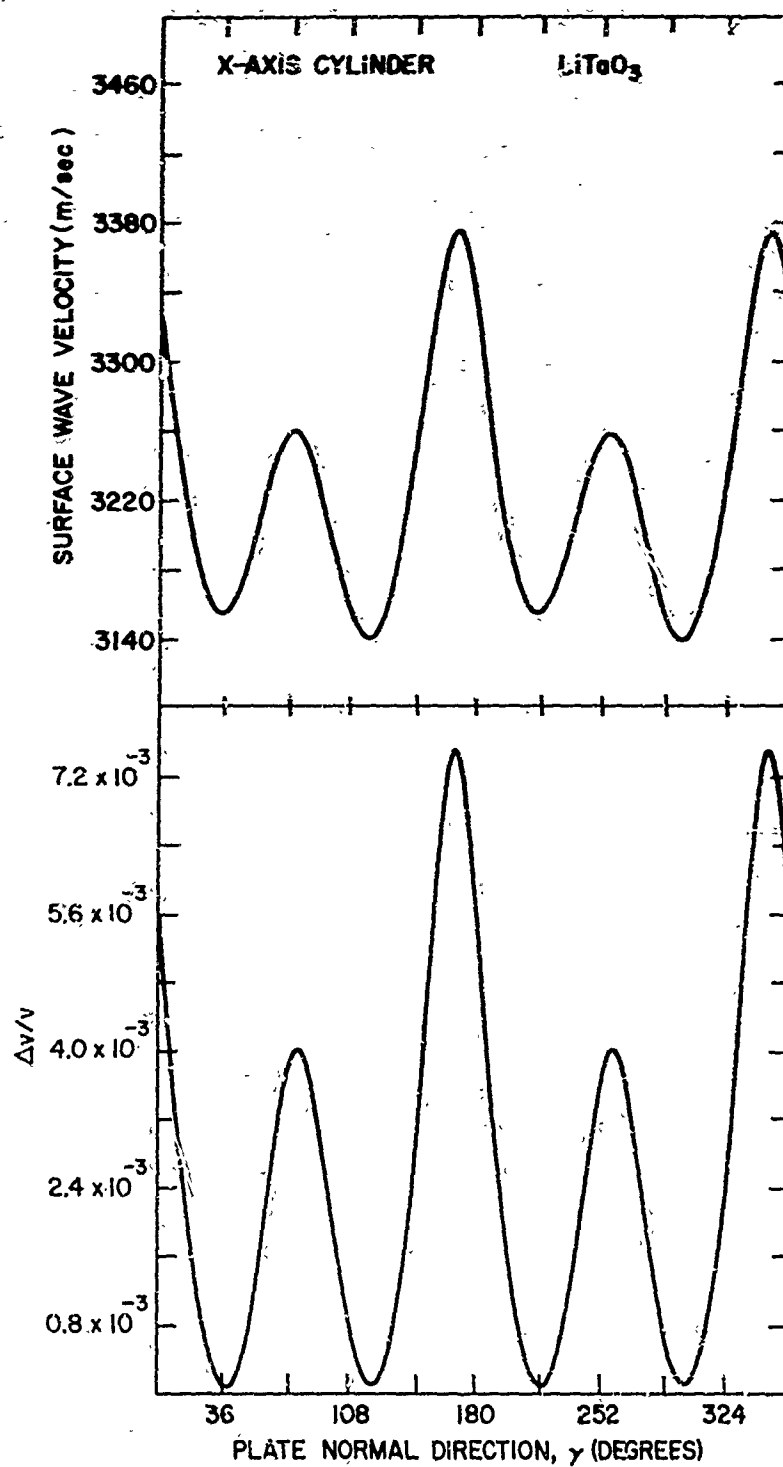




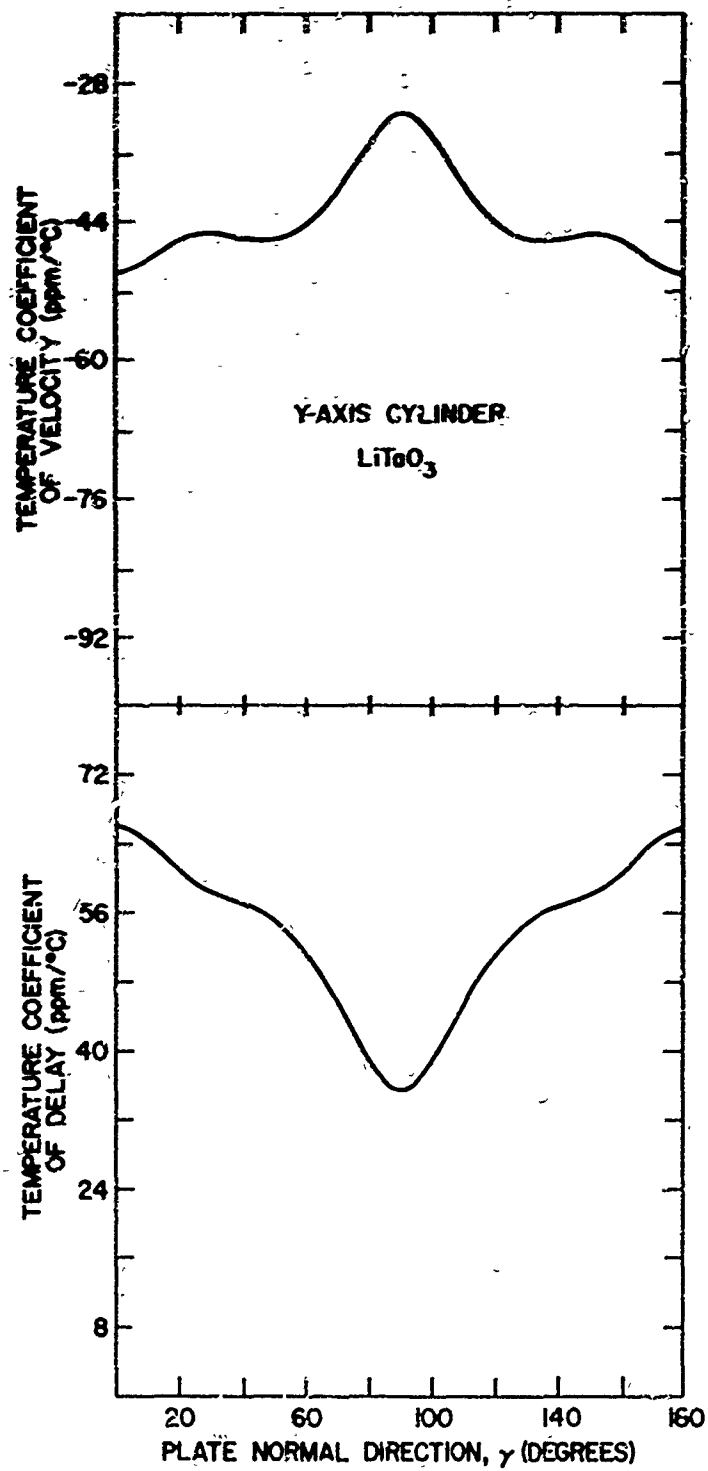


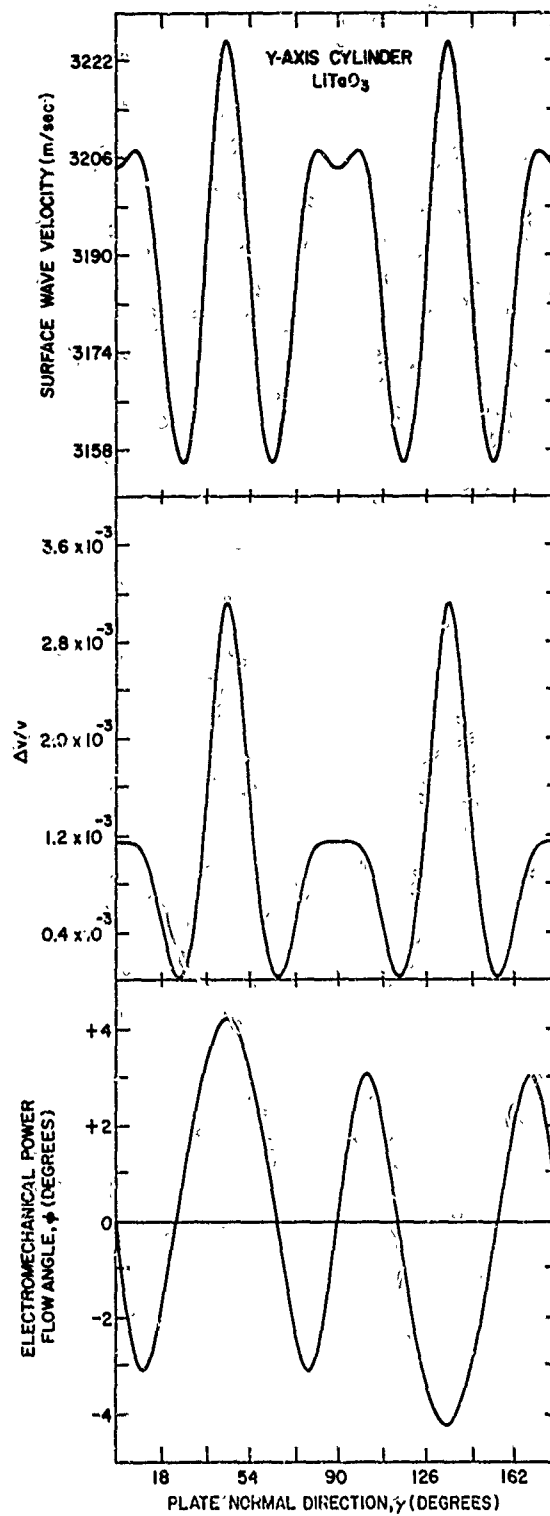


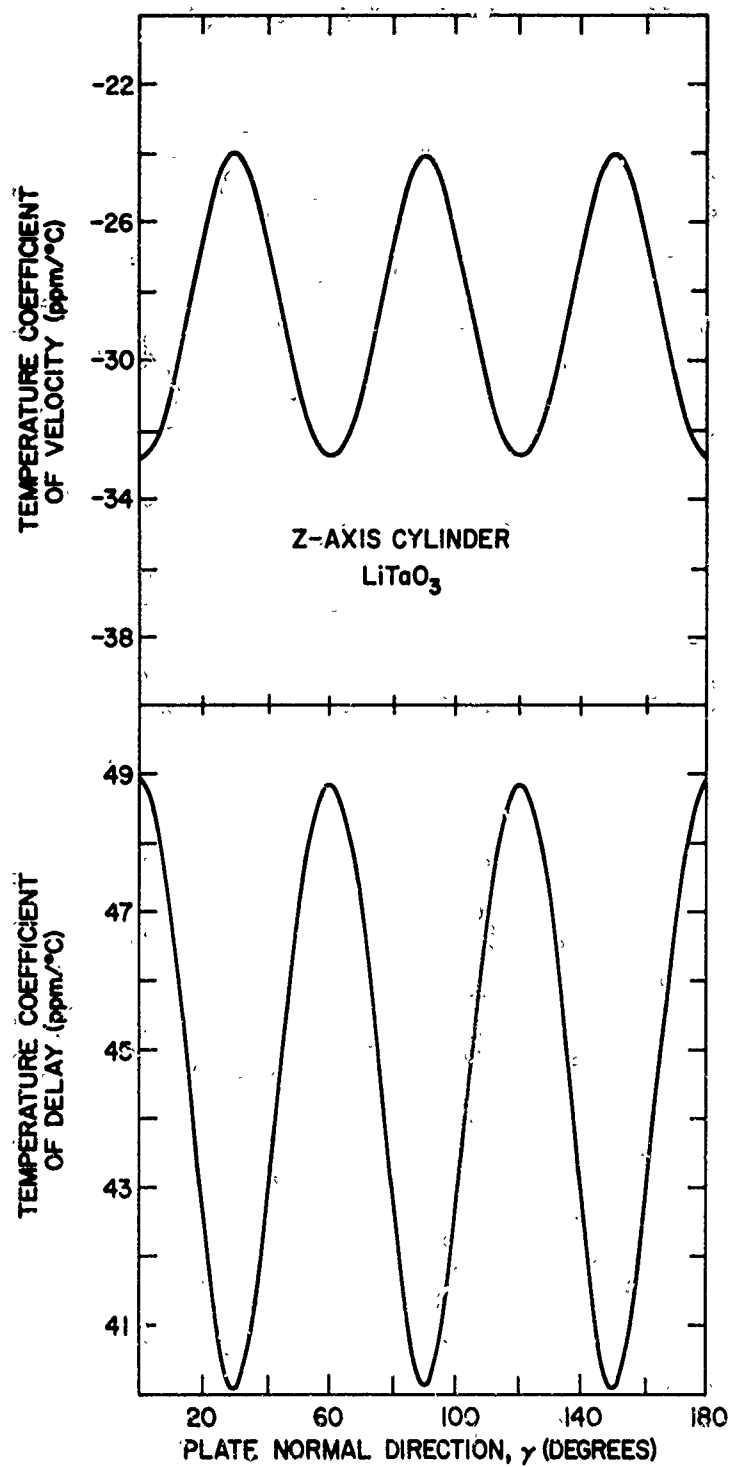




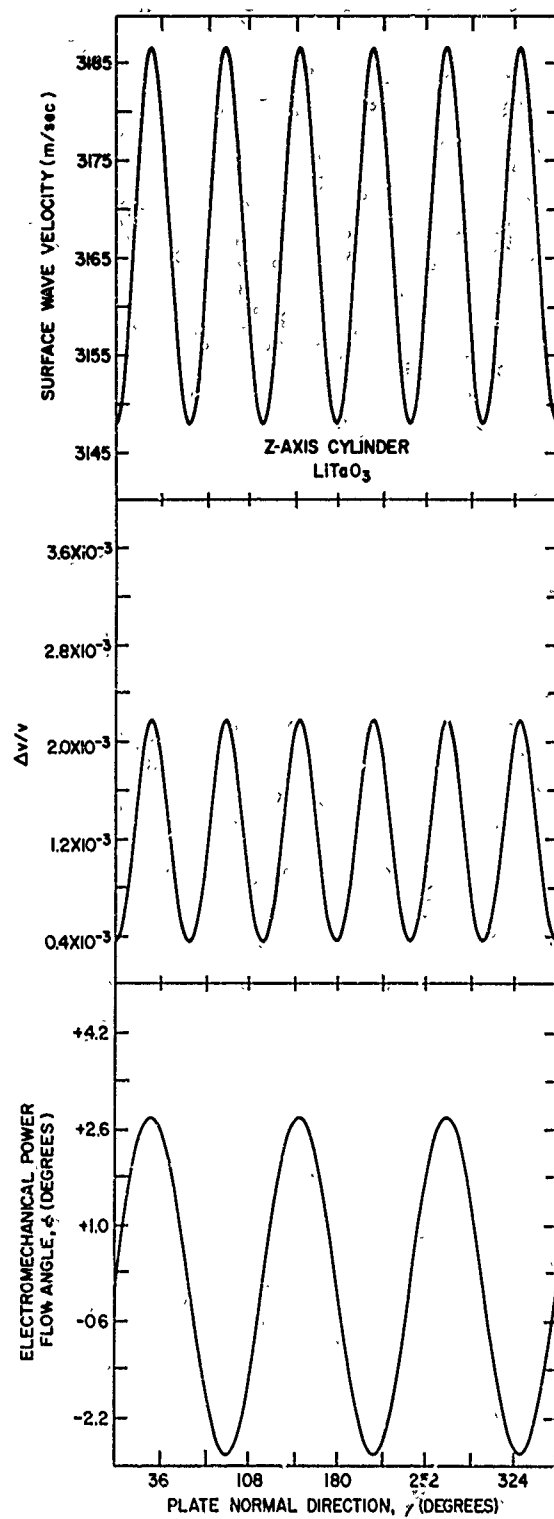
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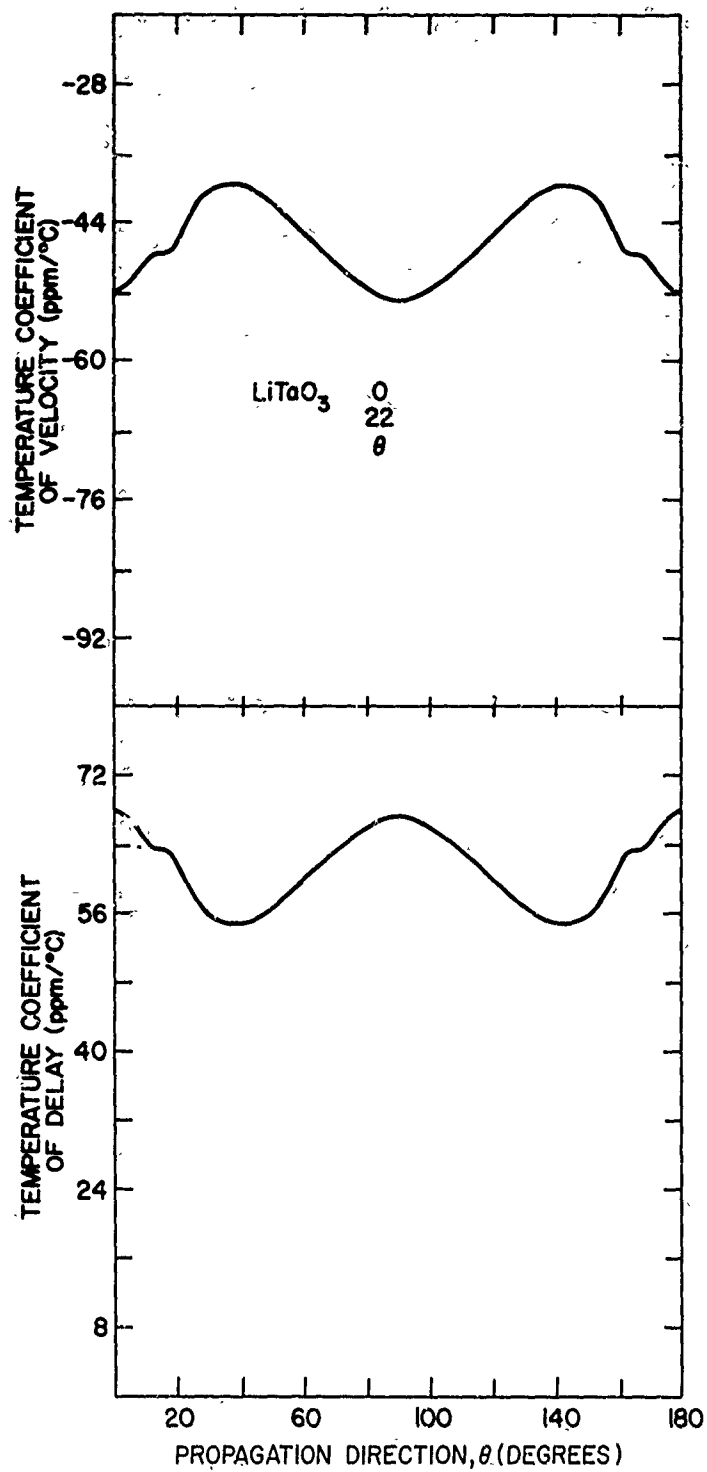


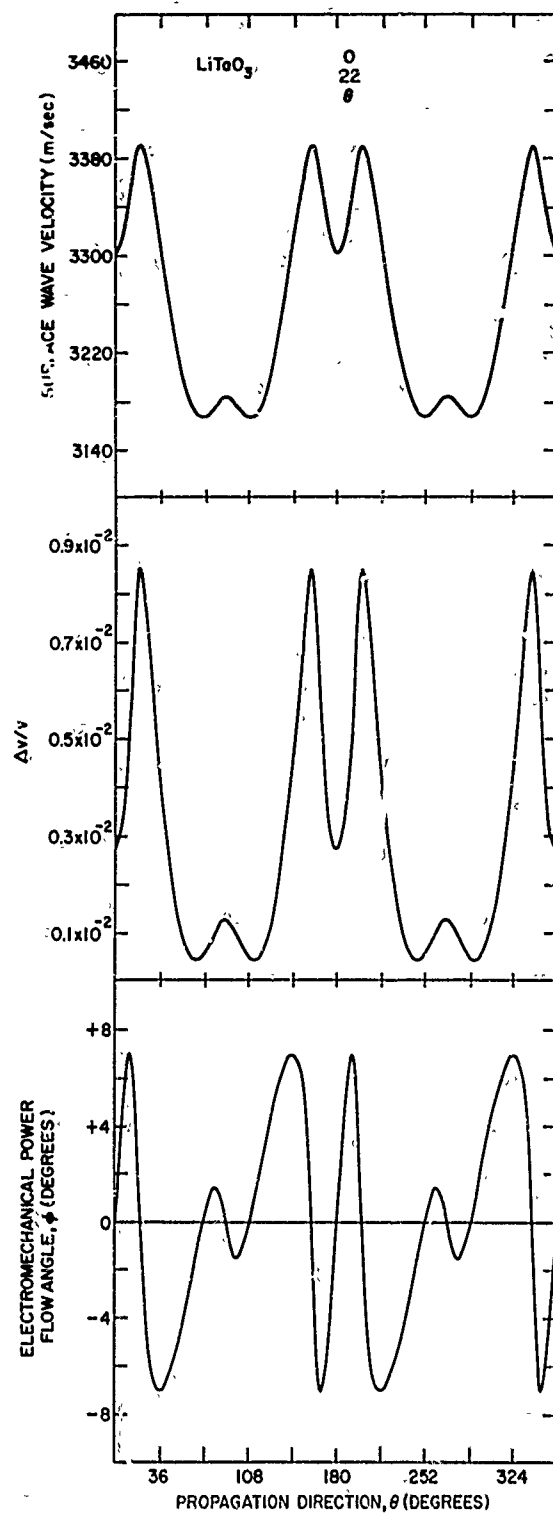


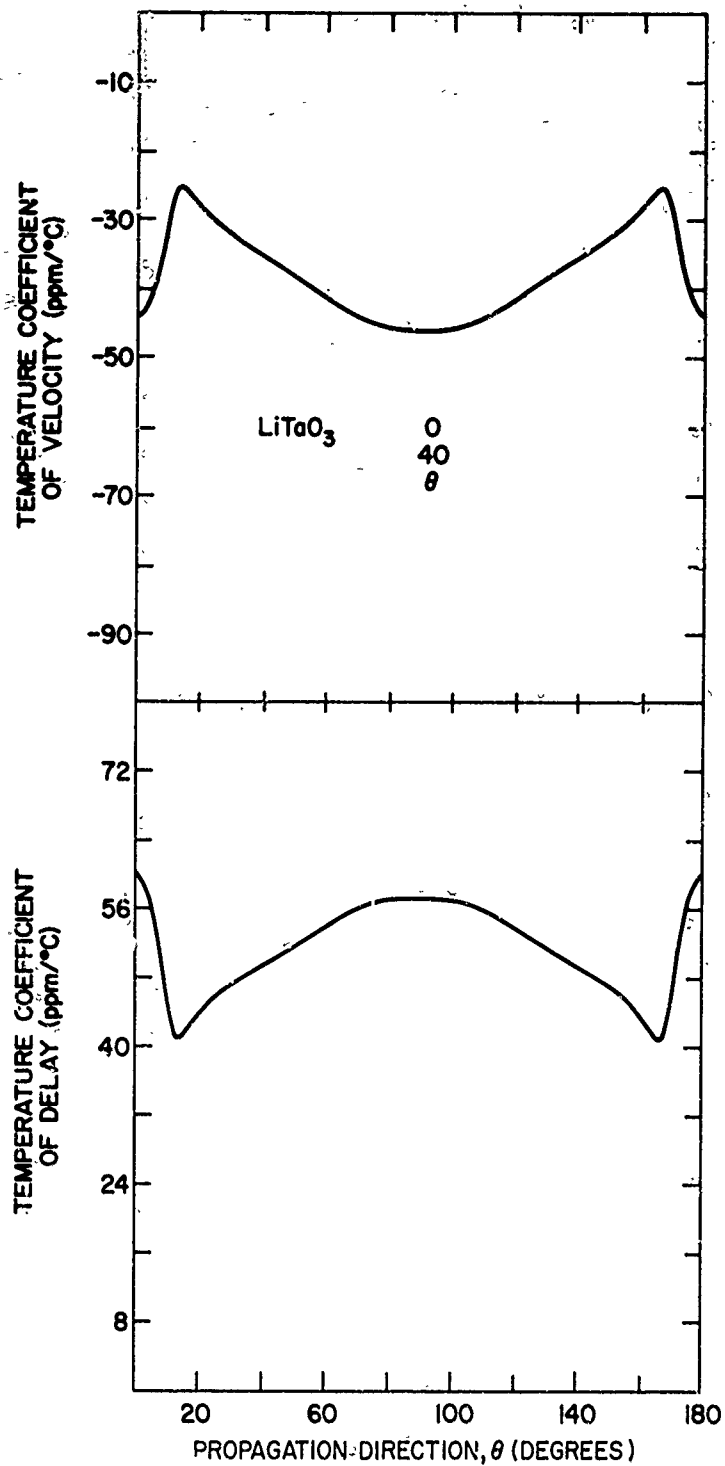


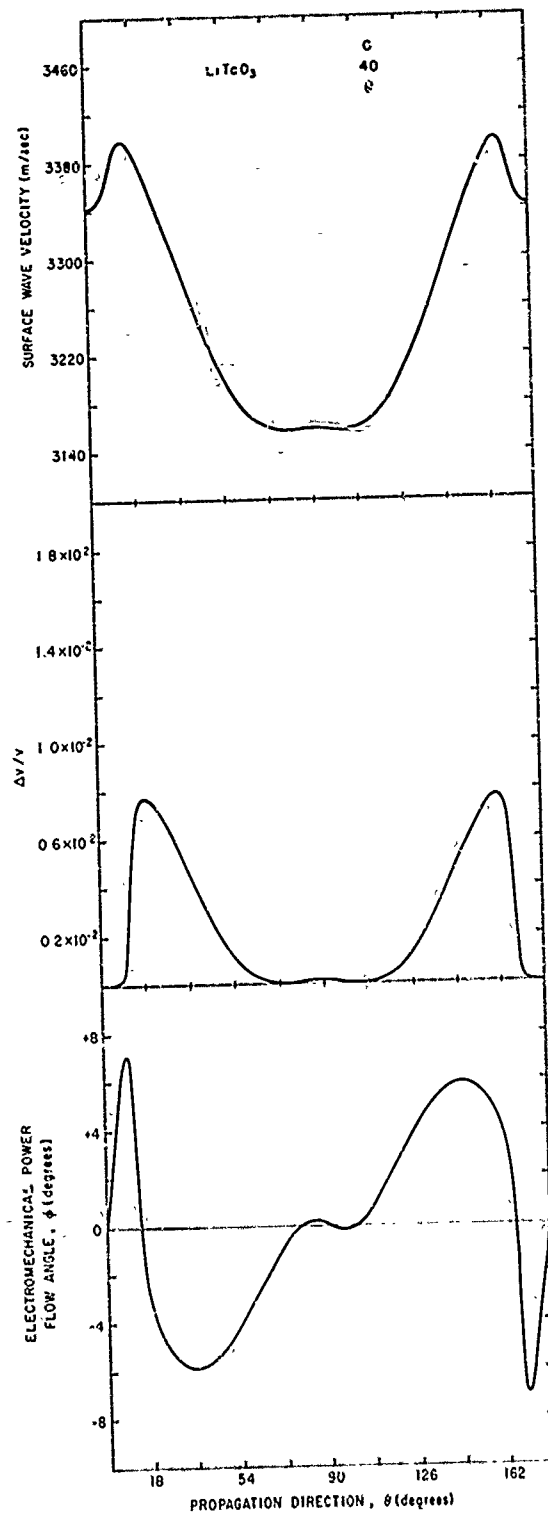


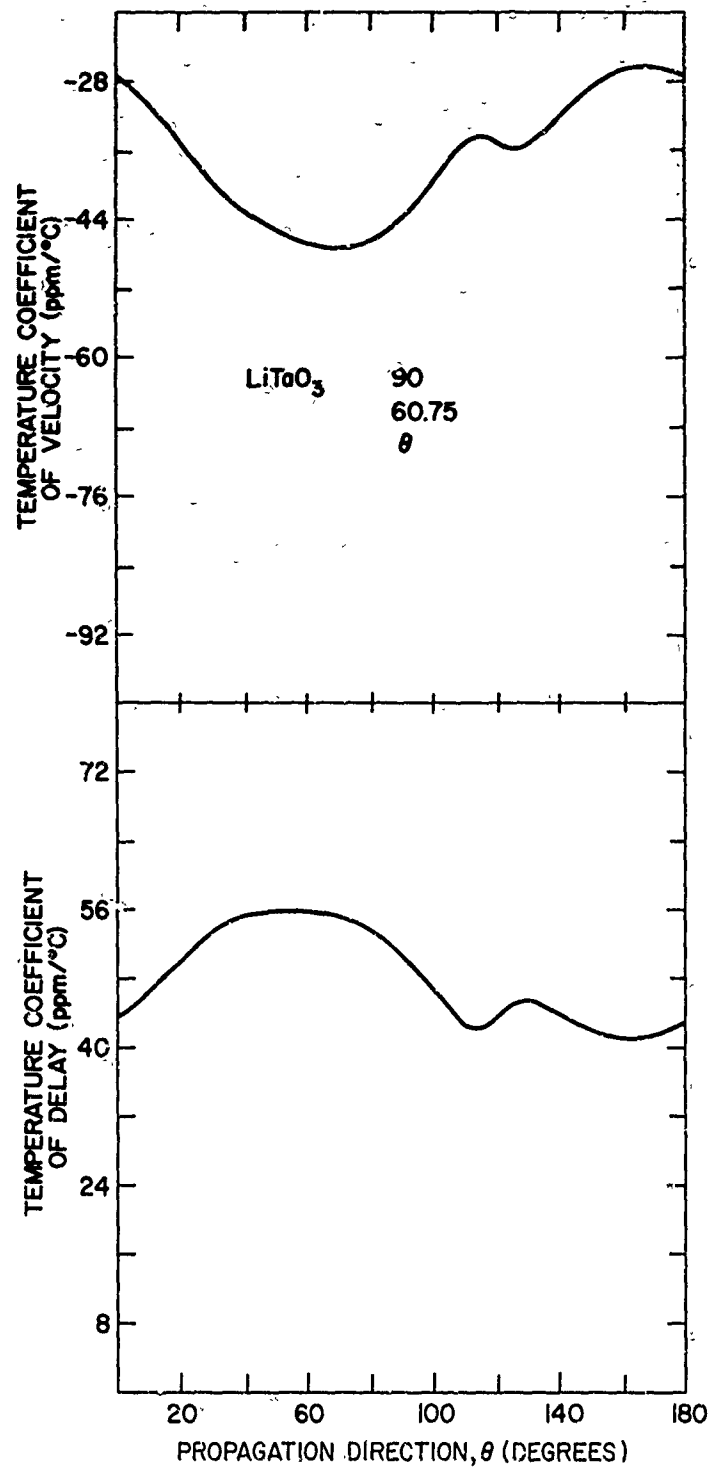


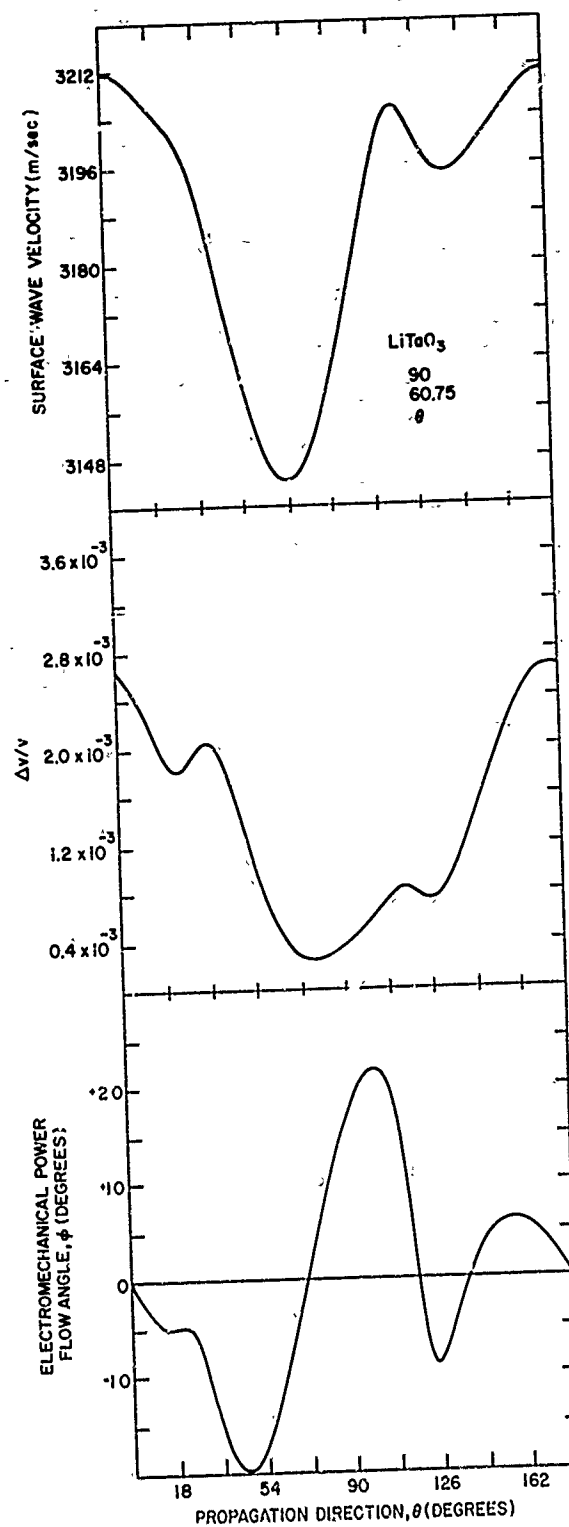


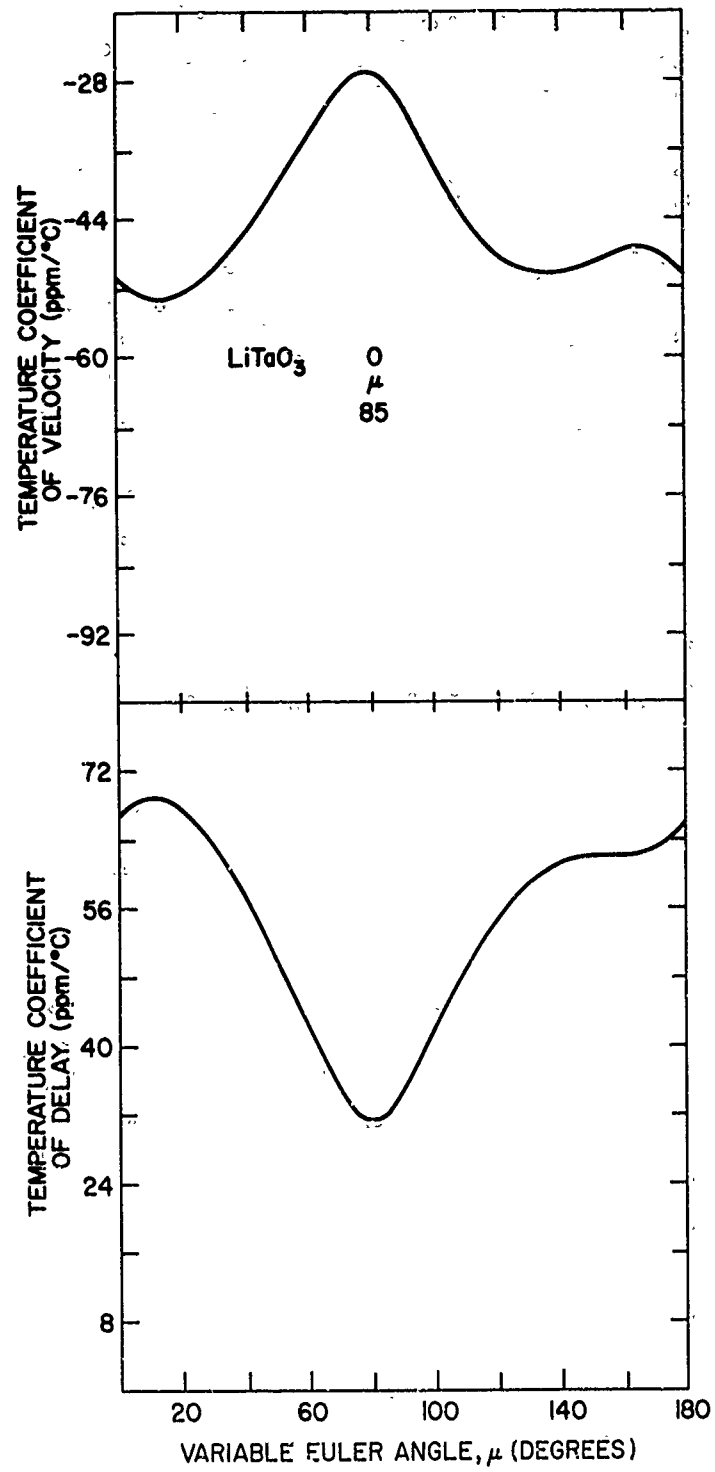




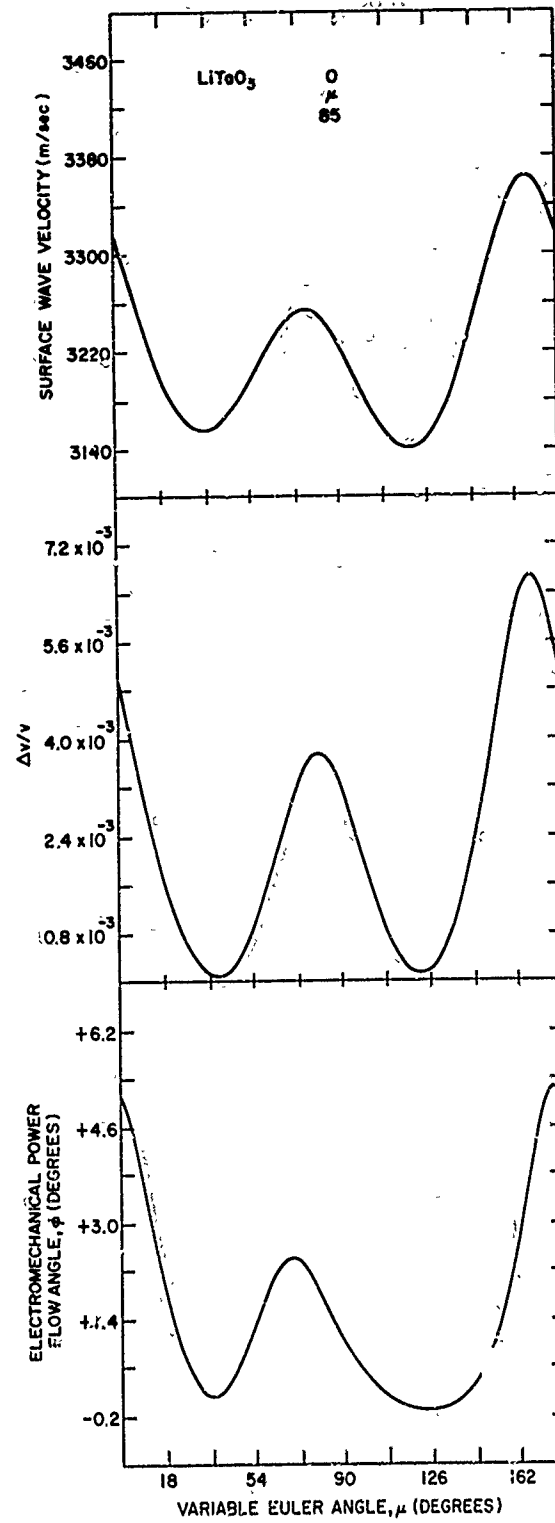


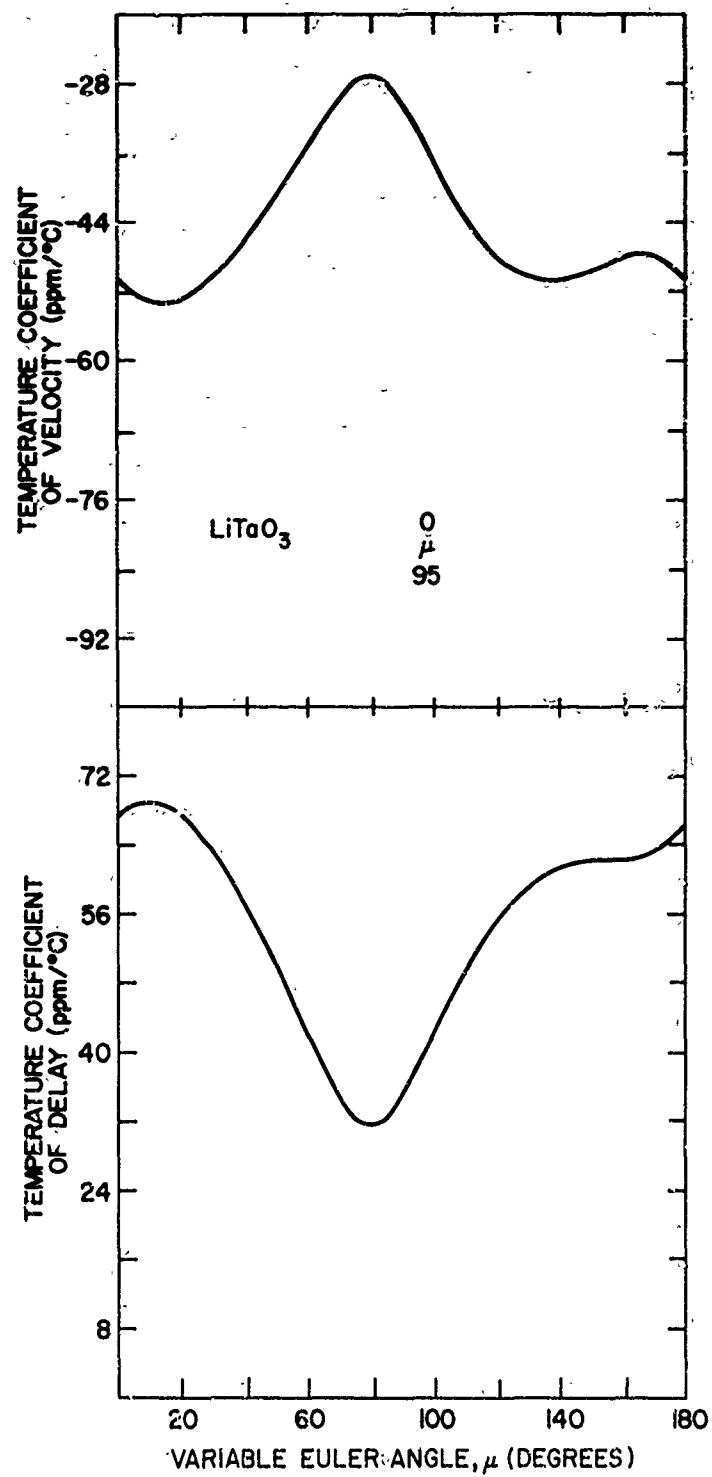


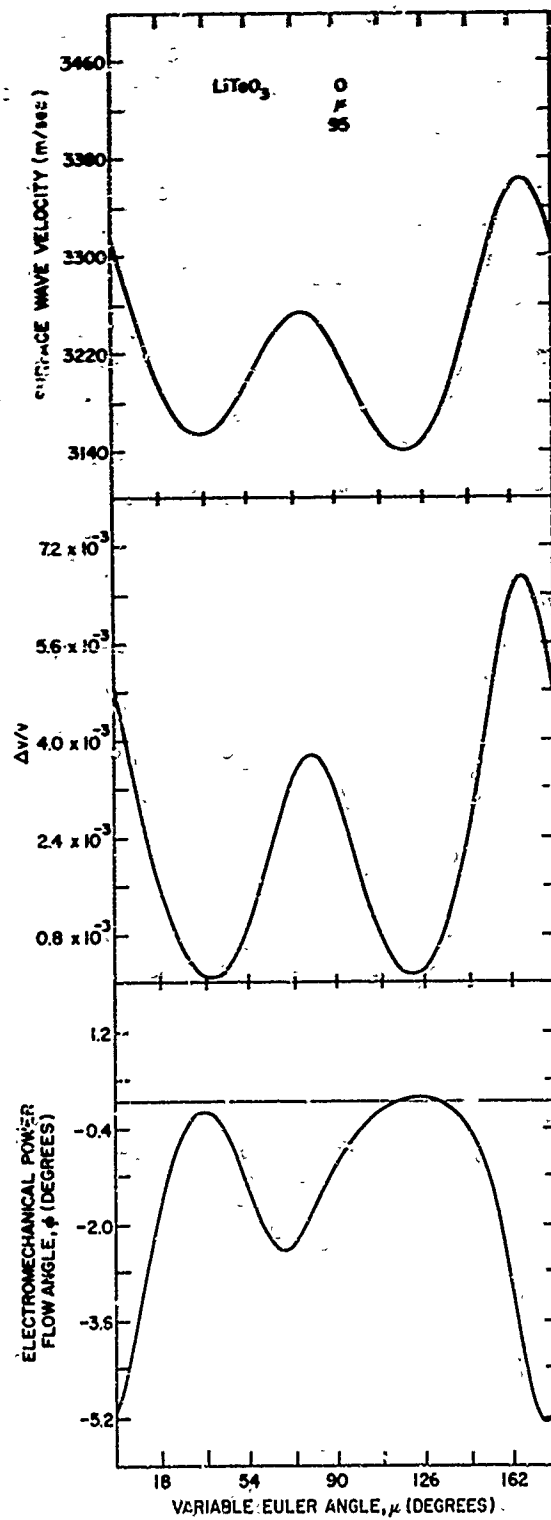


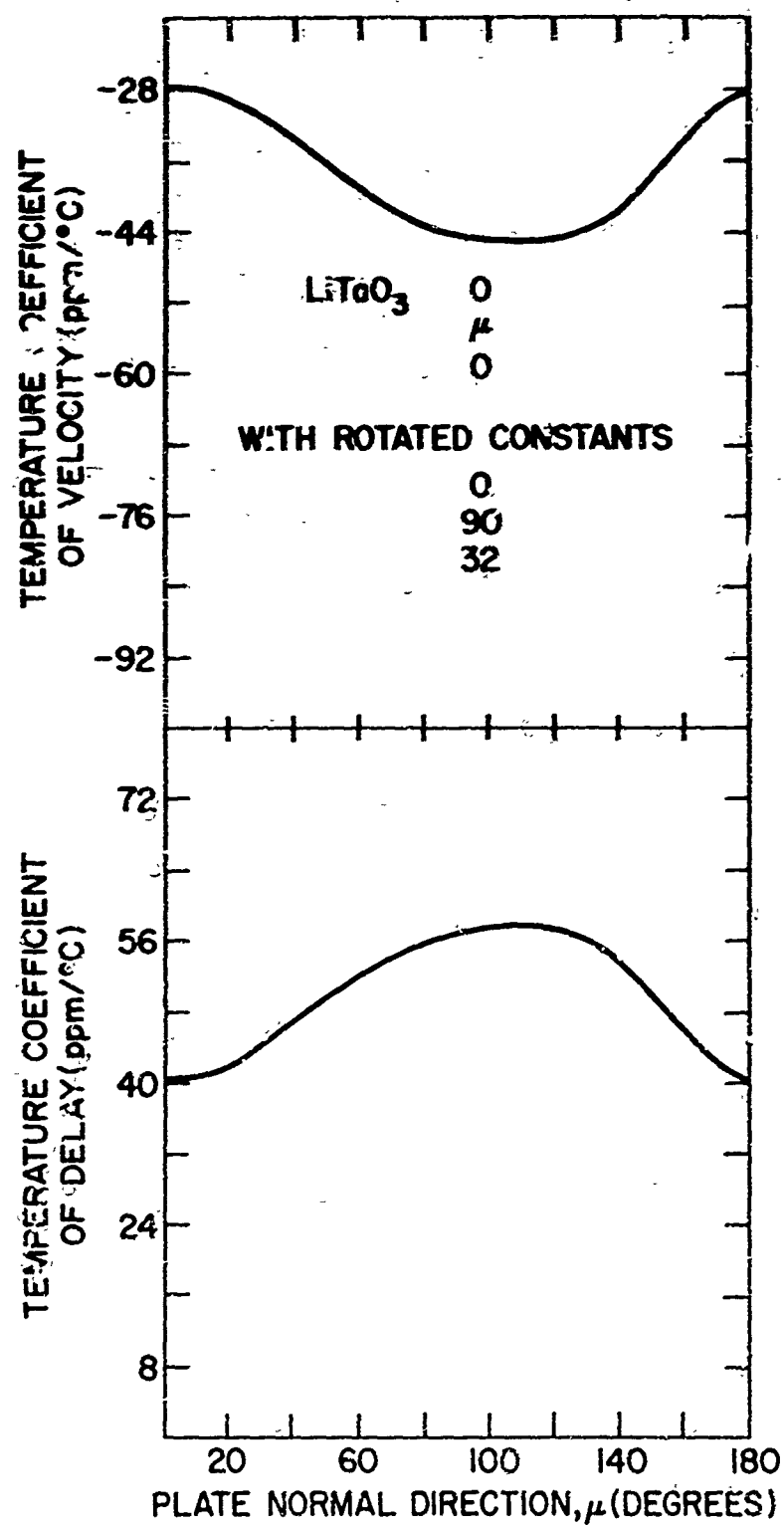


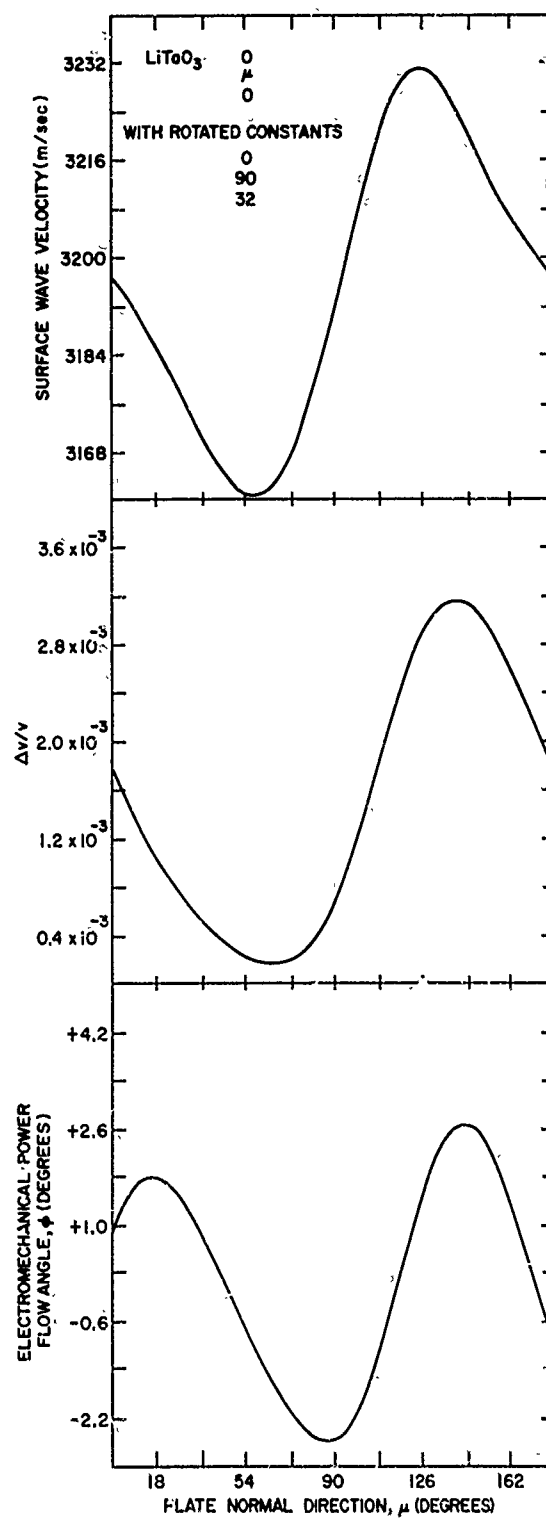


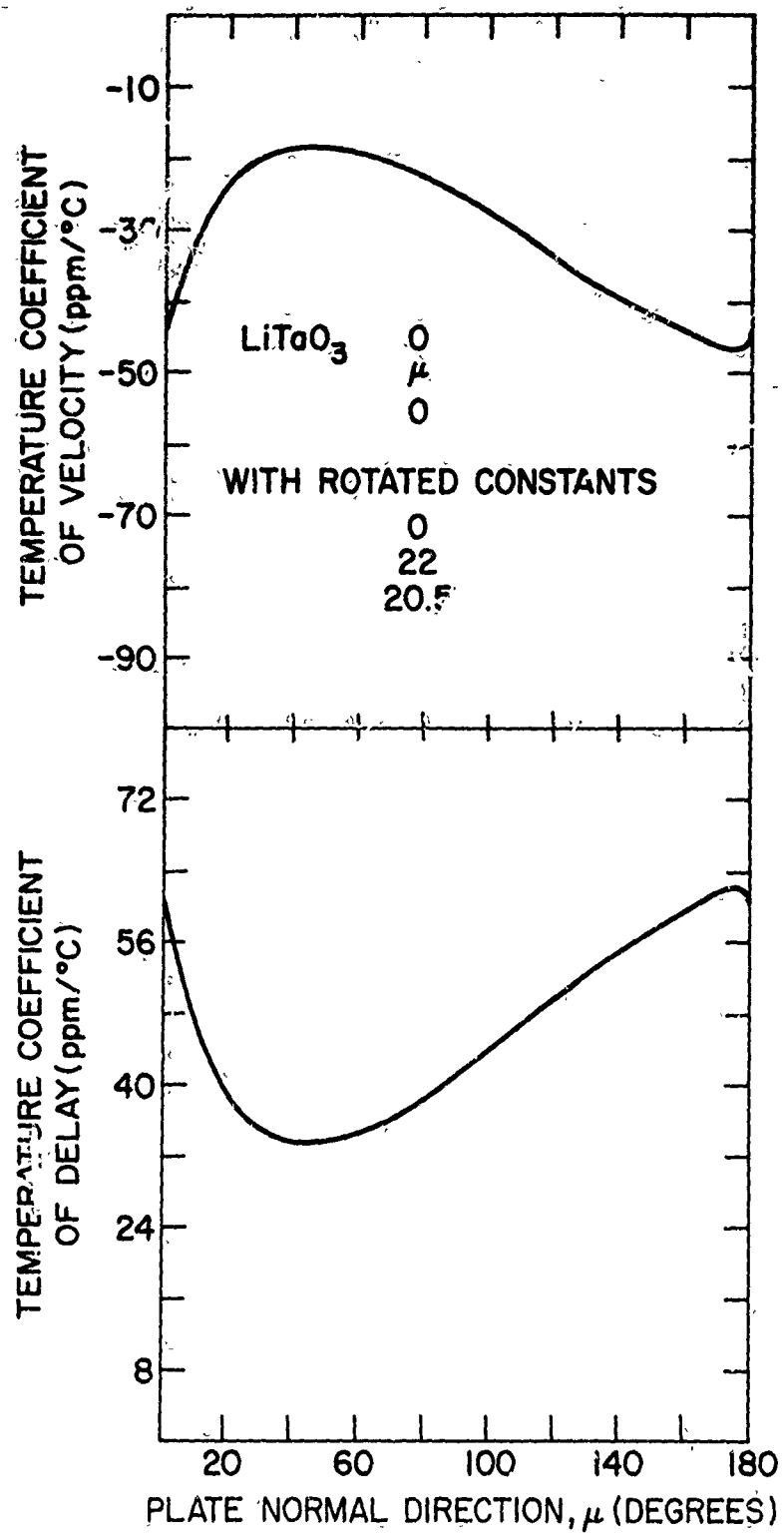


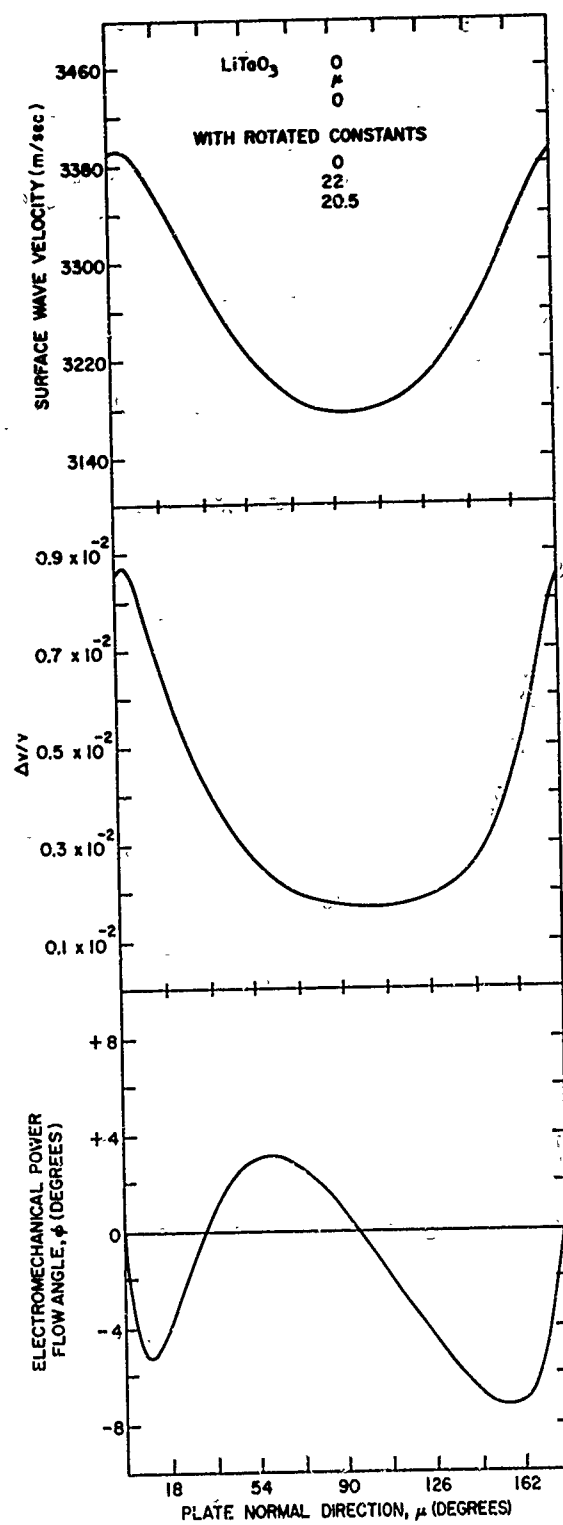


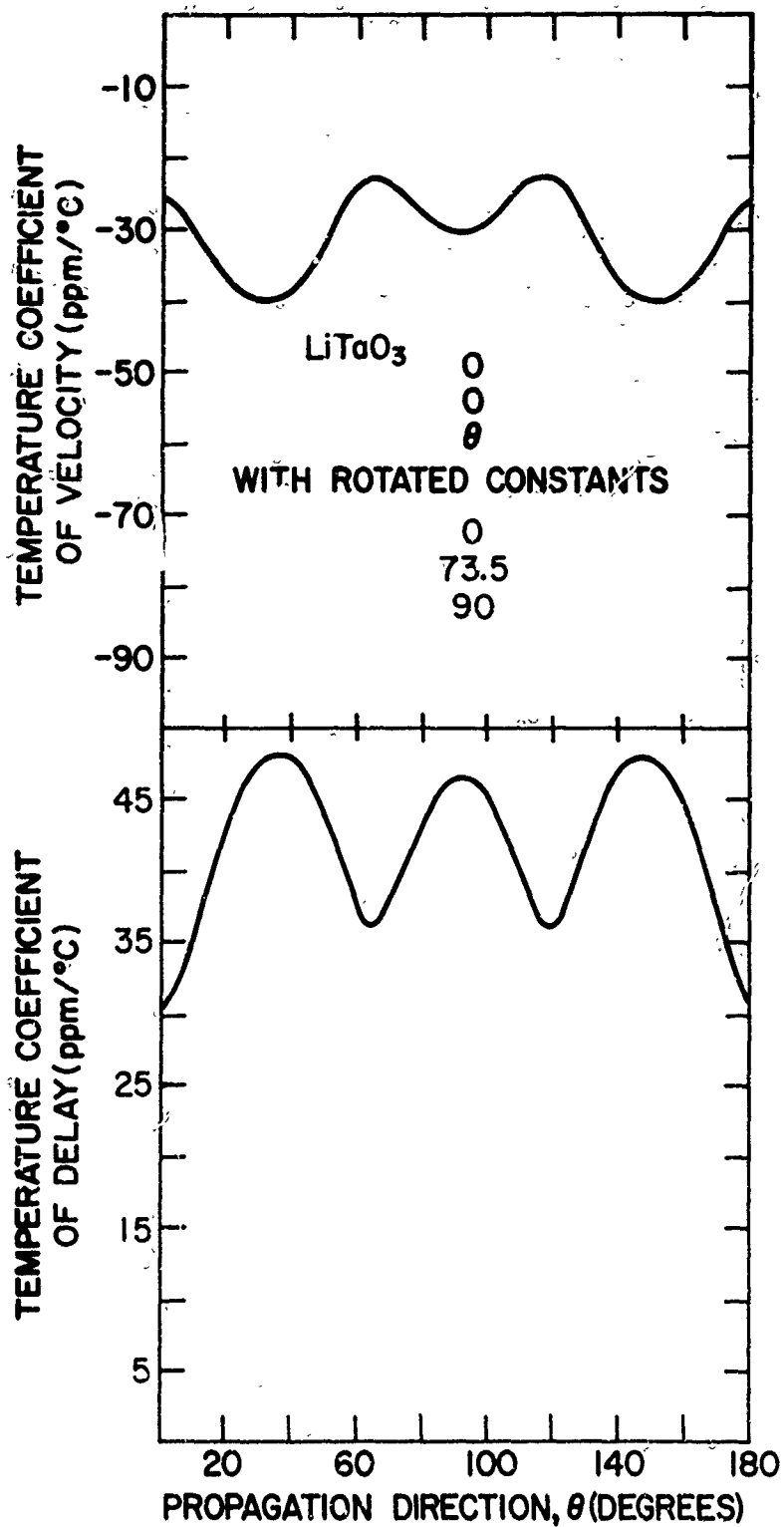




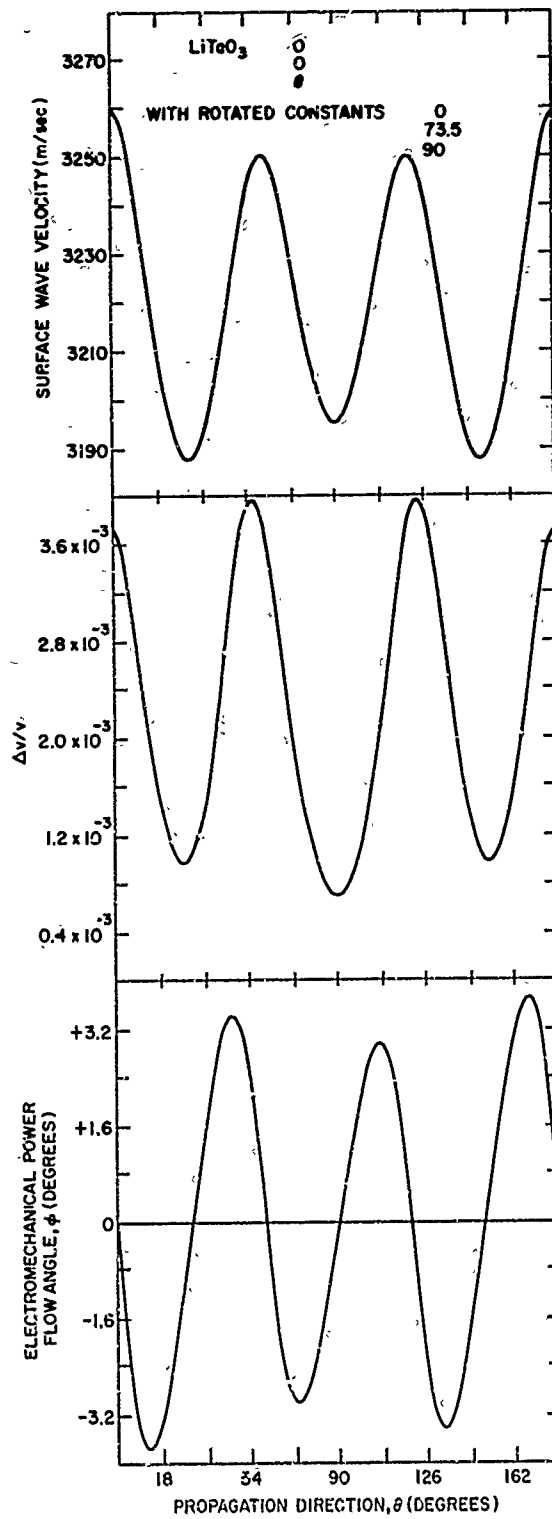


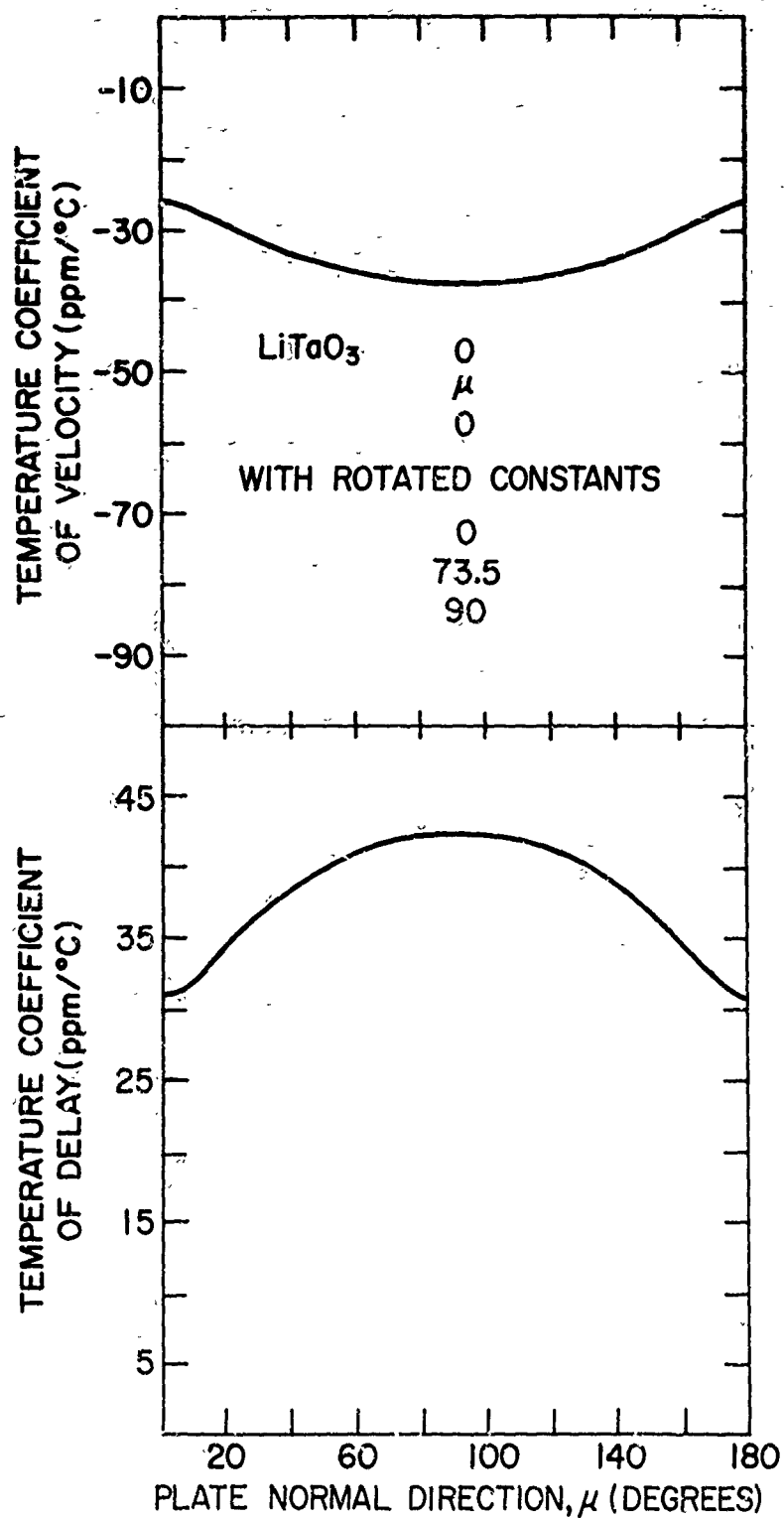


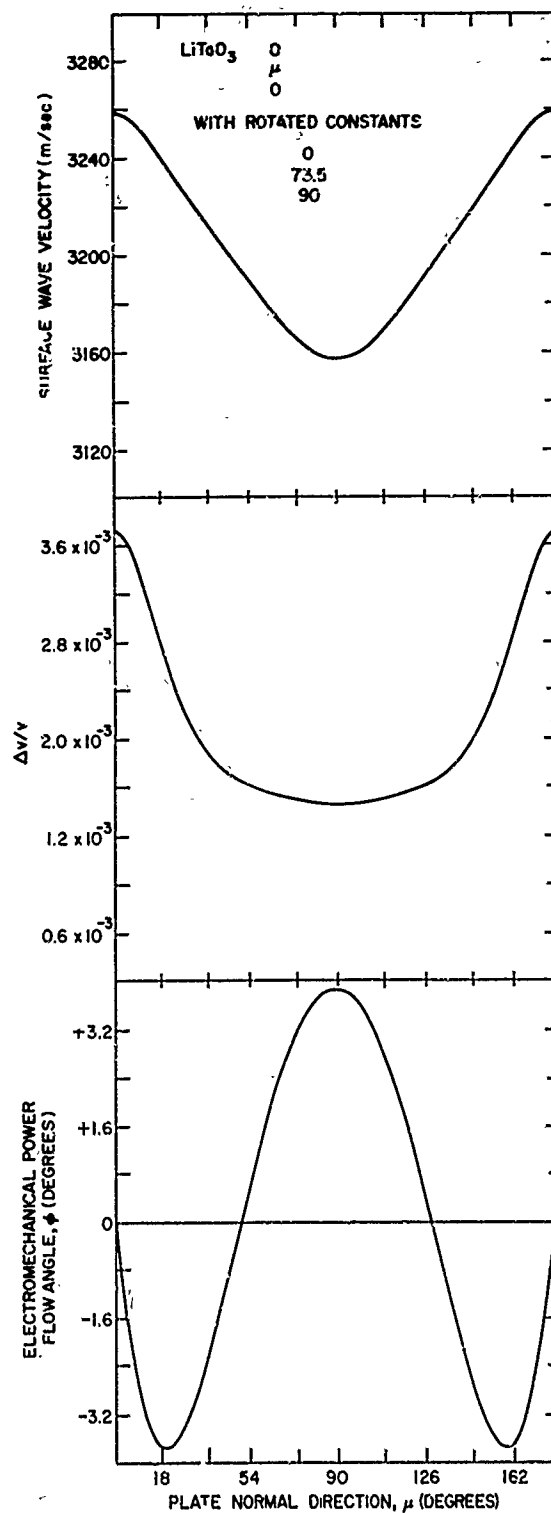


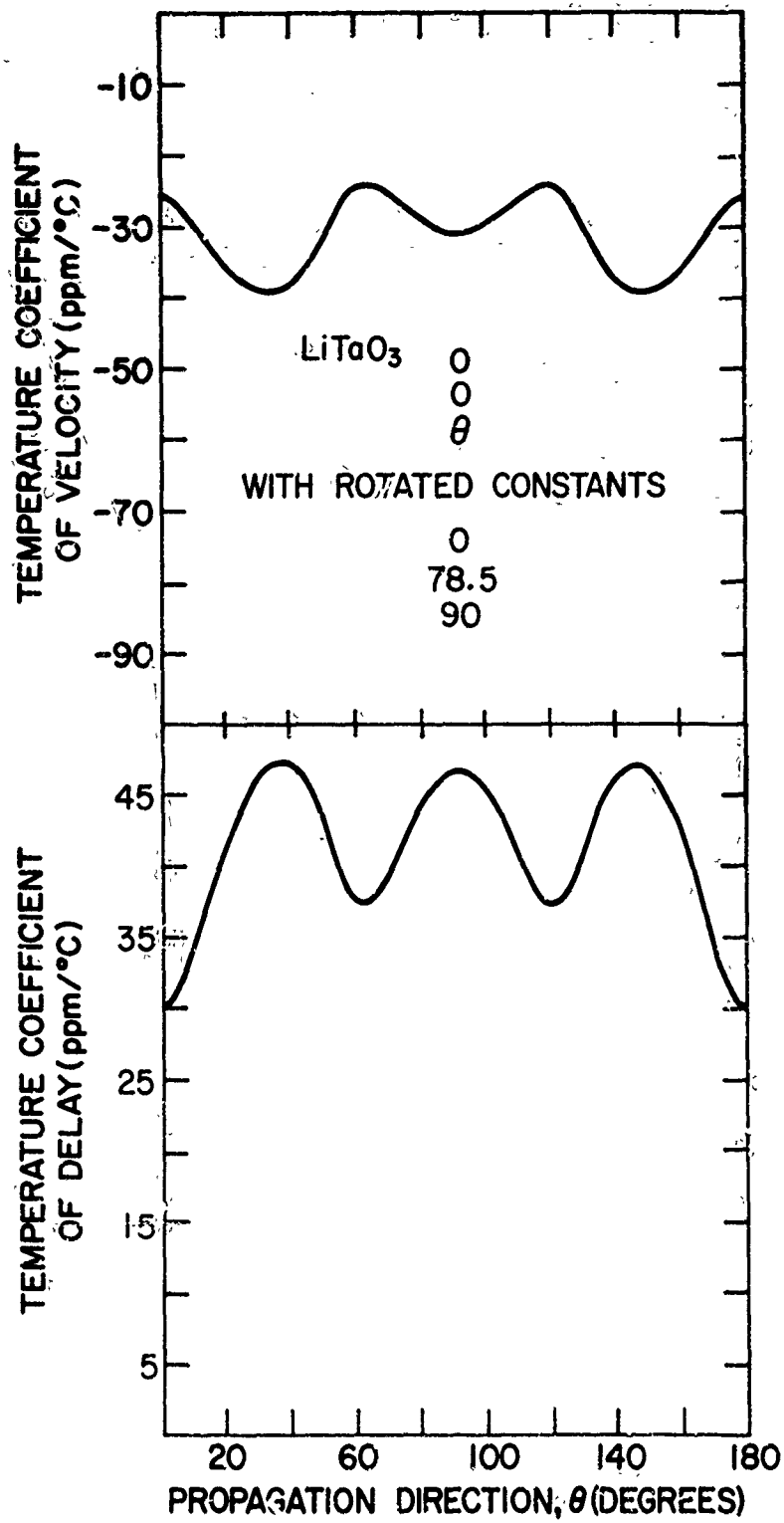


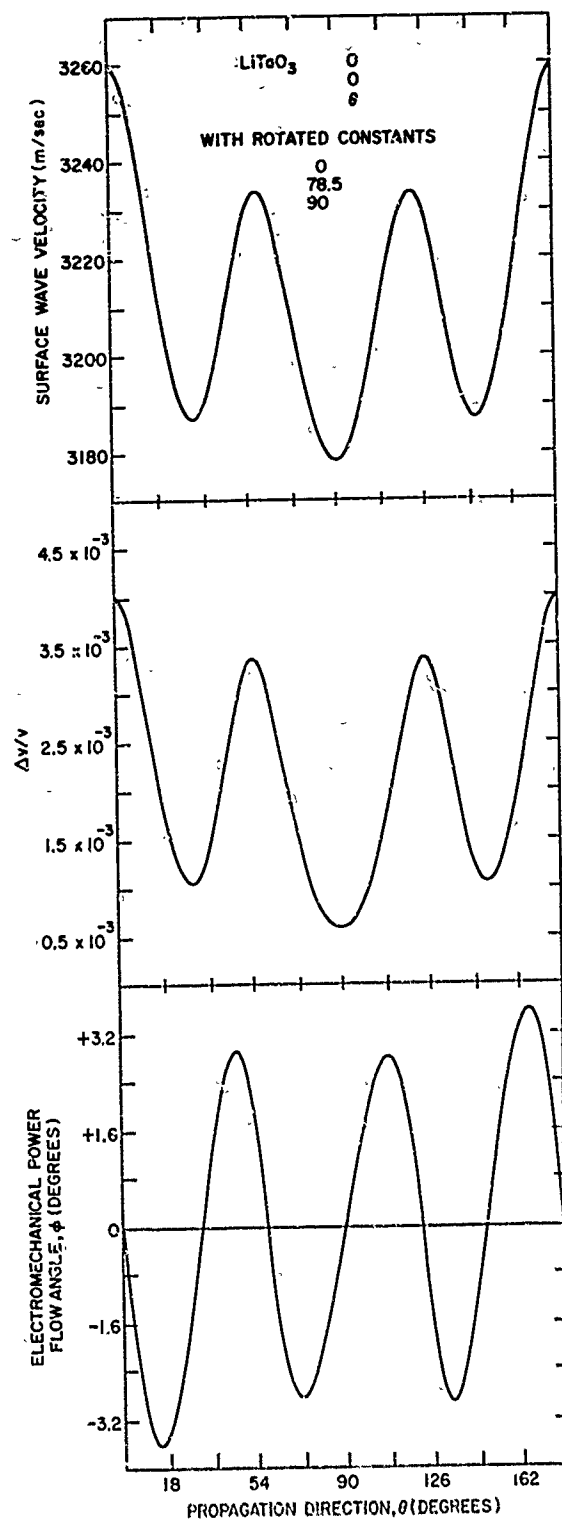


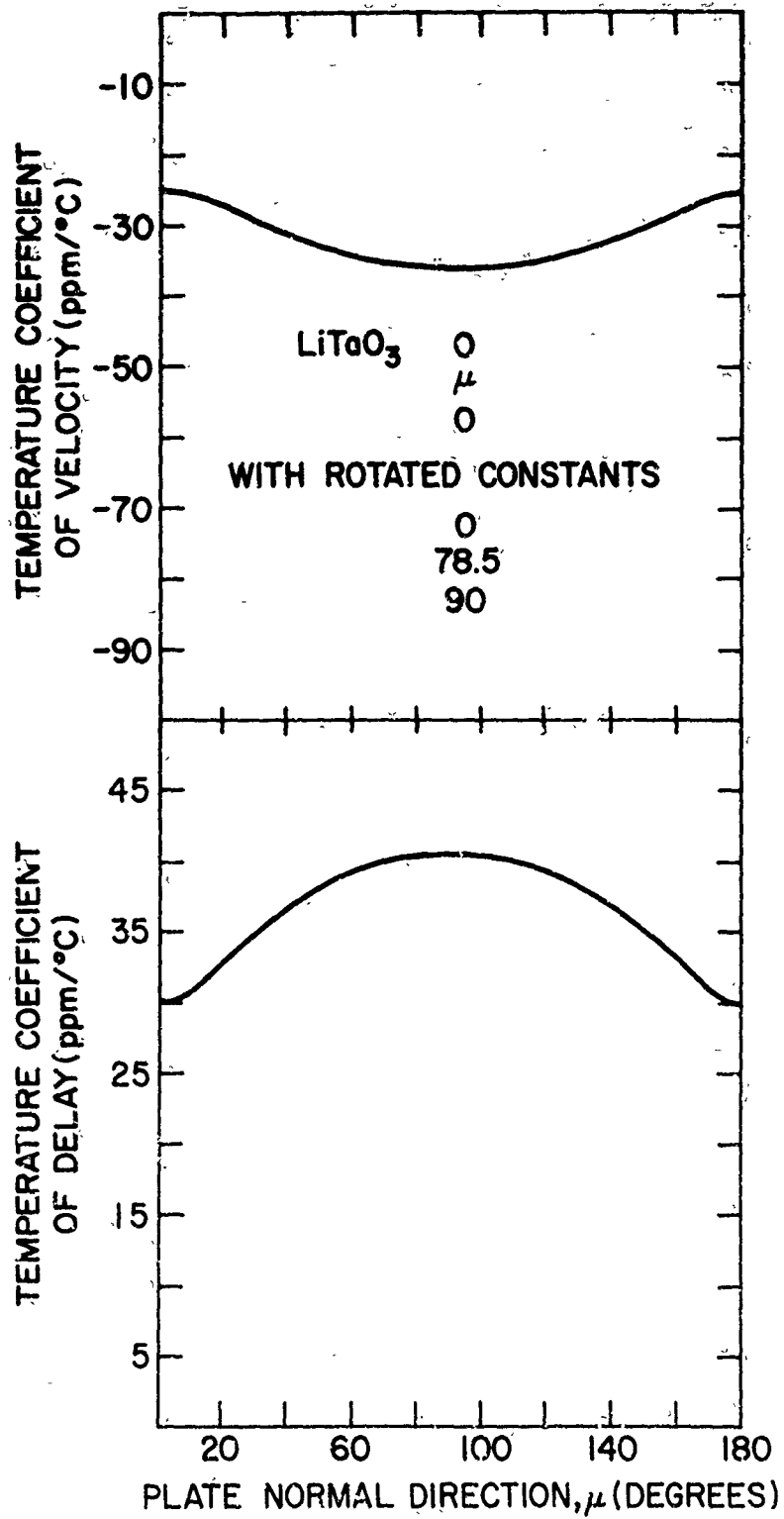


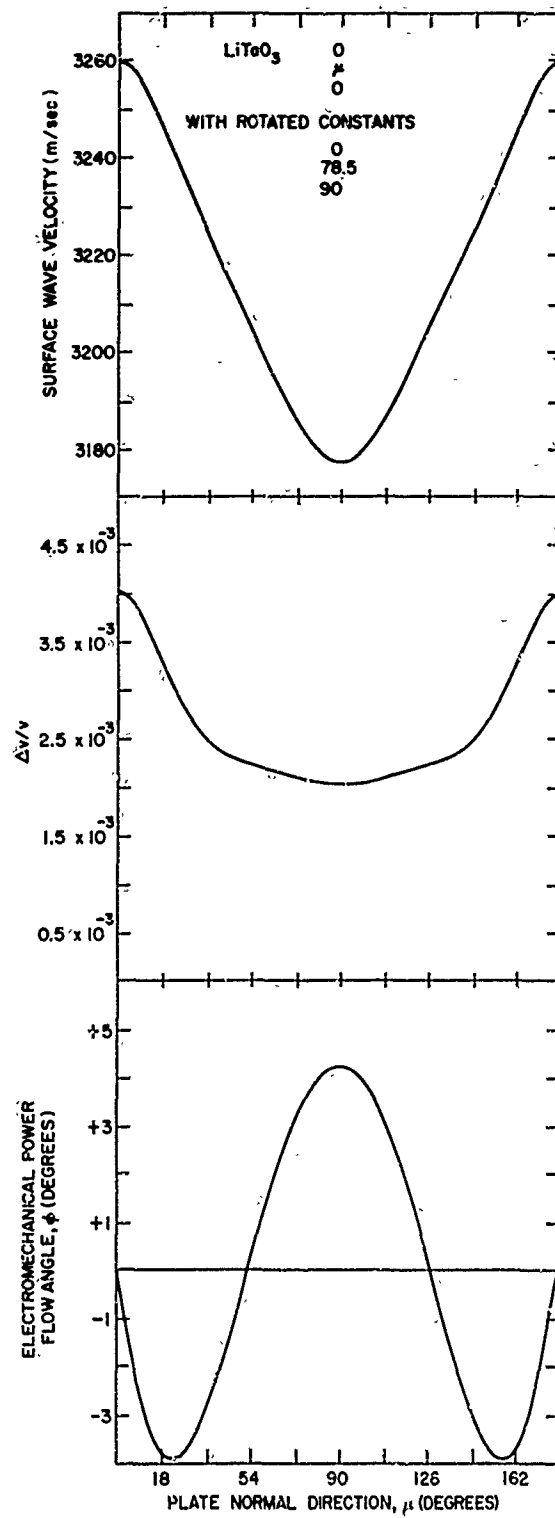


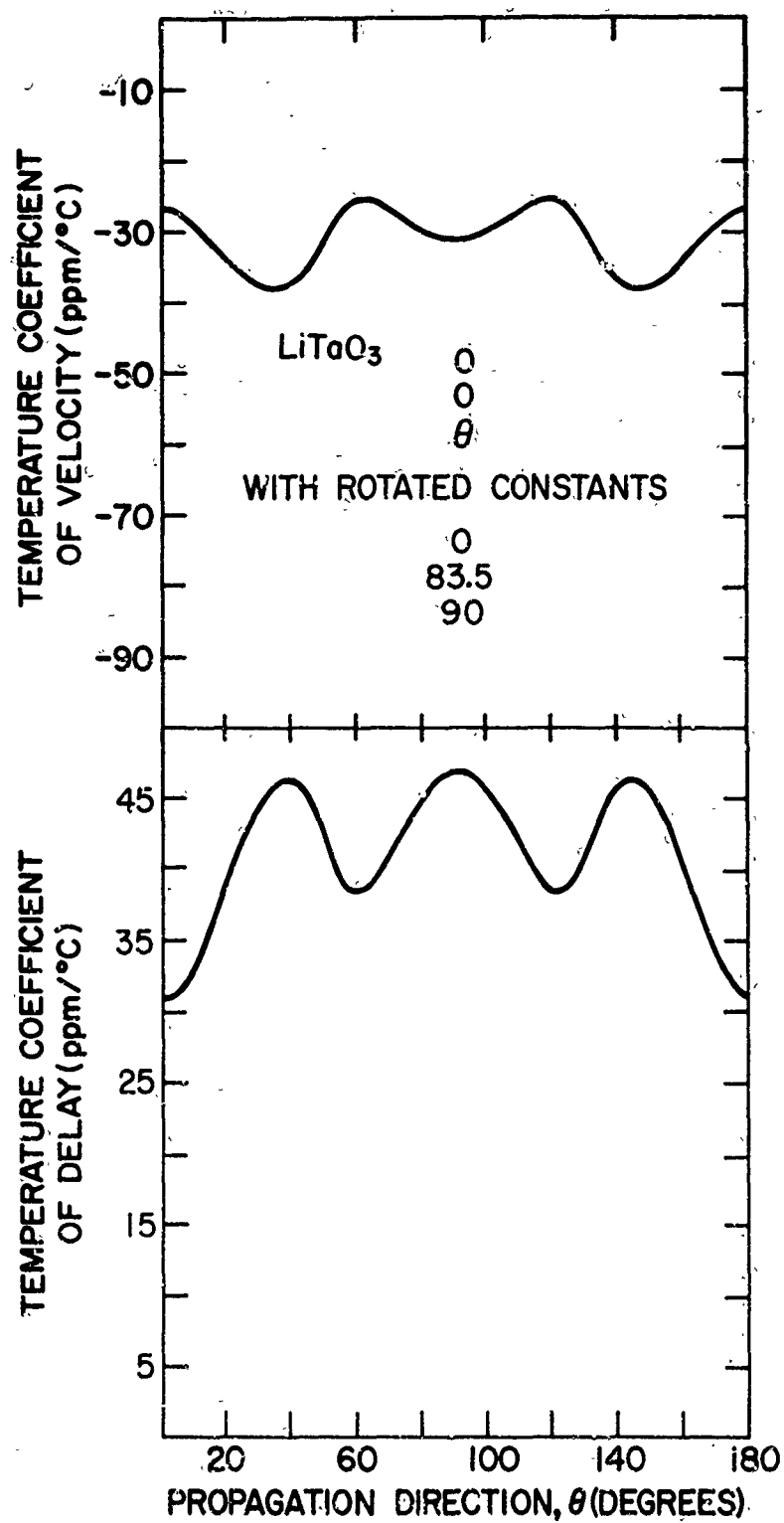




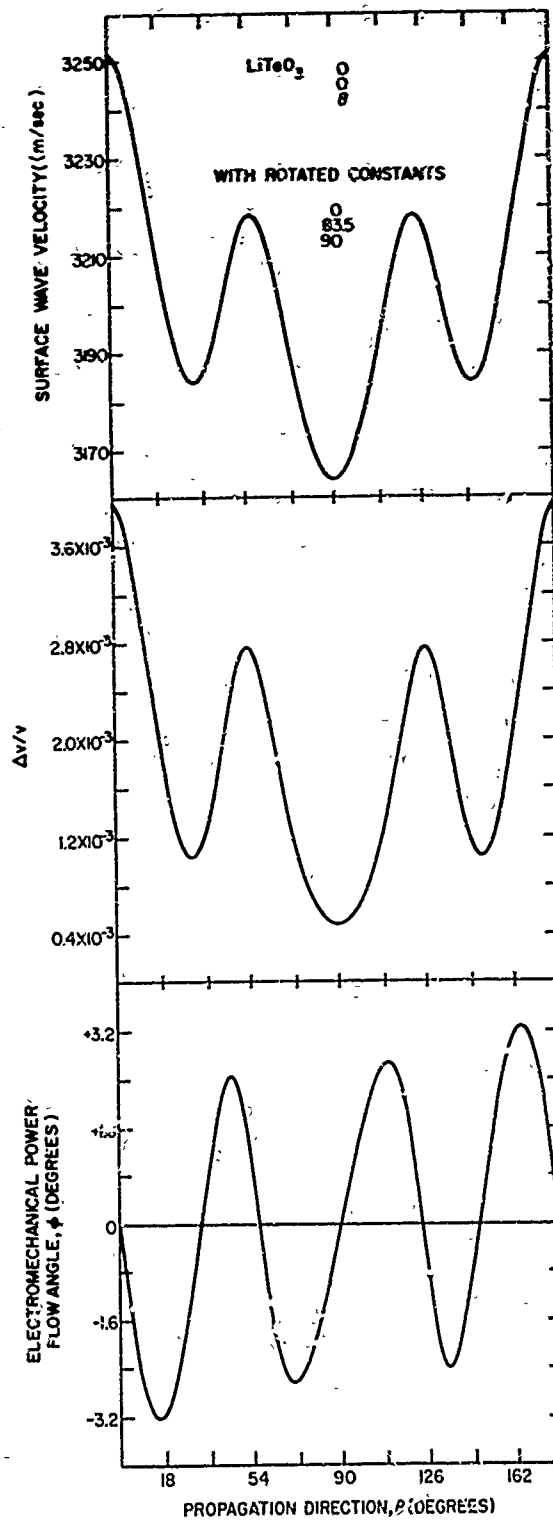


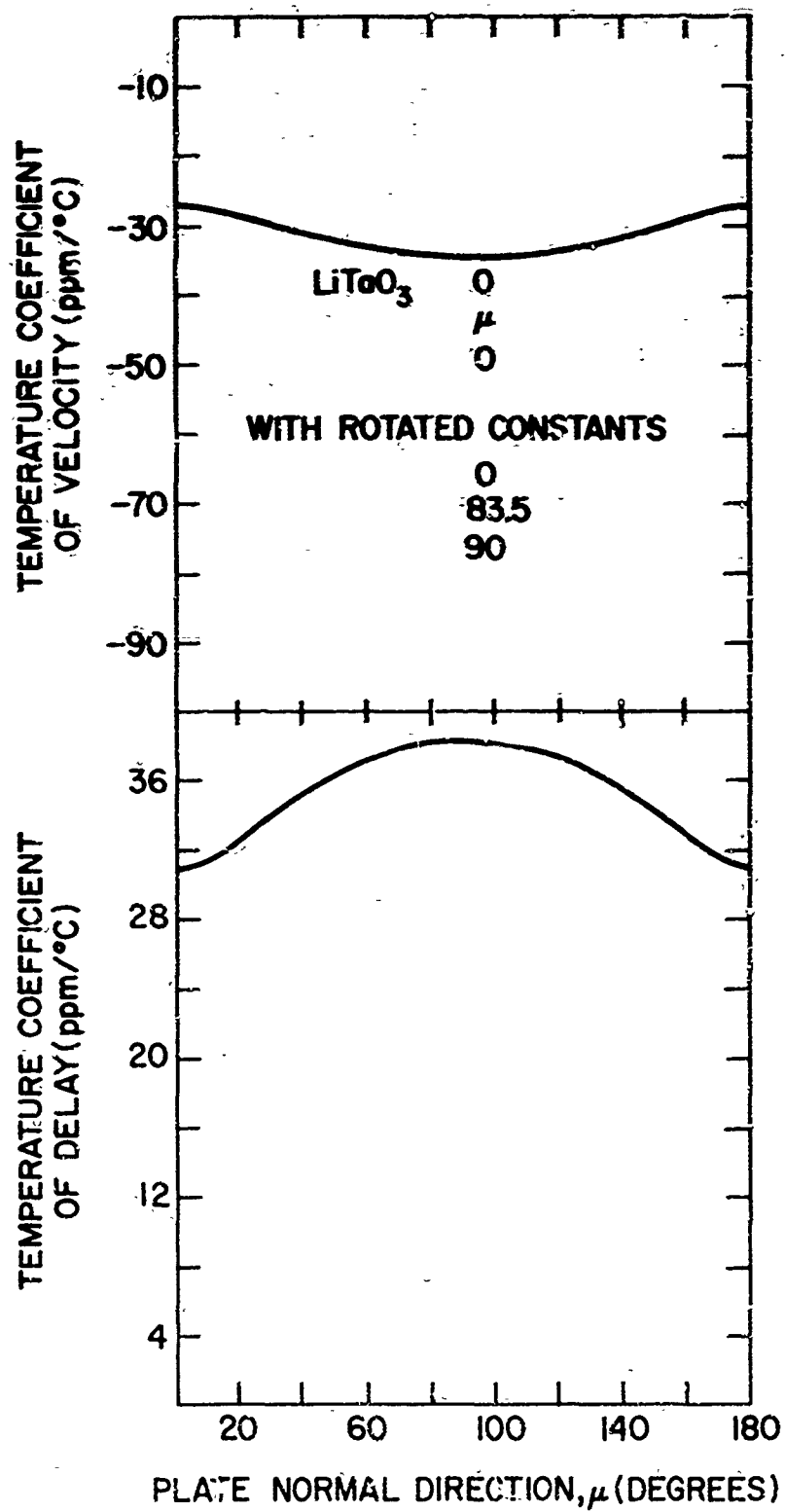


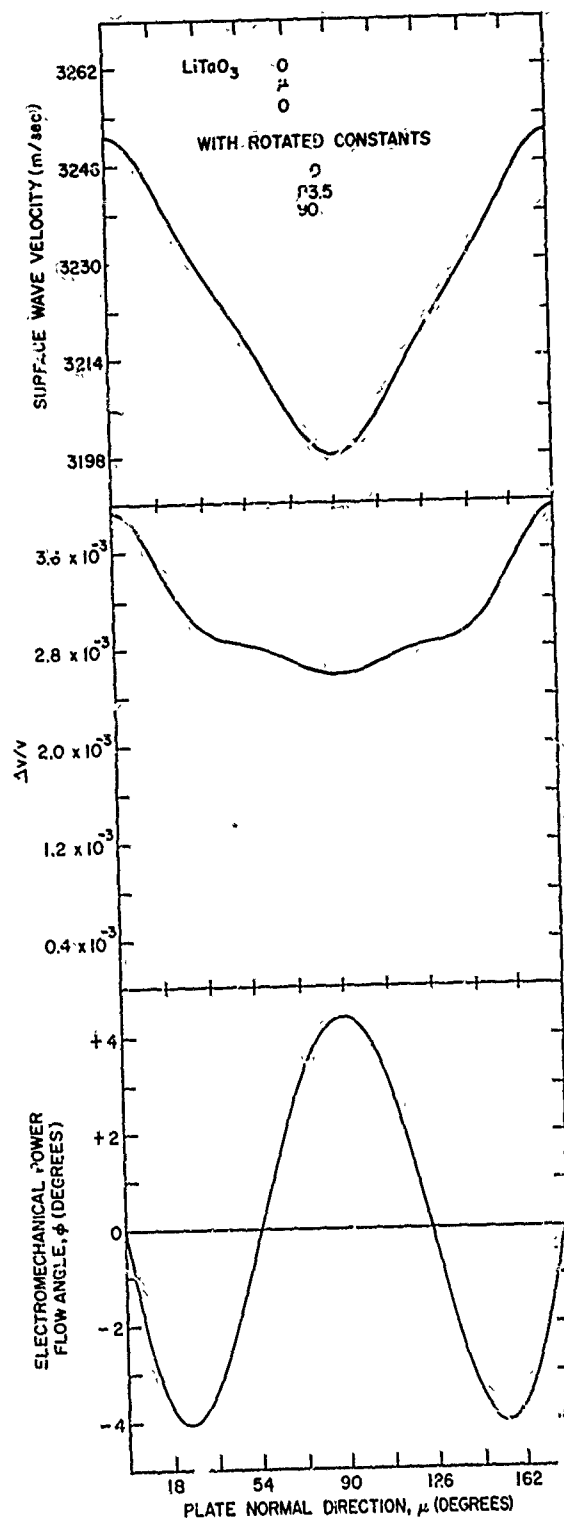


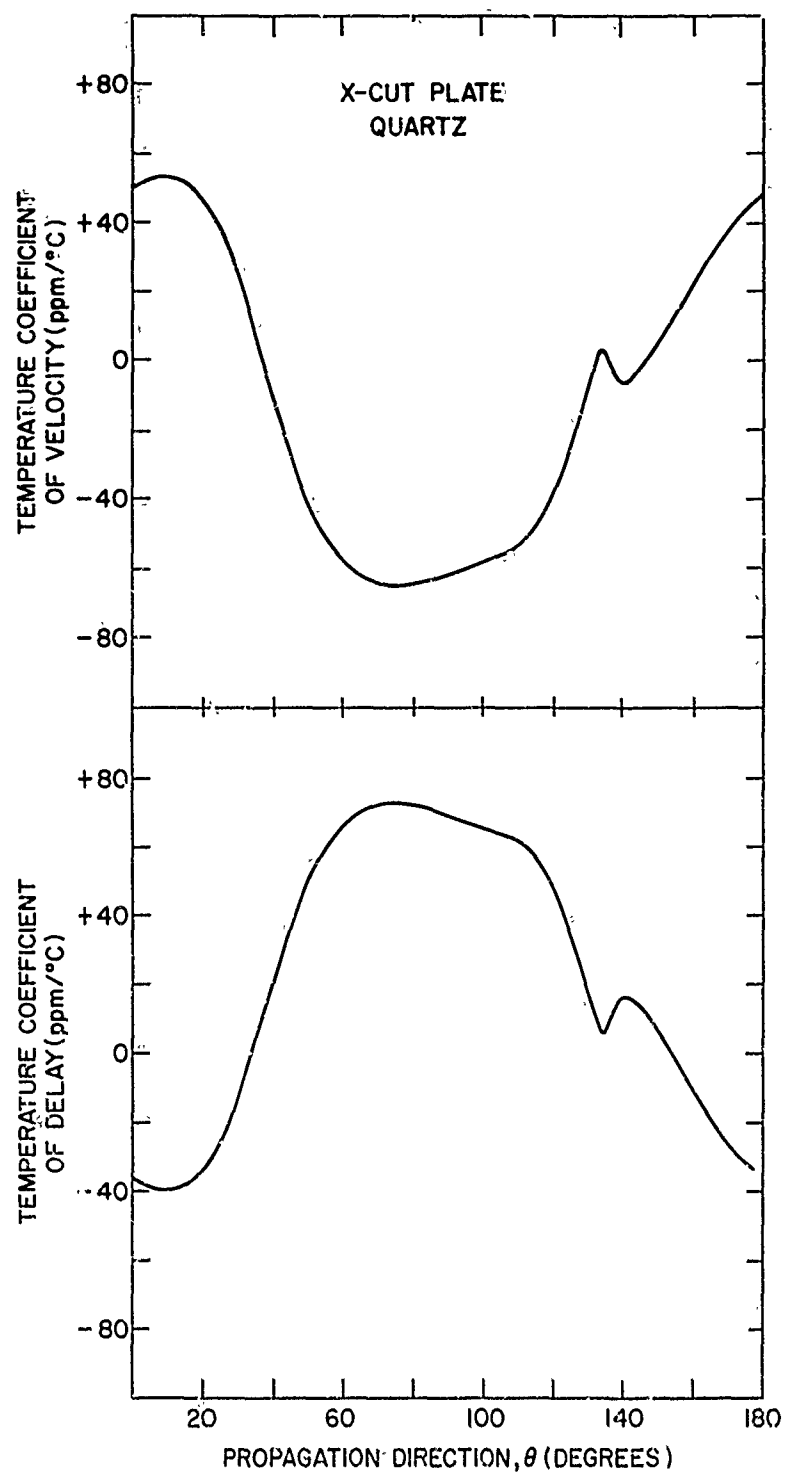


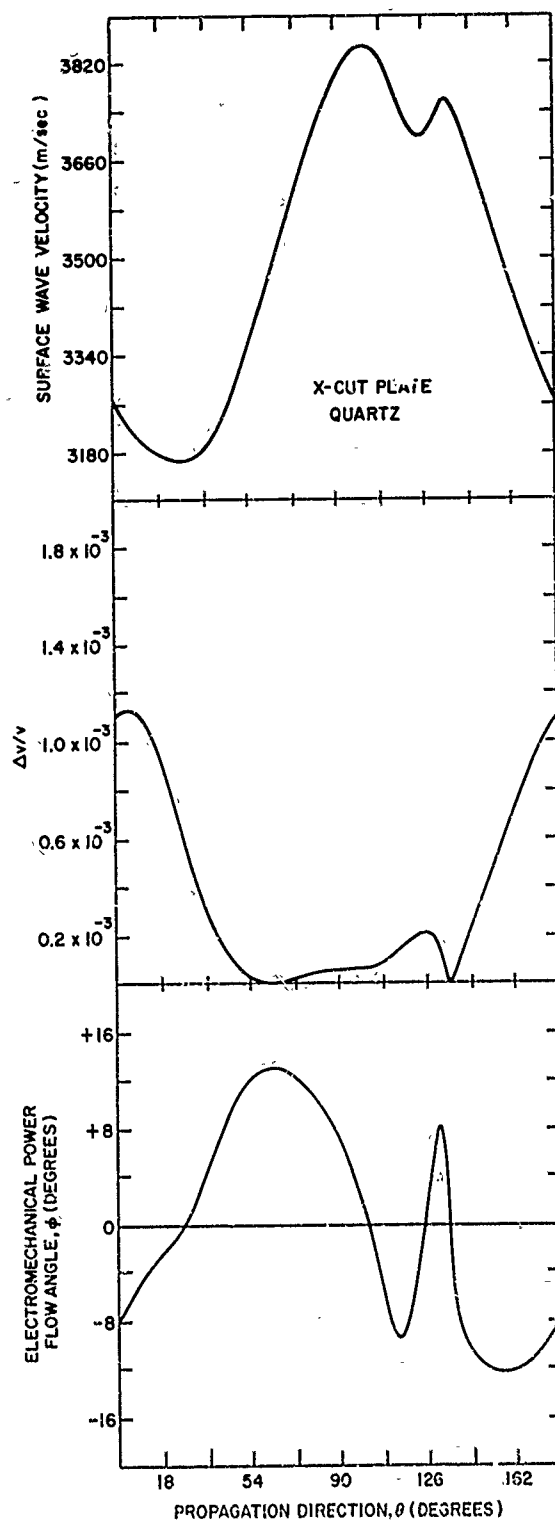


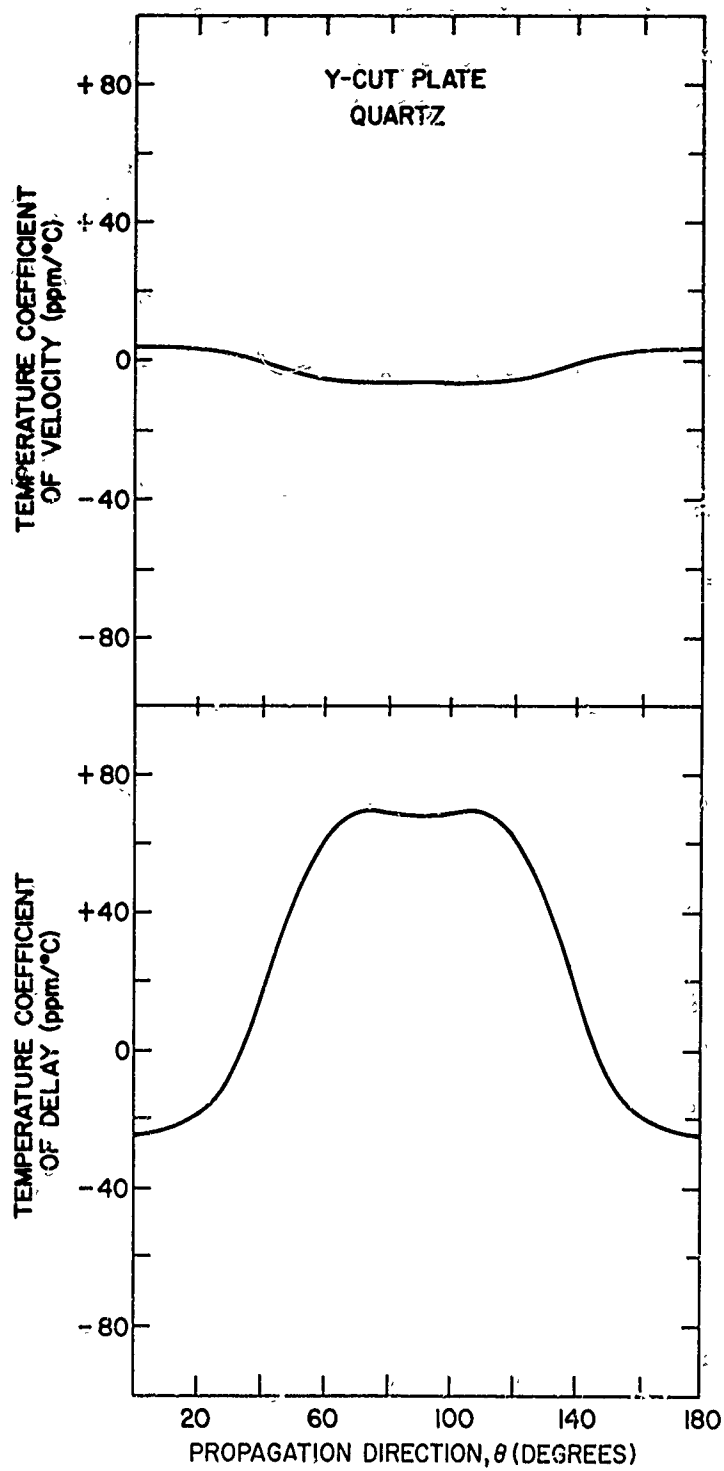


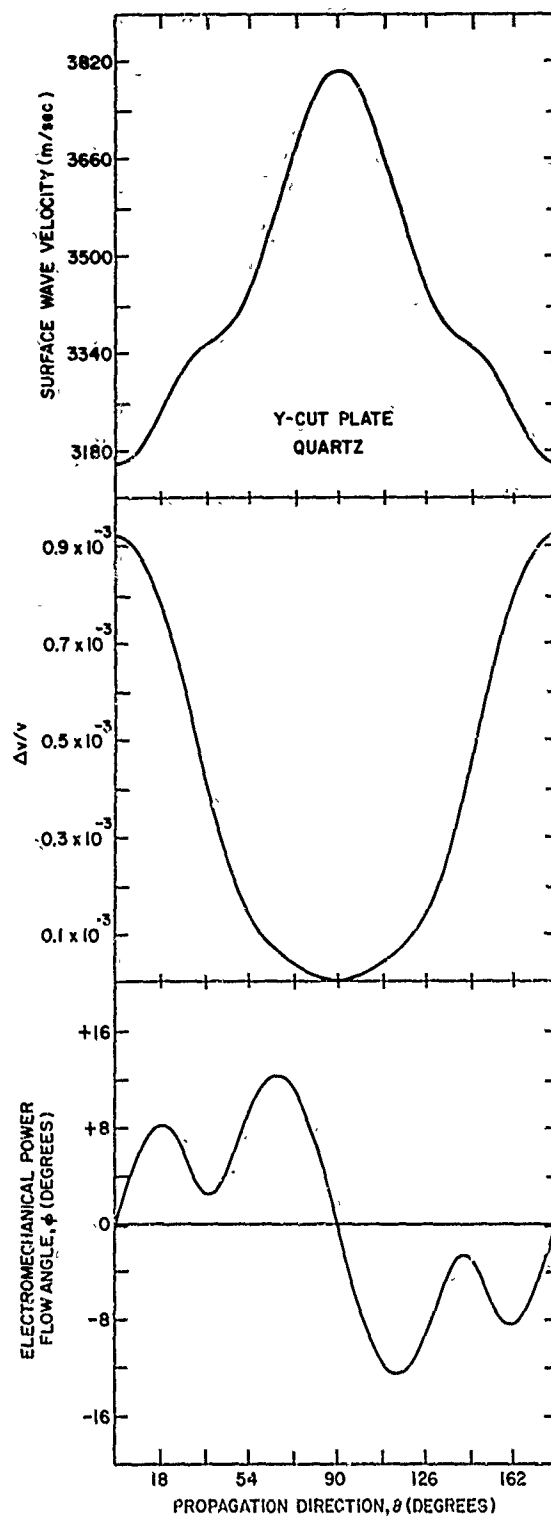


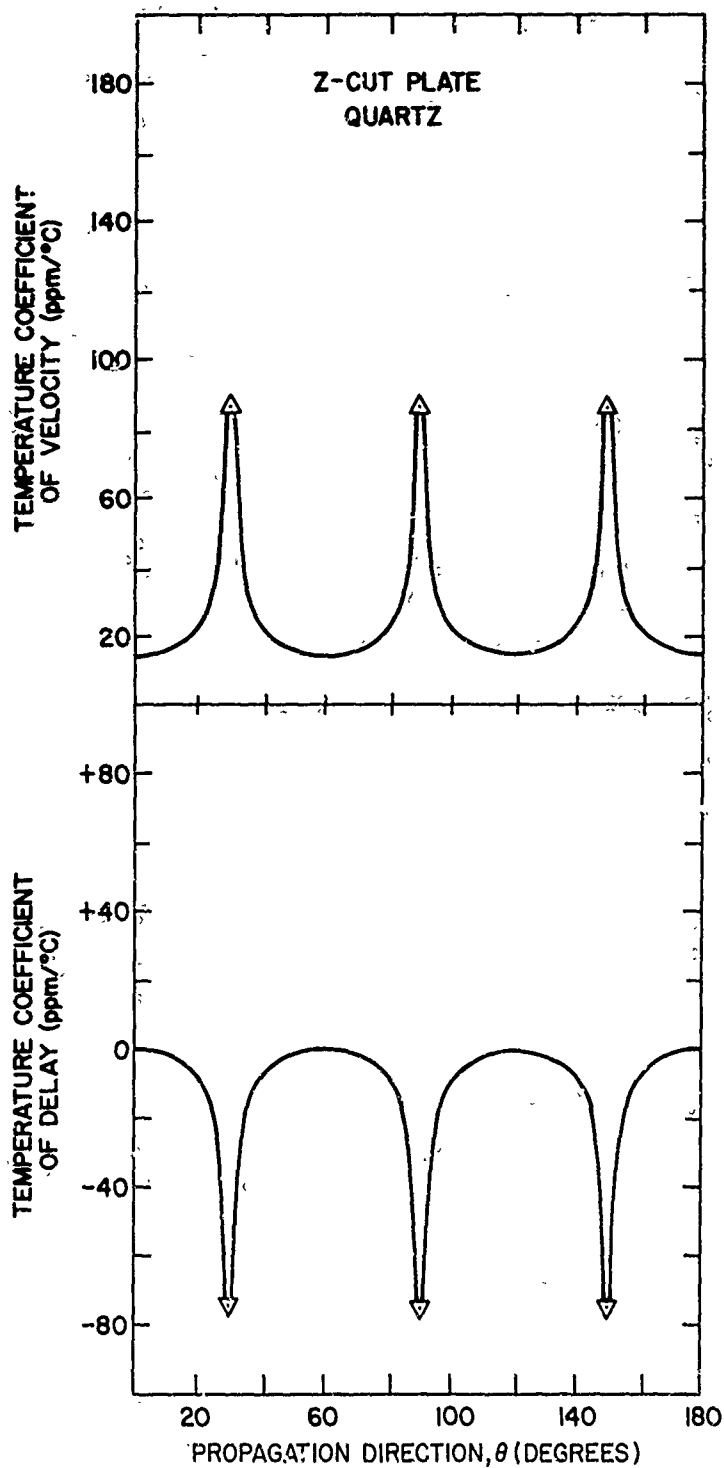






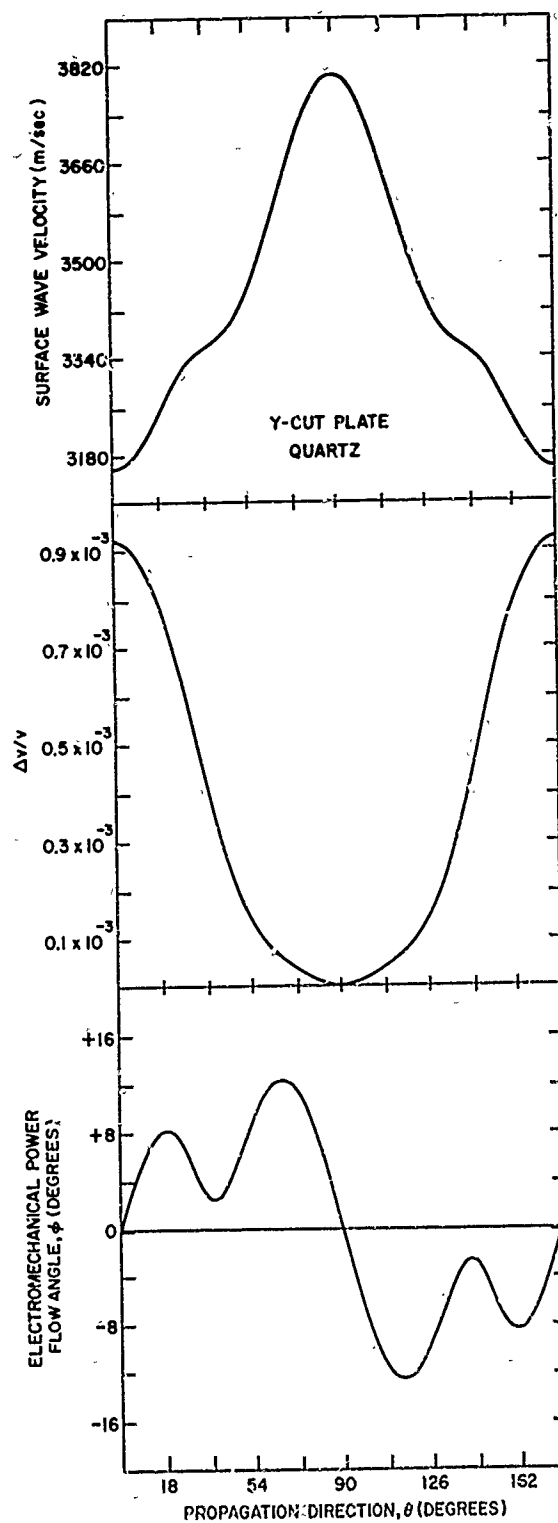


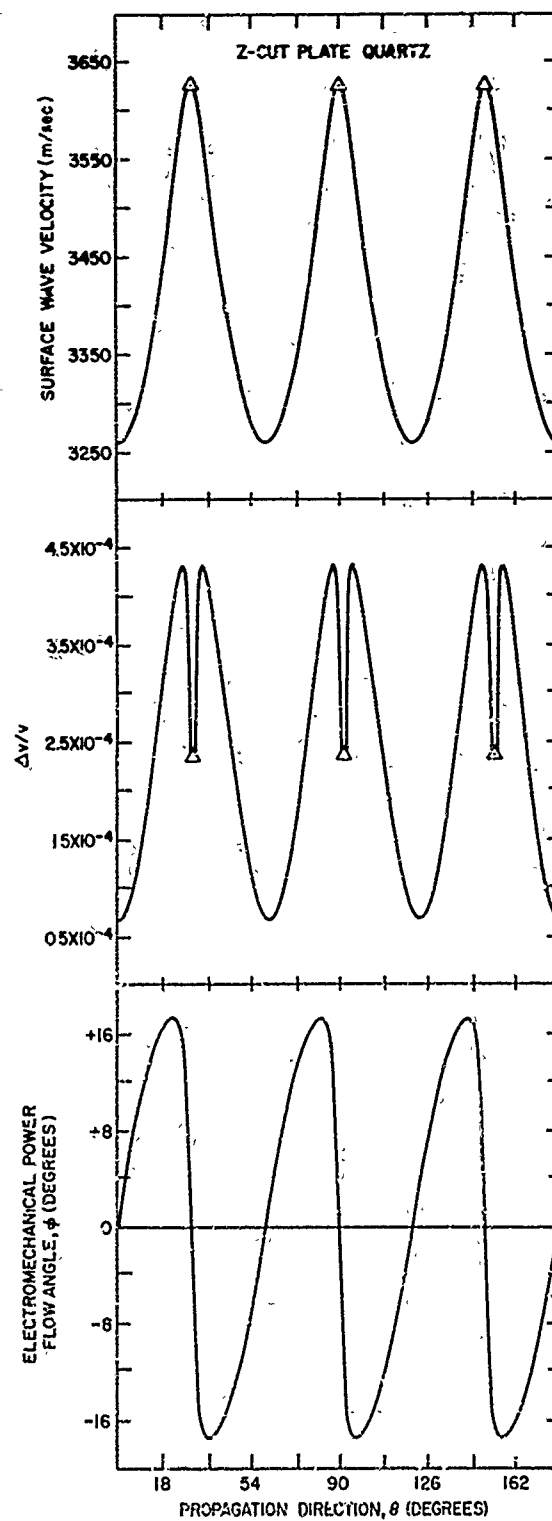




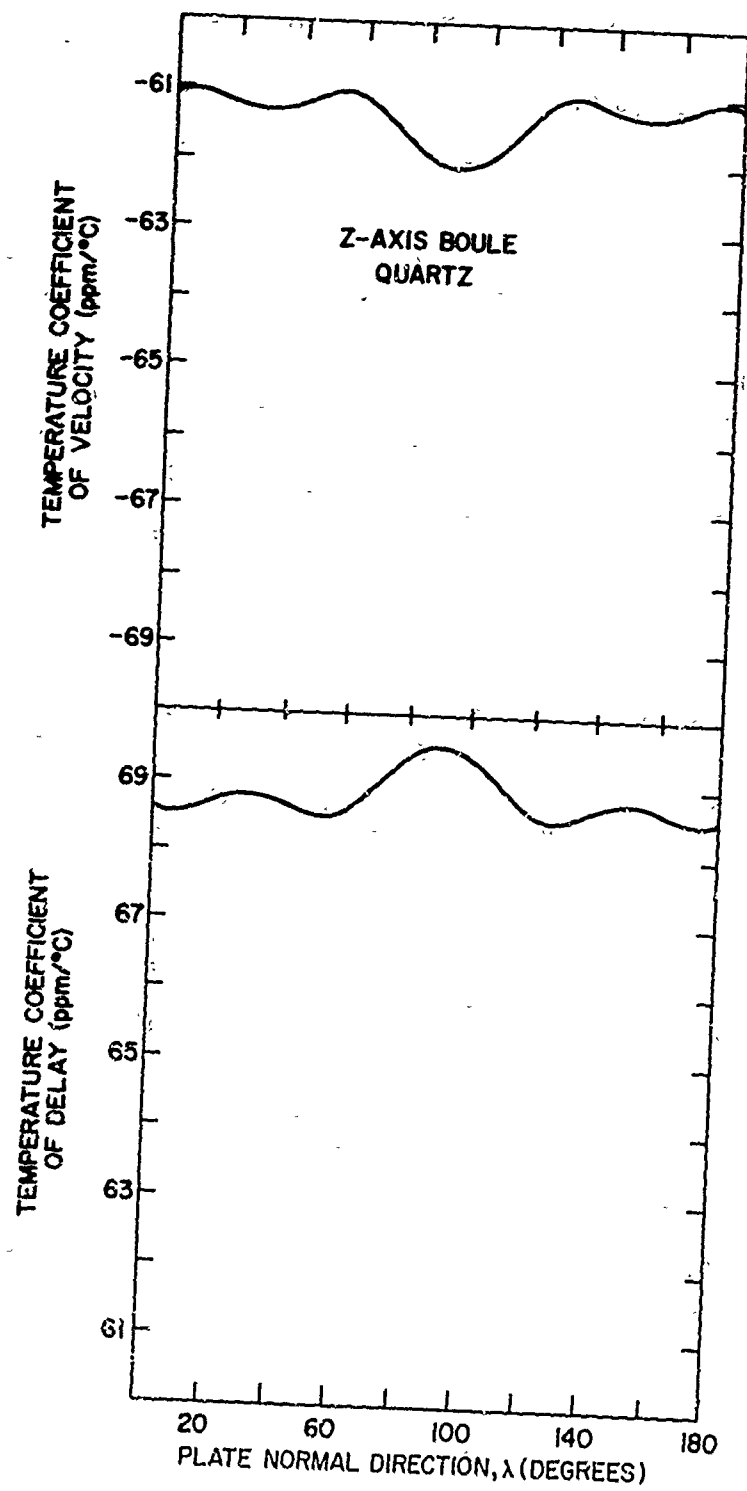
NOTE: FOR SIGNIFICANCE OF THE  
 $\Delta$  SEE FACING PAGE.

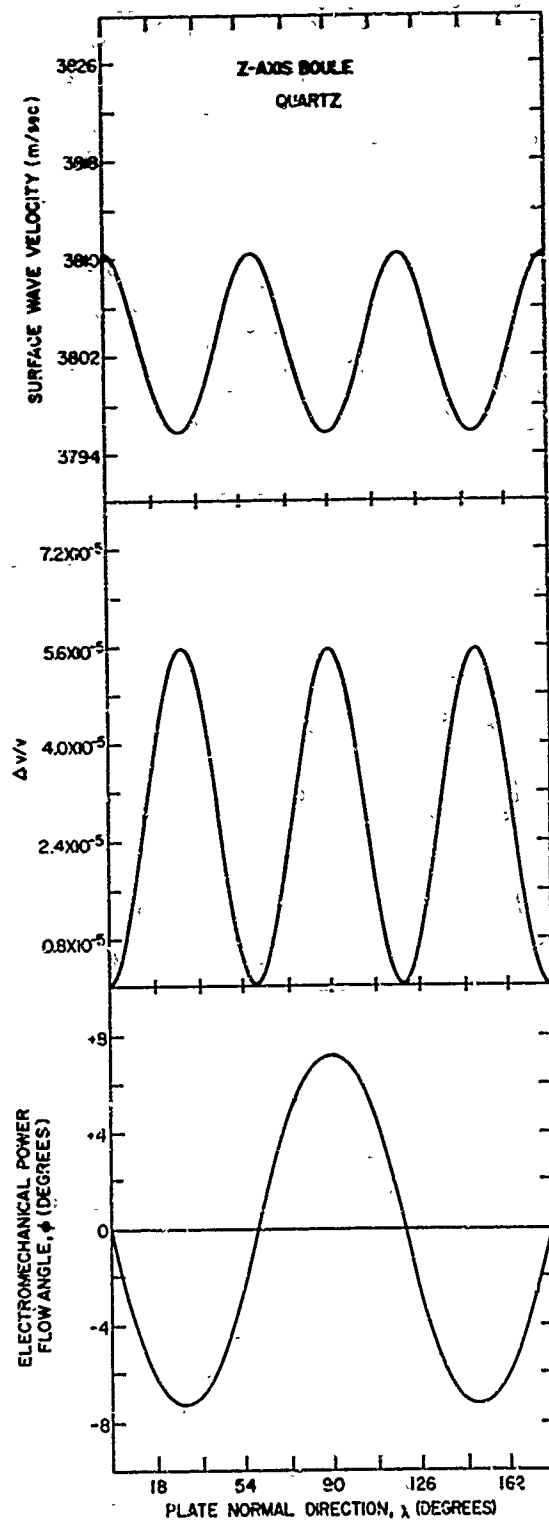


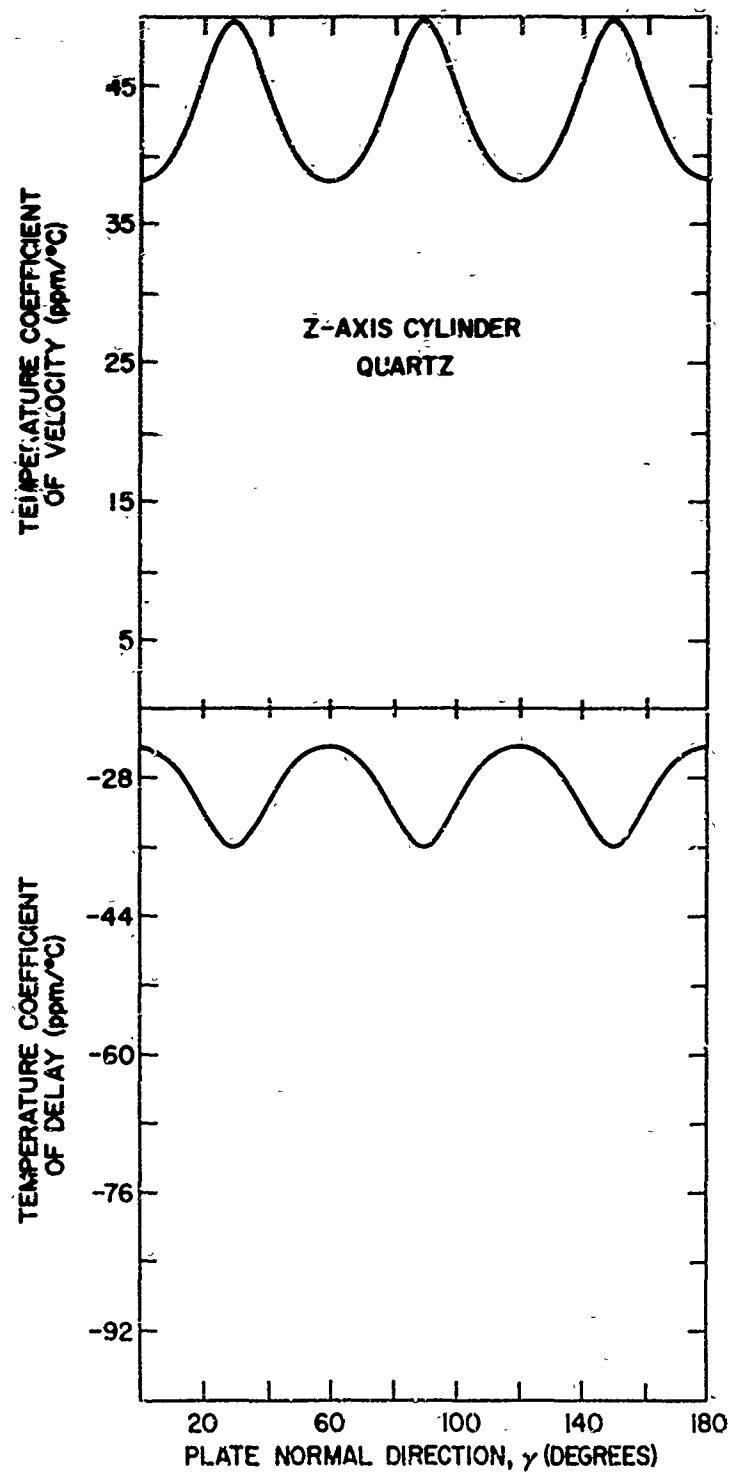


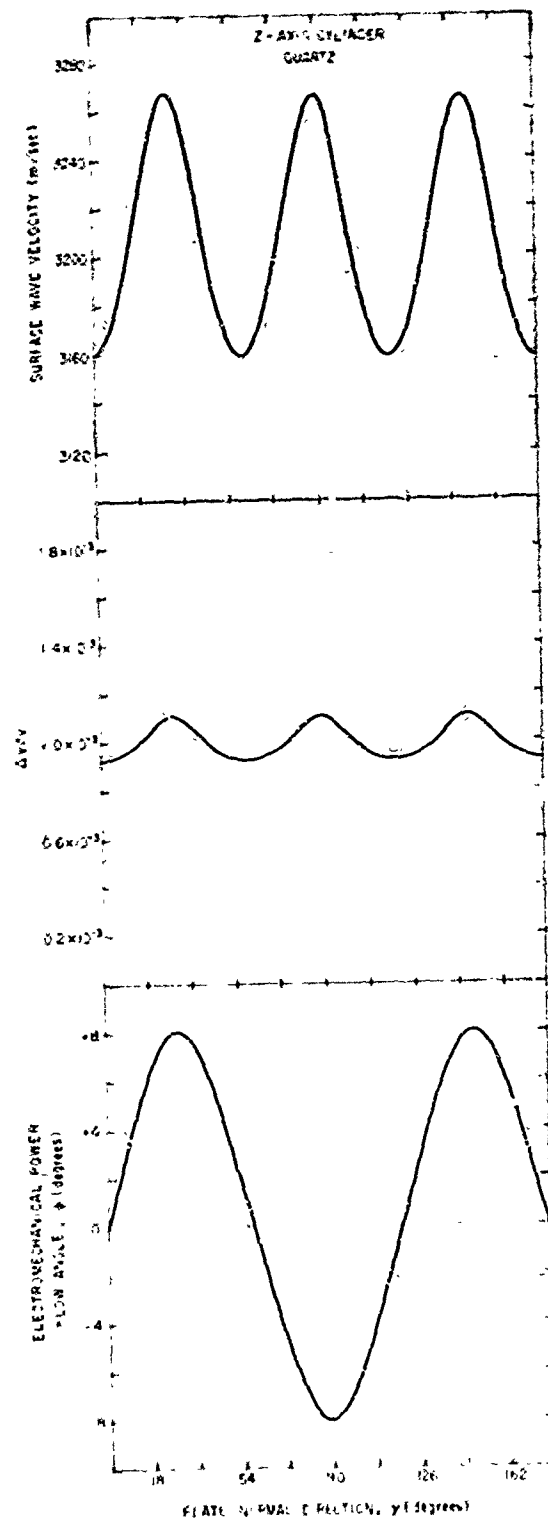


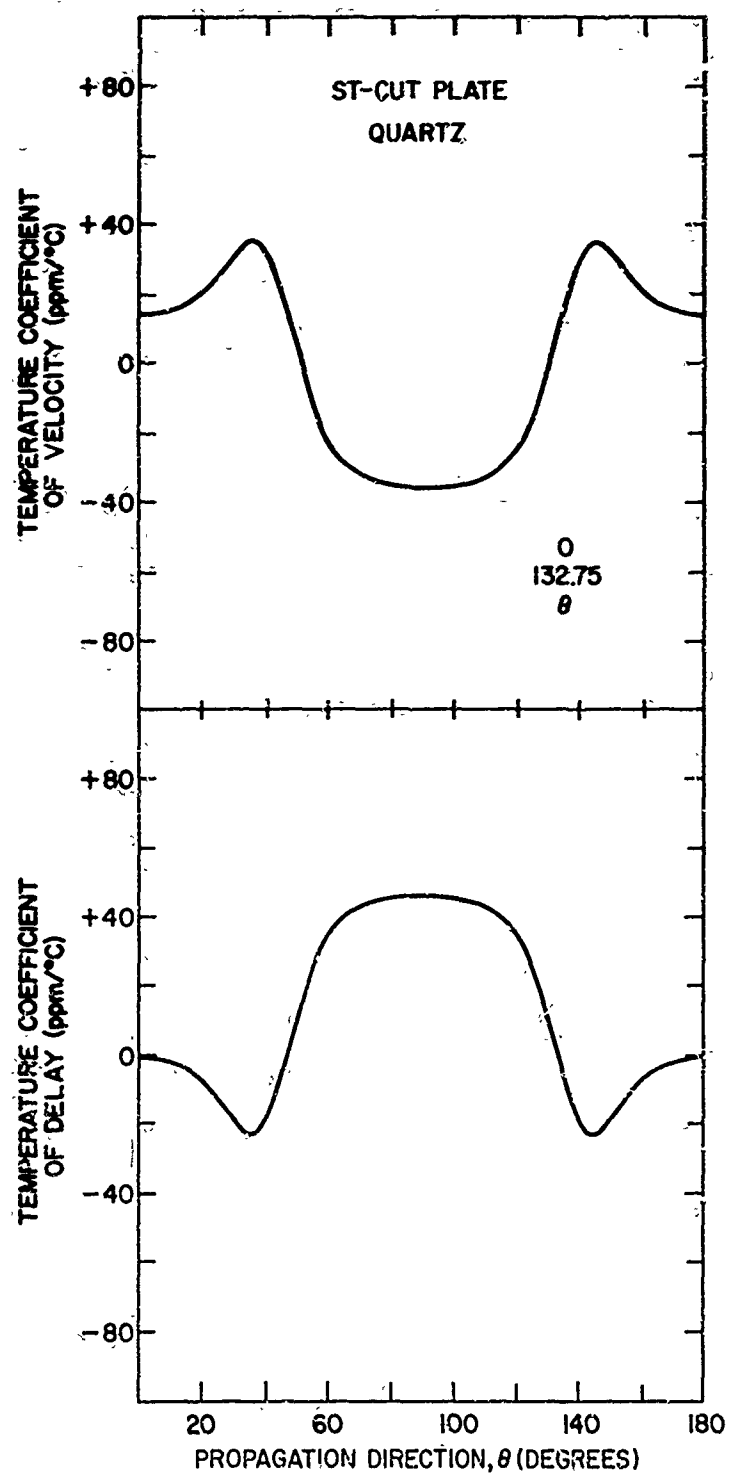
△NOTE AT  $\theta = 45^\circ, 90^\circ$  AND  $135^\circ$  THE SURFACE WAVE DEGENERATES INTO A TILTED BULK WAVE. HOWEVER, A RAYLEIGH LIKE WAVE LIES AT 368507 M/SEC ON THE PSEUDO SURFACE WAVE BRANCH. (SEE FARNELL, 1970)

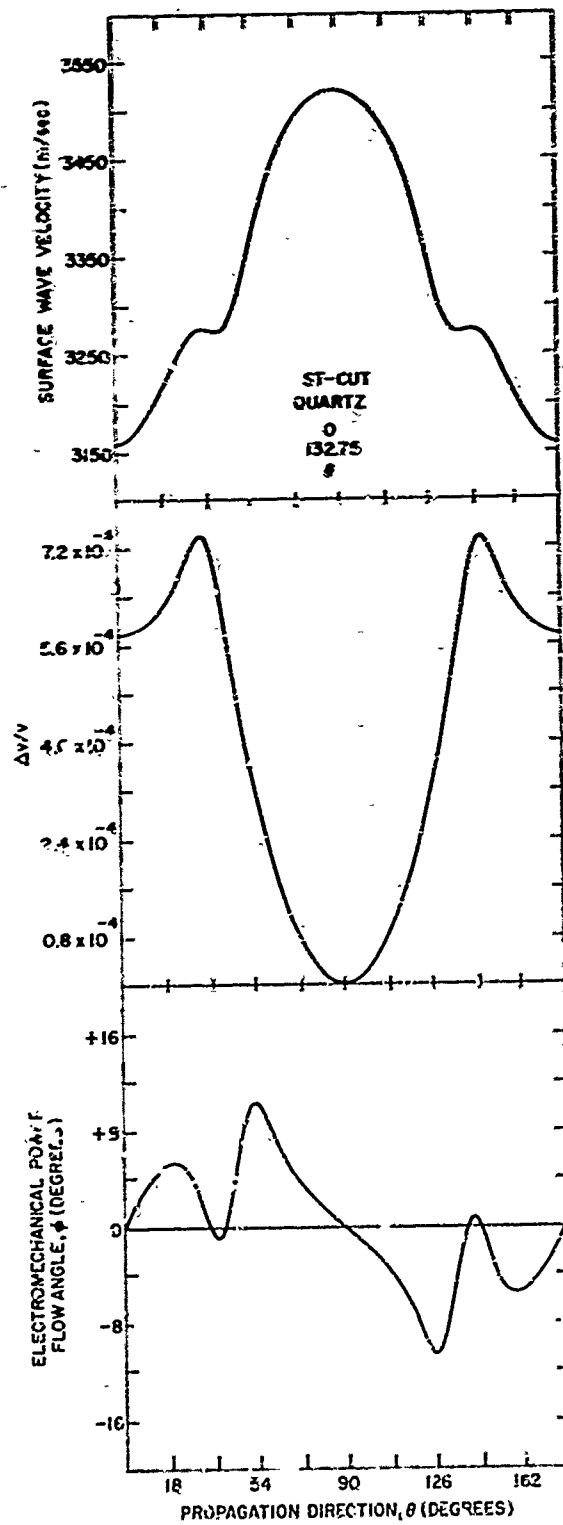




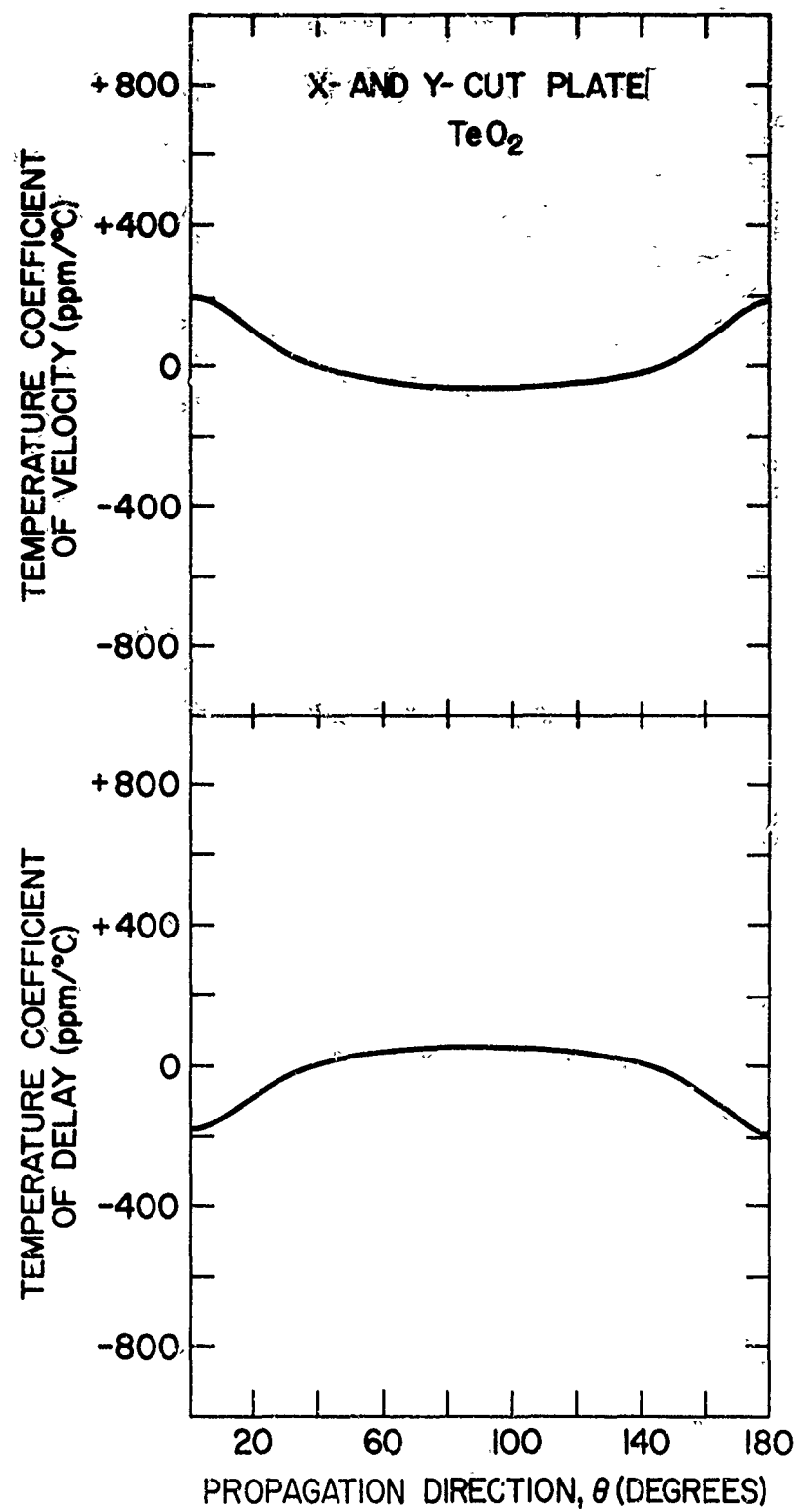


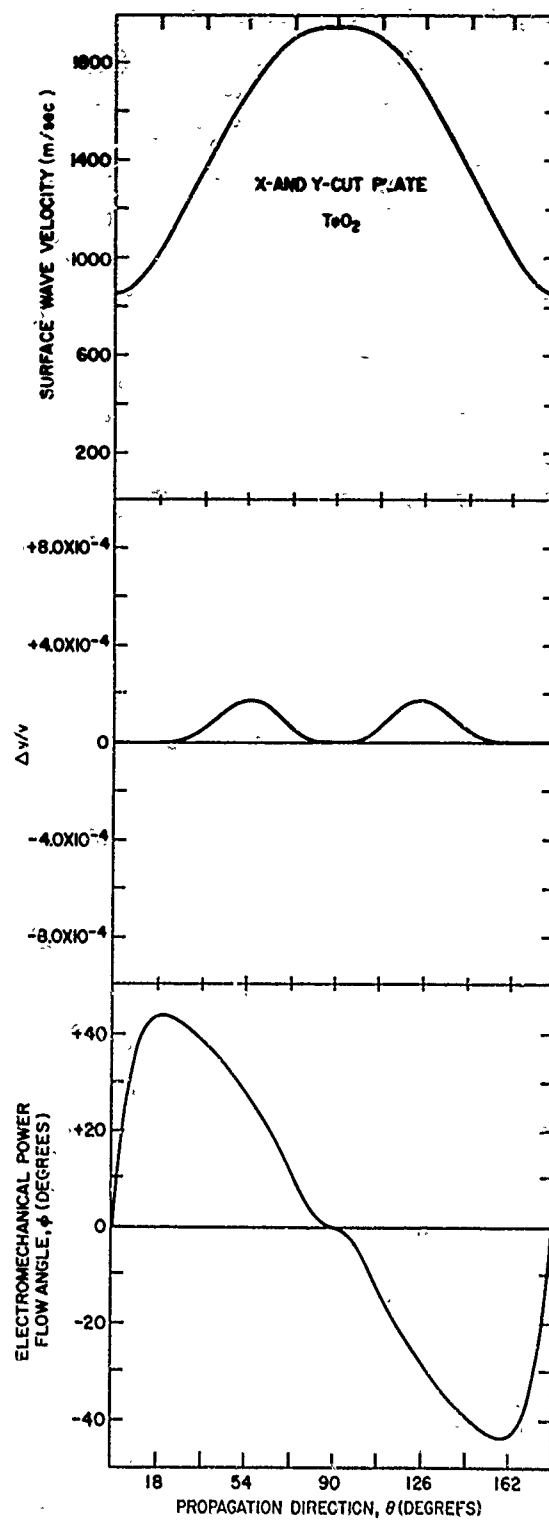


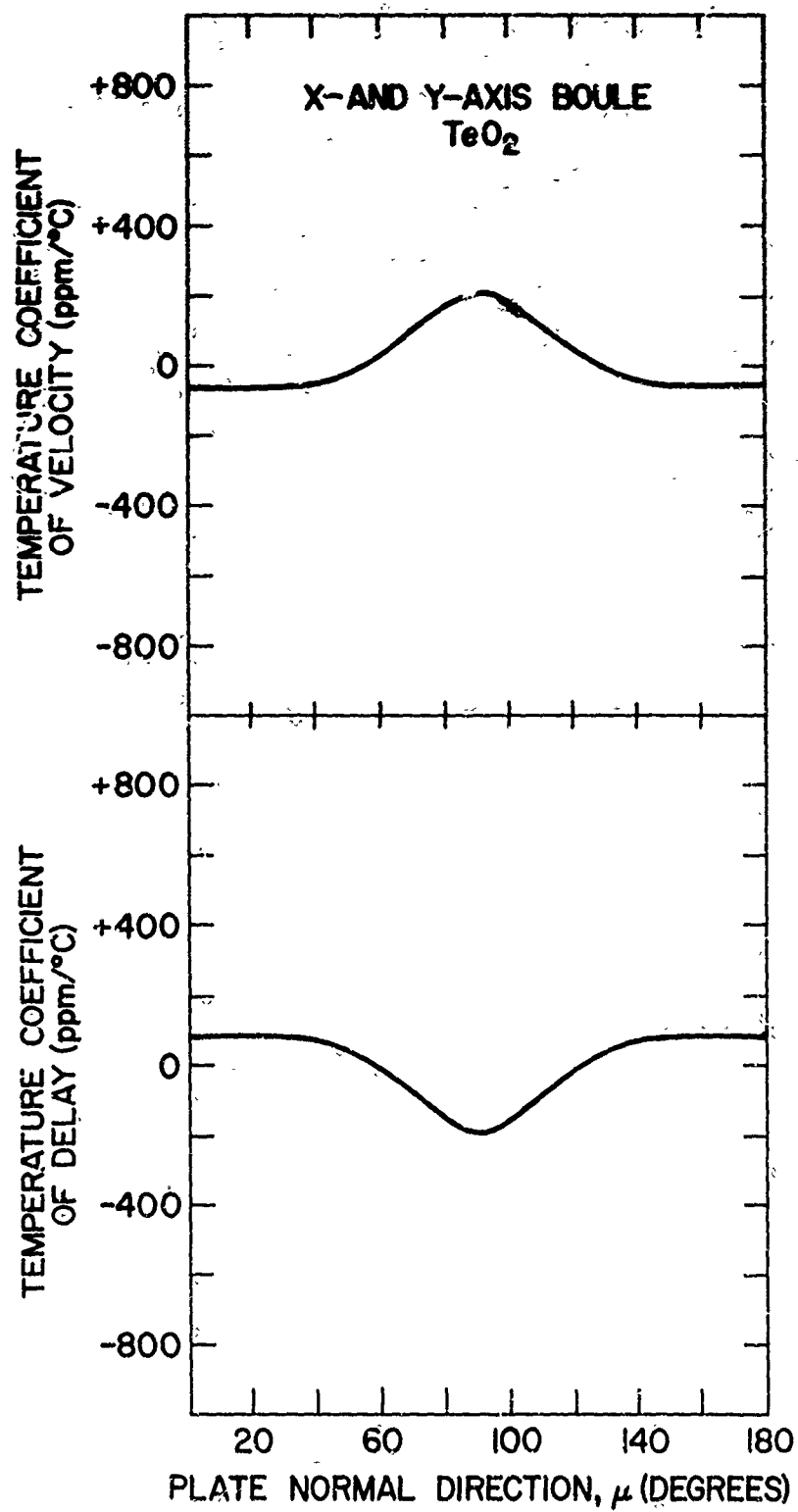


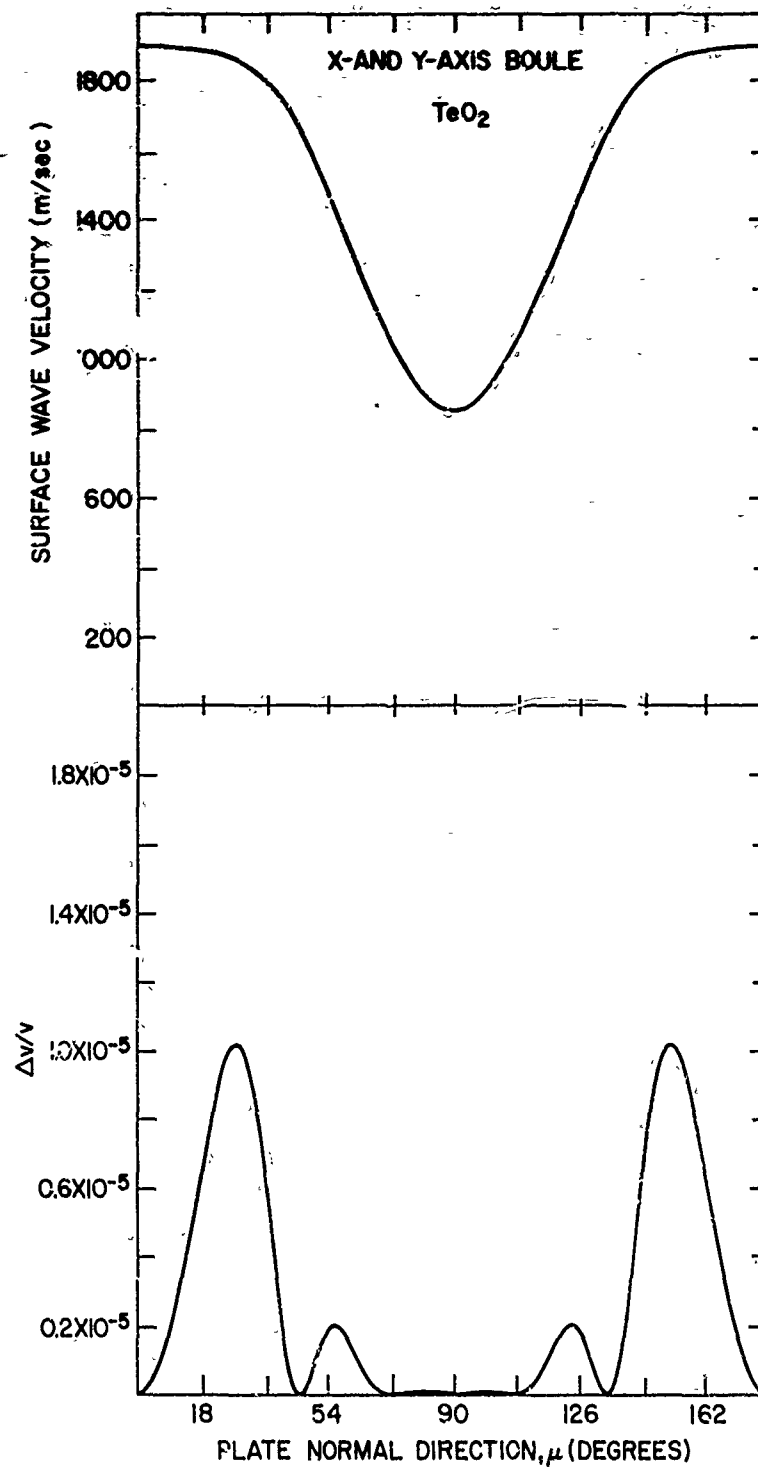




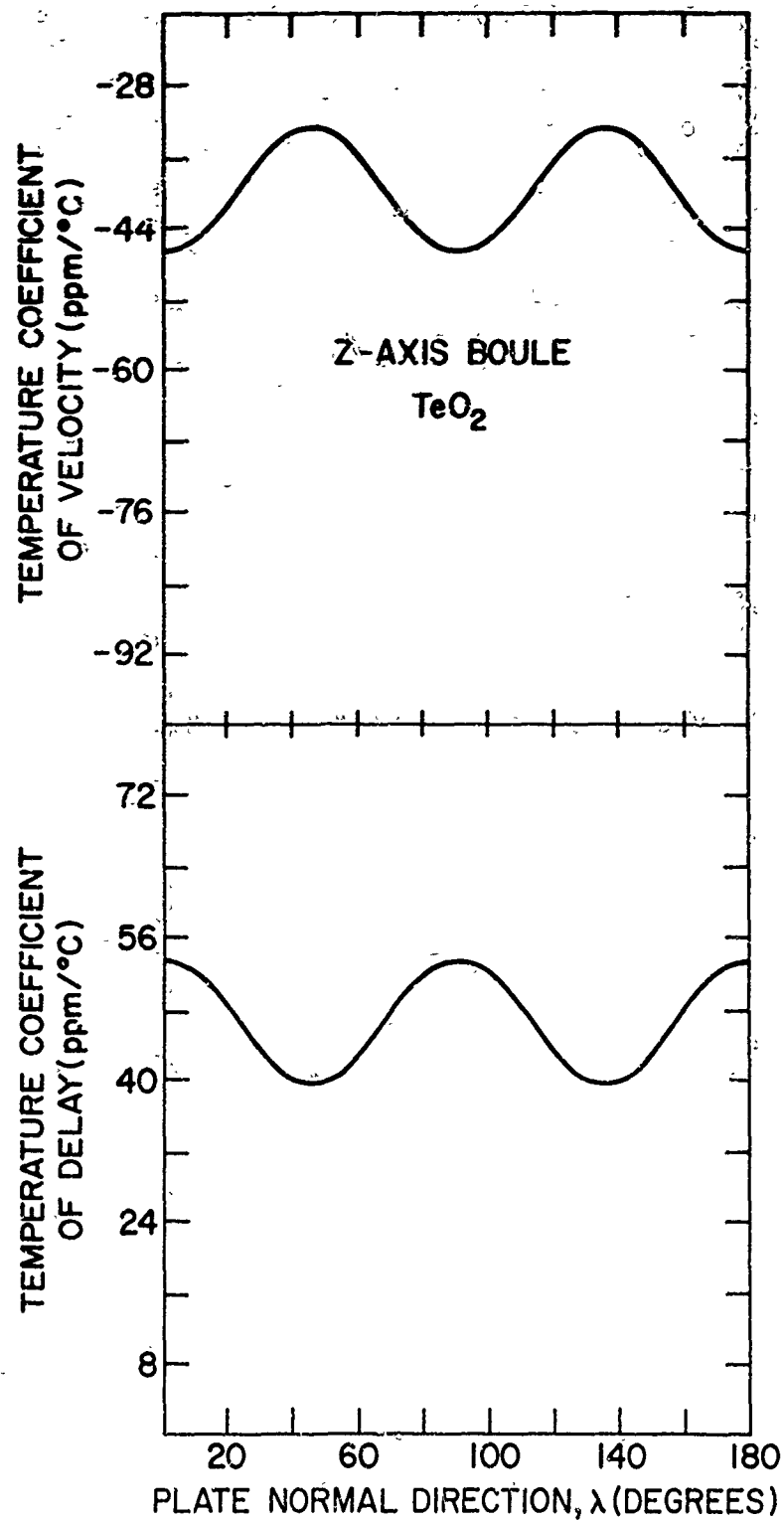


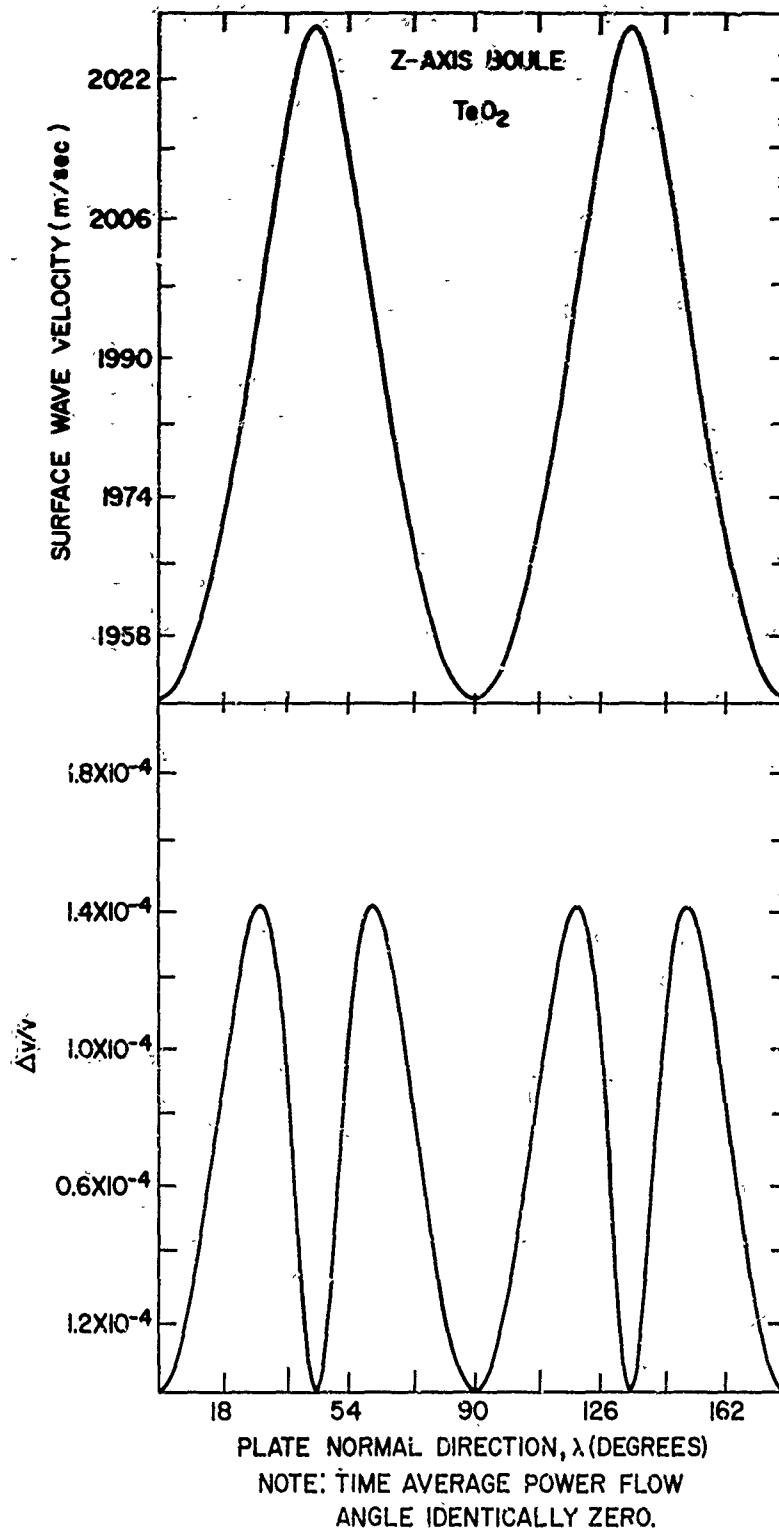






NOTE: TIME AVERAGE POWER FLOW  
ANGLE IDENTICALLY ZERO.





#### 4. SUMMARY AND CONCLUSIONS

Analysis of the data presented in section 3 yields several interesting surface wave orientations, the more significant of which are listed in Table 1. As expected no zero temperature coefficient of delay cut was found for  $\text{LiNbO}_3$ . However, very fortuitously, the  $41\frac{1}{2}^\circ$  rotated cut, X propagating orientation (Slobodnik and Conway, 1970b) previously determined to yield excellent, low loss, wide bandwidth devices also possesses the lowest temperature coefficient of delay yet found on this material.

The biggest disappointment was  $\text{LiTaO}_3$  since, contrary to expectations no zero temperature orientation was found here either. The absolute lowest value of 23 ppm was unfortunately associated with an orientation having some  $1.55^\circ$  of beam steering (Schulz and Holland, 1971). As can also be seen from Table 1, the sacrifice of several parts per million in temperature dependence yields two pure mode axes orientations having velocities of 3300 m/sec. Both of these cuts also have moderately high coupling ( $\Delta v/v$ ). The next to last orientation given in the  $\text{LiTaO}_3$  column is listed not for its low temperature coefficient but for its very high coupling which is substantially higher than any previously known.

For an exhaustive list of the zero temperature cuts of quartz, the reader is referred to Schulz, Matsinger and Holland (1970). Table 1 merely gives the popular ST cut along with ZX orientation not mentioned by Schulz et al (1970).

It is the two  $\text{TeO}_2$  orientations given in Table 1 which show the most unusual and perhaps the most potentially useful properties. Shown here for the first time is a simultaneous combination of zero temperature coefficient of delay, zero power flow-angle,  $\phi$  and ultra-low surface wave velocity. This last property allows, of course, long time delays in short spaces and the consequent reduction in size and weight. The low coupling associated with these orientations will probably require enhancement through thin films (Solie, 1971; Reeder et al, 1971; and Smith, 1971) or surface wave generation schemes other than interdigital transducers (Bertoni, 1969; Li and Yen, 1971; and Bertoni and Tamir, 1971). In addition, the high acoustic propagation loss (Ohmachi and Uchida, 1970) of  $\text{TeO}_2$  will probably limit its use to the VHF frequency range.

Table 1. Summary of Data of Temperature Coefficients of Velocity and Delay for Newly Discovered Orientations of Interest as Well as Many Popular Surface Wave Cuts

Material	Orientation	Euler Angles	Rotated Constants	Velocity (m/sec)	$\Delta v/v_\infty$	$\frac{1}{v} \frac{\partial v}{\partial T}$ (ppm/°C)	$\frac{1}{v} \frac{\partial \tau}{\partial T}$ (ppm/°C)	$\theta$ (Degrees)
LiNbO <sub>3</sub>	41-1/2,X	0,41-1/2,0	-	4000	0.0277	-57	72	0
	Y,Z	0,90,90	-	3488	0.0241	-87	94	0
	16-1/2 Double Rotated	0,73-1/2,90	-	3503	0.0268	-88	96	0
LiTaO <sub>3</sub>	-	90,90,112	-	3295	0.0035	-17	23	1.55
	-	90,90,119.5	-	3300	0.0037	-24	30	0
	-	0,33,0	0,22,20.5	3300	0.0045	-17	33	0
	Y,Z	0,90,90	-	3230	0.0033	-31	35	0
	-	0,78.5,90	-	3260	0.0040	-25	41	0
	-	0,179.5,0	0,22,20.5	3391	0.0084	-42	58	0
	Z,Y	0,0,90	-	3329	0.0059	-52	69	0
Quartz	Z,X	0,0,0	-	3260	0.00006	14	0	0
	ST,X	0,132-3/4,0	-	3158	0.00058	14	0	0
TeO	-	90,90,39	-	1424	0.00008	14	0	0
	-	0,58.2,0	-	1387	0.00002	20	0	0



## Acknowledgments

The author is deeply indebted to B.J. Welch of RDP, Inc. for his very capable and extensive computer programming assistance. Without him this report could not have been written. Mr. Welch was supported by the Analysis and Simulation Branch of AFCRL under contract and the author wishes to thank Miss E. Cronin, Chief of that branch, and Mr. P. Tsipouras for their assistance. The author also wishes to thank J.J. Campbell and W.R. Jones of the Hughes Aircraft Company for providing a copy of their basic velocity calculating program. The author also gratefully acknowledges the programming assistance of R.W. Mack and finally wishes to thank M. B. Schulz of the Raytheon Company for bringing the material  $\text{TeO}_2$  to his attention.

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## Appendix A

### Material Constants and Their Temperature Coefficients

This appendix presents the material constants, the normalized temperature coefficients of the material constants, and the temperature coefficients of thermal expansion for  $\text{LiNbO}_3$ ,  $\text{LiTaO}_3$ , quartz and  $\text{TeO}_2$ . All of the values for  $\text{LiNbO}_3$  and  $\text{LiTaO}_3$  were taken directly from Smith and Welsh (1971) except the temperature coefficient of density which was calculated from the coefficients of thermal expansion using the technique outlined in Appendix B. The values for quartz were taken directly from either Beckmann et al (1962) or from Zelenka and Lee (1971). The values for  $\text{TeO}_2$  were taken from Ohmachi and Uchida (1970).

It should be noted that the velocity,  $\Delta v/v$ , and power flow angle calculations of Section 3 for  $\text{LiNbO}_3$  and  $\text{LiTaO}_3$  were taken from the Microwave Acoustics Handbook (Slobodnik, 1972) and therefore were made using the material constants given by Warner et al (1967).

Table A1. Temperature Coefficients of Material Constants. Material:  $\text{LiNbO}_3$ ; Crystal Group: 3m; References: Smith and Welsh (1971).

		Room Temperature (25°C) Value of Constant, X	Normalized Temperature Coefficients	
			First Order, $\frac{1}{X} \frac{\partial X}{\partial T} = a_1$	Second Order $\frac{1}{2X} \frac{\partial^2 X}{\partial T^2} = a_2$
Elastic Constants	$c_{11}^E$	$2.080 \times 10^{11} \text{ N/m}^2$	$-1.74 \times 10^{-4}/^\circ\text{C}$	-
	$c_{12}^E$	0.573	-2.52	-
	$c_{13}^E$	0.752	-1.59	-
	$c_{14}^E$	0.085	-2.14	-
	$c_{33}^E$	2.424	-1.53	-
	$c_{44}^E$	0.595	-2.04	-
	$c_{66}^E$	0.7285	-1.43	-
Piezo- electric Constants	$e_{15}$	$3.76 \text{ C/m}^2$	1.47	-
	$e_{22}$	2.43	0.79	-
	$e_{31}$	0.23	2.21	-
	$e_{33}$	1.33	8.87	-
Dielectric Constants	$\epsilon_{11}^S$	$39.2 \times 10^{-11} \text{ F/m}$	3.23	-
	$\epsilon_{33}^S$	24.7	6.27	-
Density	$\rho$	$4.64 \times 10^3 \text{ kg/m}^3$	-0.383	-

Table A2. Temperature Coefficients of Thermal Expansion. Material:  $\text{LiNbO}_3$ ; Crystal Group: 3m; References: Smith and Welsh (1971)

		Temperature Coefficients (25°C)	
		First Order	Second Order
Thermal Expansion	$\alpha_{11}$	$0.154 \times 10^{-4}/^\circ\text{C}$	$0.053 \times 10^{-7}/(^\circ\text{C})^2$
	$\alpha_{33}$	0.075	-0.077

Table A3. Temperature Coefficients of Material Constants. Material:  $\text{LiTaO}_3$ ; Crystal Group: 3m; References: Smith and Welsh (1971).

		Room Temperature (25°C) Value of Constant, X	Normalized Temperature Coefficients	
			First Order, $\frac{1}{X} \frac{\partial X}{\partial T} = a_1$	Second Order $\frac{1}{2X} \frac{\partial^2 X}{\partial T^2} = a_2$
Elastic Constants	$c_{11}^E$	$2.298 \times 10^{11} \text{ N/m}^2$	$-1.03 \times 10^{-4}/^\circ\text{C}$	$0.77 \times 10^{-7}/(^\circ\text{C})^2$
	$c_{12}^E$	0.440	-3.41	-1.18
	$c_{13}^E$	0.812	-0.50	6.00
	$c_{14}^E$	-0.104	6.67	16.7
	$c_{33}^E$	2.798	-0.96	-3.21
	$c_{44}^E$	0.968	-0.43	1.67
	$c_{66}^E$	0.929	-0.47	1.24
Piezo- electric Constants	$e_{15}$	$2.72 \text{ C/m}^2$	-1.32	-7.17
	$e_{22}$	1.67	-0.60	-6.28
	$e_{31}$	-0.38	0.87	51.8
	$e_{33}$	1.09	1.54	1.41
Dielectric Constants	$\epsilon_{11}^S$	$37.7 \times 10^{-11} \text{ F/m}$	3.29	4.28
	$\epsilon_{33}^S$	37.9	11.6	78.0
Density	$\rho$	$7.454 \times 10^3 \text{ kg/m}^3$	-0.363	-

Table A4. Temperature Coefficients of Thermal Expansion. Material:  $\text{LiTaO}_3$ ; Crystal Group: 3m; References: Smith and Welsh (1971).

		Temperature Coefficients (25°C)	
		First Order	Second Order
Thermal Expansion	$\alpha_{11}$	$0.161 \times 10^{-4}/^\circ\text{C}$	$0.070 \times 10^{-7}/(^\circ\text{C})^2$
	$\alpha_{33}$	0.041	-0.100

Table A5. Temperature Coefficients of Material Constants. Material: Quartz; Crystal Group: 32; References: Bechmann et al (1962) and Zelenka and Lee (1971).

		Room Temperature (25°C) Value of Constants, X	Normalized Temperature Coefficients	
			First Order, $\frac{1}{X} \frac{\partial X}{\partial T} = a_1$	Second Order $\frac{1}{2X} \frac{\partial^2 X}{\partial T^2} = a_2$
Elastic Constants	$c_{11}^E$	$8.674 \times 10^{10} \text{ N/m}^2$	$-0.443 \times 10^{-4}/^\circ\text{C}$	-
	$c_{12}^E$	0.699	-26.90	-
	$c_{13}^E$	1.191	-5.50	-
	$c_{14}^E$	-1.791	1.17	-
	$c_{33}^E$	10.72	-1.60	-
	$c_{44}^E$	5.794	-1.754	-
	$c_{66}^E$	3.9875	1.876	-
Density	$\rho$	$2.65 \times 10^3 \text{ kg/m}^3$	$-34.92 \times 10^{-6}/^\circ\text{C}$	$-15.9 \times 10^{-9}/(^\circ\text{C})^2$

Table A6. Temperature Coefficients of Thermal Expansion. Material: Quartz; Crystal Group: 32; References: Bechmann et al (1962).

		Temperature Coefficients (25°C)	
		First Order	Second Order
Thermal Expansion	$\alpha_{11}$	$13.71 \times 10^{-6}/^\circ\text{C}$	$6.5 \times 10^{-9}/(^\circ\text{C})^2$
	$\alpha_{33}$	7.48	2.9

Table A7. Temperature Coefficients of Material Constants. Material:  $\text{TeO}_2$ ; Crystal Group: 422; References: Ohmachi and Uchida (1970).

		Room Temperature (20°C) Value of Constant, X	Normalized Temperature Coefficients	
			First Order, $\frac{1}{X} \frac{\partial X}{\partial T} = a_1$	Second Order $\frac{1}{2X} \frac{\partial^2 X}{\partial T^2} = a_2$
Elastic Constants	$c_{11}^E$	$5.57 \times 10^{10} \text{ N/m}^2$	$-2.70 \times 10^{-4}/^\circ\text{C}$	-
	$c_{12}^E$	5.12	-3.28	-
	$c_{13}^E$	2.18	-0.54	-
	$c_{14}^E$	0	-	-
	$c_{33}^E$	10.58	-2.81	-
	$c_{44}^E$	2.65	-0.73	1
	$c_{66}^E$	6.59	-4.38	-
Density	$\rho$	$5.99 \times 10^3 \text{ kg/m}^3$	$-46.6 \times 10^{-6}/^\circ\text{C}$	-

Table A8. Temperature Coefficients of Thermal Expansion; Material:  $\text{TeO}_2$ ; Crystal Group: 422; References: Ohmachi and Uchida (1970).

		Temperature Coefficients (20°C)	
		First Order	Second Order
Thermal Expansion	$\alpha_{11}$	$20.0 \times 10^{-6}/^\circ\text{C}$	-
	$\alpha_{33}$	6.6	-



## Appendix B

### The Temperature Coefficient of Density

The temperature coefficient of density can be obtained from the coefficients of thermal expansion as shown below.

By definition the density is the mass per unit volume

$$\rho(T) \equiv \frac{M}{l_1 l_2 l_3} = M l_1^{-1} l_2^{-1} l_3^{-1} \quad (B1)$$

where  $l_1$ ,  $l_2$ , and  $l_3$  are unit lengths along the X, Y and Z crystalline axes, respectively. M is, of course, the mass. Taking the derivative of Eq. (B1) yields

$$\frac{\partial \rho}{\partial T} = M l_1^{-1} \frac{\partial l_2^{-1} l_3^{-1}}{\partial T} + M l_2^{-1} l_3^{-1} \frac{\partial l_1^{-1}}{\partial T} \quad (B2)$$

or

$$\frac{\partial \rho}{\partial T} = M l_1^{-1} l_2^{-1} \frac{\partial l_3^{-1}}{\partial T} + M l_1^{-1} l_3^{-1} \frac{\partial l_2^{-1}}{\partial T} + M l_2^{-1} l_3^{-1} \frac{\partial l_1^{-1}}{\partial T}. \quad (B3)$$

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This is also equivalent to

$$\frac{\partial \rho}{\partial T} = -M l_1^{-1} l_2^{-1} l_3^{-2} \frac{\partial l_3}{\partial T} - M l_1^{-1} l_3^{-1} l_2^{-2} \frac{\partial l_2}{\partial T} - M l_2^{-1} l_3^{-1} l_1^{-2} \frac{\partial l_1}{\partial T}. \quad (B4)$$

Grouping terms yields

$$\frac{\partial \rho}{\partial T} = -M l_1^{-1} l_2^{-1} l_3^{-1} \left[ \frac{1}{l_3} \frac{\partial l_3}{\partial T} + \frac{1}{l_2} \frac{\partial l_2}{\partial T} + \frac{1}{l_1} \frac{\partial l_1}{\partial T} \right]. \quad (B5)$$

Thus

$$\frac{1}{\rho} \frac{\partial \rho}{\partial T} = - \left[ \frac{1}{l_1} \frac{\partial l_1}{\partial T} + \frac{1}{l_2} \frac{\partial l_2}{\partial T} + \frac{1}{l_3} \frac{\partial l_3}{\partial T} \right]. \quad (B6)$$

Or by definition of the thermal expansion coefficients

$$\frac{1}{\rho} \frac{\partial \rho}{\partial T} = - \left[ \alpha_{11} + \alpha_{22} + \alpha_{33} \right]. \quad (B7)$$

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## Appendix C

Material Constants at 15°C, 25°C and 35°C

This appendix presents, in tabular form, the independent material constants of  $\text{LiNbO}_3$ ,  $\text{LiTaO}_3$ , quartz and  $\text{TeO}_2$  at 15°C, 25°C and 30°C (10°C, 20°C and 30°C for  $\text{TeO}_2$ ). These quantities were computed using Eq. (3) along with the temperature coefficients listed in Appendix A.

Table C1. Independent Elastic (in  $10^{11}$  N/m<sup>2</sup>), Dielectric (in  $10^{-11}$  F/m), and Piezoelectric (in C/m<sup>2</sup>) Constants of LiNbO<sub>3</sub> at Various Temperatures. Density (in  $10^3$  kg/m<sup>3</sup>) is also included. Complete matrices can be obtained using the symmetry of crystal group 3m (see for example Berlincourt et al, 1964).

	Constant	Temperature		
		15°C	25°C	35°C
LiNbO <sub>3</sub>	$c_{11}^E$	2.03353	2.030	2.02647
	$c_{12}^E$	0.574444	0.573	0.571556
	$c_{13}^E$	0.753196	0.752	0.750804
	$c_{14}^E$	0.085182	0.085	0.084818
	$c_{33}^E$	2.42771	2.424	2.42029
	$c_{44}^E$	0.596214	0.595	0.593786
	$c_{66}^E$	0.729542	0.7285	0.727458
	$e_{15}$	3.75447	3.76	3.76553
	$e_{22}$	2.42808	2.43	2.43192
	$e_{31}$	0.229492	0.23	0.230508
	$e_{33}$	1.31820	1.33	1.34180
	$\epsilon_{11}^S$	37.0734	39.2	39.3266
	$\epsilon_{33}^S$	24.5451	24.7	24.8549
	$\rho$	4.64178	4.64	4.63822

Table C2. Independent Elastic (in  $10^{11}$  N/m<sup>2</sup>), Dielectric (in  $10^{-11}$  F/m), and Piezoelectric (in C/m<sup>2</sup>) Constants of LiTaO<sub>3</sub> at Various Temperatures. Density (in  $10^3$  kg/m<sup>3</sup>) is also included. Complete matrices can be obtained using the symmetry of crystal group 3m (see for example Berlincourt et al, 1964).

	Constant	Temperature		
		15°C	25°C	35°C
LiTaO <sub>3</sub>	$c_{11}^E$	2.30038	2.298	2.29565
	$c_{12}^E$	0.441495	0.440	0.438494
	$c_{13}^E$	0.812455	0.812	0.811643
	$c_{14}^E$	-0.103324	-0.104	-0.1047110
	$c_{33}^E$	2.80060	2.798	2.79522
	$c_{44}^E$	0.968432	0.968	0.967600
	$c_{66}^E$	0.929448	0.929	0.928575
	$e_{15}$	2.72340	2.72	2.71621
	$e_{22}$	1.67090	1.67	1.66889
	$e_{31}$	-0.379866	-0.38	-0.380527
	$e_{33}$	1.08834	1.09	1.09169
	$\epsilon_{11}^S$	37.5776	37.7	37.8256
	$\epsilon_{33}^S$	37.4899	37.9	38.3692
	$\rho$	7.45671	7.454	7.45129

Table C3. Independent Elastic (in  $10^{11}$  N/m<sup>2</sup>), Dielectric (in  $10^{-11}$  F/m), and Piezoelectric (in C/m<sup>2</sup>) Constants of Quartz at Various Temperatures. Density (in  $10^3$  kg/m<sup>3</sup>) is also included. Complete matrices can be obtained using the symmetry of crystal groups 32 (see for example Berlincourt et al, 1964).

	Constant	Temperature		
		15°C	25°C	35°C
Quartz	$c_{11}^E$	0.867784	0.8674	0.867016
	$c_{12}^E$	0.071780	0.0699	0.06802
	$c_{13}^E$	0.119755	0.1191	0.118445
	$c_{14}^E$	-0.178890	-0.1791	-0.179310
	$c_{33}^E$	1.073715	1.072	1.070285
	$c_{44}^E$	0.580416	0.5794	0.578384
	$c_{66}^E$	0.398002	0.39875	0.399498
	$e_{11}$	-	0.171	-
	$e_{14}$	-	-0.0406	-
	$\epsilon_{11}^S$	-	3.92	-
	$\epsilon_{33}^S$	-	4.1	-
	$\rho$	2.65092	2.65	2.64907

Table C4. Independent Elastic (in  $10^{11}$  N/m<sup>2</sup>), Dielectric (in  $10^{-11}$  F/m), and Piezoelectric (in C/m<sup>2</sup>) Constants of TeO<sub>2</sub> at Various Temperatures. Density (in  $10^3$  kg/m<sup>3</sup>) is also included. Complete matrices can be obtained using the symmetry of crystal group 422 (see for example Berlincourt et al, 1964).

	Constant	Temperature		
		10°C	20°C	30°C
TeO <sub>2</sub>	$c_{11}^E$	0.5585	0.557	0.5555
	$c_{12}^E$	0.51368	0.512	0.51032
	$c_{13}^E$	0.218118	0.218	0.21788
	$c_{33}^E$	1.0610	1.058	1.0550
	$c_{44}^E$	0.26519	0.265	0.26481
	$c_{66}^E$	0.66189	0.659	0.65611
	$e_{14}$	-	0.216	-
	$\epsilon_{11}^S$	-	20.1	-
	$\epsilon_{33}^S$	-	21.9	-
	$\rho$	5.9928	5.99	5.9872

## Appendix D

### "Rotated Constants" and Euler Angle Notation

The meaning of the "rotated constant" Euler angle notation can best be explained with reference to several examples.

Figure D1 illustrates the standard starting coordinate system in which the propagation axes line up with the crystalline axes X, Y and Z. Thus, one can follow how the standard Euler angle notation  $0, 90, 0$  refers to rotation in the XZ plane, starting with a propagation direction along the X axis and a plate normal along the -Y axis. This is the Y-cut plate illustrated in Figure D2.

If, however, we first rotate through the Euler angles  $45, 90, 35.264$  then the 1 axis, or propagation direction, is initially aligned with the  $[111]$  crystalline axis and the 3 axis or plate normal would lie along the  $[1\bar{1}0]$  crystalline axis. This is illustrated in Figure D3 which also indicates how further rotations can then be accomplished from this starting point. The notation used in the text to describe this situation is illustrated in Figure D4.

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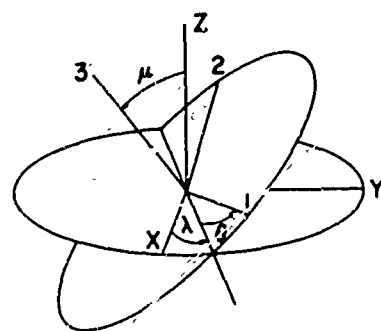
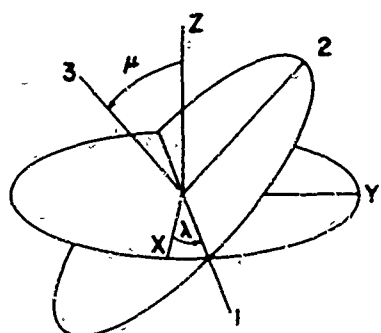
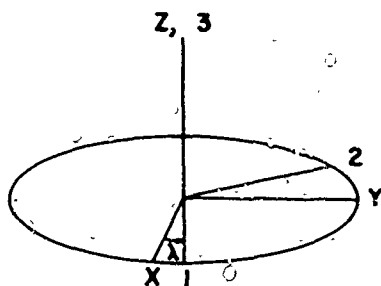


Figure D1. Coordinate System Used to Define Acoustic Surface Wave Propagation. The phase velocity vector lies along the 1 axis while the plate normal lies along the negative 3 axis. The crystalline axes are given by X, Y, and Z while the Euler angles are  $\lambda$ ,  $\mu$ , and  $\theta$  (after H. Goldstein in Classical Mechanics).

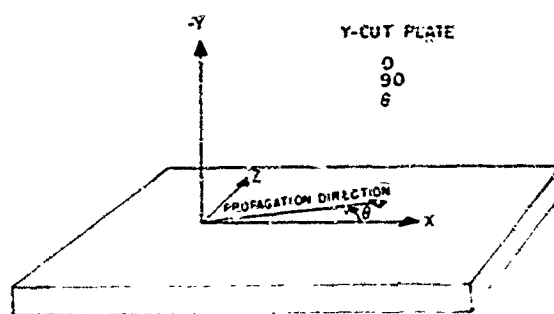


Figure D2. Standard Notation for a Y-cut Plate. Rotation of  $\mu$  through the angle of  $90^\circ$  aligns the plate normal with the (-Y) crystalline axis while the propagation direction remains along the X axis. Further rotations in the plane of the plate are then accomplished through the angle  $\theta$ .

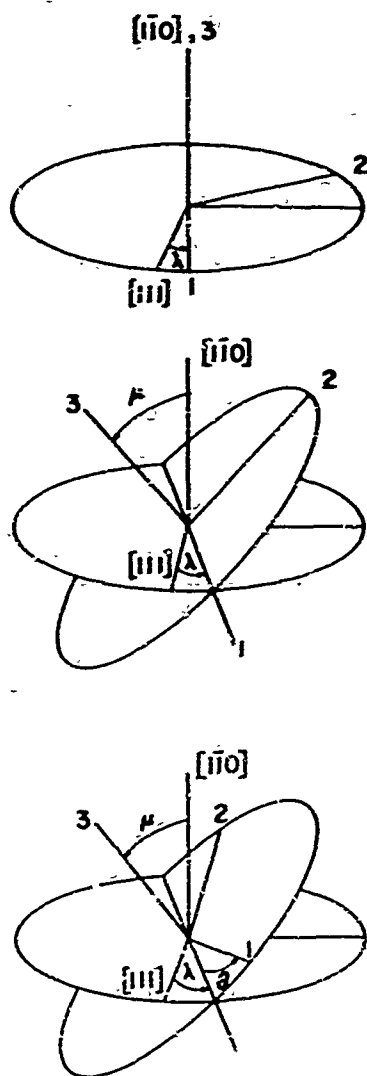


Figure D3. Coordinate System After Initial Rotation Through the Euler Angles 45, 90, 35.264. The phase velocity vector lies along the 1 axis while the plate line axis are given by  $[111]$  and  $[1\bar{1}0]$  while the Euler angles for further rotations from this starting point are  $\lambda$ ,  $\mu$ , and  $\theta$  (after H. Goldstein in Classical Mechanics)

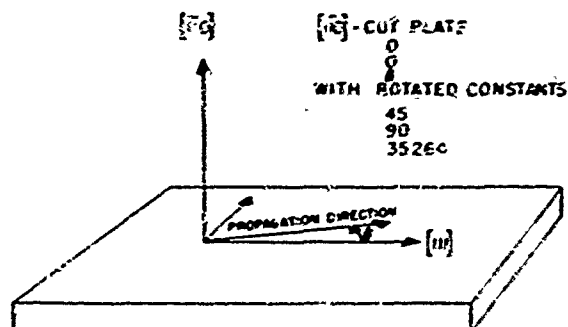


Figure D4. Standard Notation for a  $[1\bar{1}0]$ -cut Plate. Initial rotation through the Euler angles 45, 90, 35.264 aligns the propagation direction with the  $[111]$  crystalline axis and the plate normal with the  $[1\bar{1}0]$  crystalline axis. Further rotations in the plane of the plate are then accomplished through the angle  $\theta$